

Research Article

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Polymer nanocomposite for protecting photovoltaic cells from solar ultraviolet in space

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Abstract: Polymer nanocomposite coatings of solar photovoltaic cells that absorb solar ultraviolet (UV) radiation and convert it into visible and near-infrared (NIR) light can increase the operational lifetime and the energy efficiency of the cells. We report a polymer nanocomposite spectrum converting layer (SCL) made of colorless polyimide CORIN impregnated with the nanoparticles (NPs) of fluoride NaYF_4 doped with three-valent ions of Europium at a molar concentration of 60%. The NPs were the nanocrystals ($179 \pm 35\text{ nm}$ in size) in thermally stable hexagonal beta-phase. The visible-NIR photoluminescence quantum yield of the nano-powder was 69%. The SCLs were applied using the open-air multi-beam multi-target pulsed laser deposition method to silicon heterojunction (SHJ), copper-indium-gallium-selenide

(CIGS), and inverted metamorphic multijunction (IMM) solar cells. The cells were exposed to UV radiation from a 365 nm light emitting diode. The I - V characteristics of the cells were measured with a solar simulator using AMO filter. The proposed SCLs improved the UV stability of all three types of the cells: the power degradation of SHJs and IMM cells was stopped or slightly reversed and the degradation rate of CIGSs decreased by 25%. The proposed SCLs have great commercial potential, especially for applications to spare power.

Keywords: rare earth doped compounds, silicon heterojunction solar cell, copper-indium-gallium-selenide solar cell, inverted metamorphic multijunction solar cell, solar power, renewable energy, pulsed laser deposition, space vehicles

Abbreviations

AM	air mass
AO	atomic oxygen
BOL	beginning-of-life
CTGS	copper-indium-gallium-selenide
DLS	dynamic light scattering
EDTA	N-ethylenediaminetetraacetic acid
EOL	end-of-life
ESH	equivalent sun hours
GPIB-USB	general purpose interface bus-universal serial bus
IMM	inverted metamorphic multijunction
IPCE	incident photon to charge carrier efficiency
I - V	current-voltage
JCPDS	joint committee on powder diffraction standards
LED	light emitting diode
MBMT-PLD	multi-beam multi-target pulsed laser deposition
Nd:YAG	neodymium doped yttrium aluminum garnet
NP	nanoparticle
NIR	near-infrared
OS	oligomeric silsesquioxane

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PL	photoluminescence
PLD	pulsed laser deposition
PLQY	photoluminescence quantum yield
PV	photovoltaic
RE	rare-earth
SCL	spectrum converting layer
SEM	scanning electron microscopy
UV	ultraviolet
VIS	visible
XRD	X-ray diffraction

1 Introduction

Significant efforts have been put toward the development of polymer coatings protecting photovoltaic (PV) solar cells against harmful ultraviolet (UV) spectral components of solar radiation reducing operational lifetime (1- 5). The advantages of a polymer protecting layer over previously used semi-flexible cover glass are flexibility and light weight. This is critical for space applications with ultra-compact solar array deployment systems such as NASA's Lightweight Integrated Solar Array and AnTenna, slip wrapping concept by Caltech, and R3D2 antenna deployment system by MMA Design developed for small spacecraft (6). While protecting a solar cell, the polymer overcoat itself is subject to degradation under exposure to solar UV. This degradation reveals as darkening, yellowing, or sublimation (6). Besides, the energy of UV radiation just gets wasted in the polymer layer without producing electricity. In this study, we describe our efforts to make polymer nanocomposite layers that convert UV into visible and near-infrared (NIR) light that can be used by solar PV cells for producing extra electricity. We call such coatings the spectrum converting layers (SCLs). The configuration of a PV cell coated with an SCL is schematically presented in Figure 1. The SCL made of a polymer nanocomposite embedded with nanoparticles (NPs) is deposited on a protective (optically transparent) layer on the top of the PV cell. Both UV and visible-NIR spectral components of sun radiation reach the SCL. UV component is absorbed by the NPs and spectrally converted into visible-NIR radiation through the mechanism of downshifting. The visible-NIR radiation produced by the spectrum conversion along with the major visible-NIR components pass to the PV cell and generate extra electricity. On their passage through the SCL and the protecting layer, the major and extra visible-NIR radiation might have losses due to reflection, absorption, and scattering. Accordingly, the major yellow arrows below the SCL are shown slightly thinner. Protecting transparent layer can be absent. The SCL is expected to shield itself and

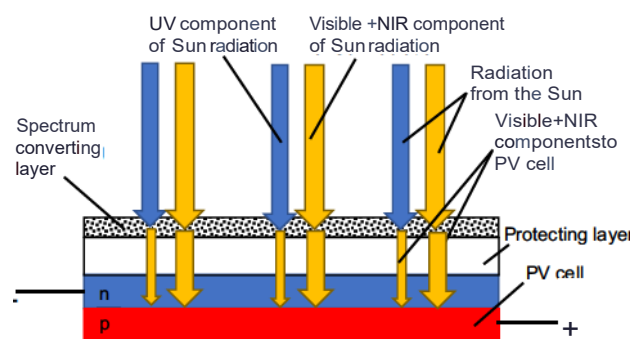


Figure 1: Sketch illustrating the usage of an SCL on the top of a solar PV cell. There is also solar UV, visible, and NIR radiation reflected from the SCL and the down-shifted visible and NIR radiation emitted by the SCL upwards that is not shown in the sketch.

the protecting layer and PV cell covered by it from solar UV radiation thus increasing operational lifetime. It must also improve photoelectric energy conversion efficiency. In this work, for the first time to our knowledge, we demonstrated that the proposed SCL improved the UV stability of three types of PV cells suitable for space power.

In Section 2 we describe the mechanism of spectrum conversion, the selection, and synthesis of the materials, making SCLs, and building the experimental setup for testing SCL prototypes. Section 3 includes the results and discussion of the experimental characterization of the performance of the SCL prototypes integrated with typical solar cells, including the candidates for space solar arrays followed by the conclusion in Section 4.

2 Materials and methods

2.1 Solar spectrum converting NPs

Among possible candidates for spectral conversion, we selected the NPs made of fluoride NaYF_4 doped with three-valent ions of rare-earth (RE) element Europium. NaYF_4 is a suitable host for RE ions due to its low phonon energy ($\sim 300 \text{ cm}^{-1}$) that makes multi-phonon assisted nonradiative relaxation of the excited ions weak (7). Superior performance of Eu^{3+} as an efficient spectrum converter in various inorganic matrices has been reported in the literature (8-18).

The powders of Eu-doped NaYF_4 compound were synthesized using the economic wet process, which in its essence is co-precipitation in the presence of N-ethylenediaminetetraacetic acid (EDTA). In a typical procedure, 21 g NaF (0.05 mol) was dissolved in 60 mL of deionized water. Another solution

was prepared by mixing $a \times 16\text{ mL}$ of 0.2-mol/L aqueous solution of YCl_3 and $b \times 16\text{ mL}$ of 0.2-mol/L solution of EuCl_3 and 20 mL of 0.2-mol/L EDTA aqueous stock solution to form the metal-EDTA complex ($a + b = 1$). All the chemicals were acquired from Millipore-Sigma. The complex solution was injected in the NaF solution quickly, and the mixture was stirred vigorously for 1 h at room temperature. After stirring, the mixture was allowed to stay overnight for the precipitate to settle. The precipitate was collected and washed several times with distilled water and anhydrous ethanol. In the second stage of the process, the precipitate was dried under vacuum to remove any traces of water. The resulting microcrystalline powder had a doping rate according to formula $\text{NaY}_{1-x}\text{Eu}_x\text{F}_4$. For instance, the 10% molar concentration of Eu corresponded to $a = 0.9$, $b = 0.1$. We synthesized the powders at various molar proportions between Y and Eu.

To investigate crystalline properties, we conducted the X-ray diffraction (XRD) spectroscopy of the obtained powders using a Bruker D2 Phaser X-ray diffractometer. The results are presented in Figure 2. Spectrum 1 corresponds to a portion of compound $\text{NaY}_0.9\text{Eu}_{0.1}\text{F}_4$; it was intentionally heat-treated at 500°C for 1 h. All other spectra are of freshly made compounds without heat treatment. Spectrum 1 is like the one of hexagonal β -phase of NaYF_4 (JCPDS No. 28-1192) that agrees with our earlier findings about heat treatment in the

study by Patel *et al.* (19). Spectra 2 and 3 of unheated powders with molar concentrations 10 and 20% of Eu^{3+} , respectively, are like the ones of cubic α -phase of NaYF_4 (JCPDS No. 77-2042). This is also in agreement with the study by Patel *et al.* (19). There is a little shift of the diffraction peaks to the left due to a slight change in the lattice volume caused by the substitution of Yttrium ions in their sites by Europium ions. However, for a molar concentration of 40% of Eu^{3+} , spectrum 4 becomes a mixture of the α - and β -phases, and for 60% of Eu^{3+} , spectrum 5 is like the one of hexagonal β -phase of NaEuF_4 (JCPDS No. 49-1987) (20).

The synthesized compounds were reduced to nano-powders by ball-milling in water using a PQ-N04 Planetary Ball Mill from Across International. The nano-powders were dried and transferred to organic solvent diglyme. The size distribution of the obtained NPs was measured using the Dynamic Light Scattering (DLS) method with a Zetasizer DLS instrument from Malvern Instruments. DLS scan of the size distribution of the NPs is presented in Figure 3. The size of the NPs (assuming their spherical shape) was determined as $179 \pm 35\text{ nm}$.

2.2 Optical properties of the spectrum converting compounds

The mechanism of spectrum conversion in Eu^{3+} is down-shifting as illustrated in the energy level diagram in Figure 4 (21). After absorbing UV photons and making transitions shown in the left part of the diagram, excited Eu^{3+} ions radiationlessly relax to lower energy levels and emit visible and NIR photons

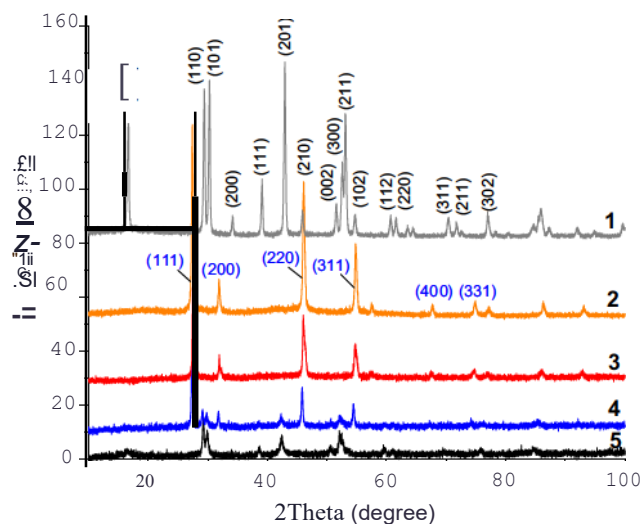


Figure 2: XRD spectra of $\text{NaYF}_4:\text{Eu}^{3+}$ powders at different molar concentrations of Eu. Spectrum 1 corresponds to $\text{NaY}_{0.9}\text{Eu}_{0.1}\text{F}_4$; heat-treated at 500°C (for 1 h); Spectrum 2 - freshly made $\text{NaY}_{0.9}\text{Eu}_{0.1}\text{F}_4$; Spectrum 3 - freshly made $\text{NaY}_{0.8}\text{Eu}_{0.2}\text{F}_4$; Spectrum 4 - freshly made $\text{NaY}_{0.6}\text{Eu}_{0.4}\text{F}_4$; Spectrum 5 - freshly made $\text{NaY}_{0.4}\text{Eu}_{0.6}\text{F}_4$. Numbers in parenthesis are triple-digit Miller indices. Spectrum 1 is like the spectrum of hexagonal β -phase of NaYF_4 (JCPDS No. 28-1192); Spectrum 2 is like the spectrum of cubic α -phase of NaYF_4 (JCPDS No. 77-2042); Spectrum 5 is like the spectrum of hexagonal β -phase of NaEuF_4 (JCPDS No. 49-1987).

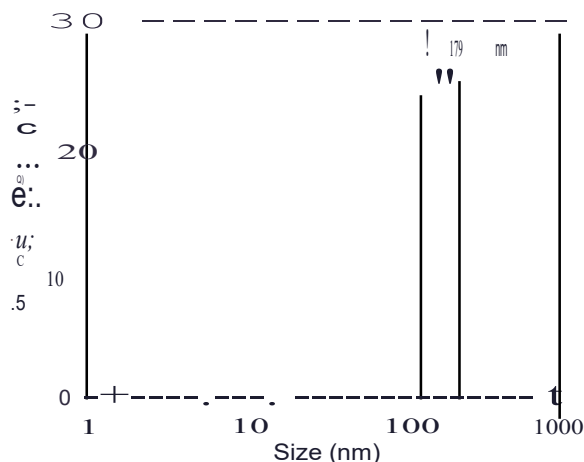


Figure 3: Size distribution of the NPs dispersed in diglyme. Concentration was 4 mg of solids per 3 ml liquids. The nanocolloid was filtered with a $1.0\mu\text{m}$ filter.

during the transition further down the energy ladder in the right half of the diagram. The samples for optical spectroscopy measurements were prepared by compressing the nano-powders into pellets using a 5-T hydraulic press. Figure 5 presents the diffuse reflectance spectrum of $\text{NaY}_0.4\text{F}_4\text{Eu}$ sample measured with a Shimadzu UV-2600-ISR-2600 Plus UV-VIS-NIR spectrophotometer with an integrating sphere (measurable spectral range was 190-1,400 nm). The inverted absorption peaks can be attributed to the transitions of Eu^{3+} ions to excited states: ${}^7\text{F}_0 \rightarrow {}^5\text{D}_0$ (362 nm), ${}^7\text{F}_0 \rightarrow {}^5\text{F}_5$ (375 nm), ${}^7\text{F}_0 \rightarrow {}^5\text{G}_7$ (382 nm), ${}^7\text{F}_0 \rightarrow {}^5\text{L}_6$ (395 nm), ${}^7\text{F}_0 \rightarrow {}^5\text{F}_4$ (415 nm), ${}^7\text{F}_0 \rightarrow {}^5\text{D}_2$ (465 nm), ${}^7\text{F}_0 \rightarrow {}^5\text{D}_1$ (526 nm), ${}^7\text{F}_1 \rightarrow {}^5\text{D}_1$ (535 nm), and ${}^7\text{F}_1 \rightarrow {}^5\text{H}_6$ (590 nm) shown in the left, "Absorption" part of the energy level diagram in Figure 4. Photoluminescence (PL) spectroscopy of the nano-powders was conducted with a spectrometer AvaSpec-ULS4096CL-EVO with integrating sphere AvaSphere-30 from Avantes and a fiber-coupled UV light emitting diode (LED) M365FP1 from Thorlabs (365 nm emission peak, 11 nm bandwidth) as a source of UV excitation. This source was suitable for simulating UV-A solar spectrum. The powder of heat-treated compound $\text{NaY}_0.4\text{F}_4\text{Eu}$ did not exhibit noticeable PL. All the unheated powders demonstrated PL with the intensity increasing with the increase in the concentration of Eu^{3+} . Starting from 10% molar concentration of $\text{Eu}(\text{NaY}_{0.4}\text{F}_4\text{Eu})$, the powders did not change their crystalline phase after heating at 500°C for several hours. They remained to be like hexagonal phase of NaEuF_4 . Correspondingly, heating did not bring the drop of PL intensity. This stability of PL under heating indicated that the SCL coated solar cells would operate steadily in space where the temperature exceeds $+120^\circ\text{C}$ (near earth or on the moon) or at higher temperatures (closer to the

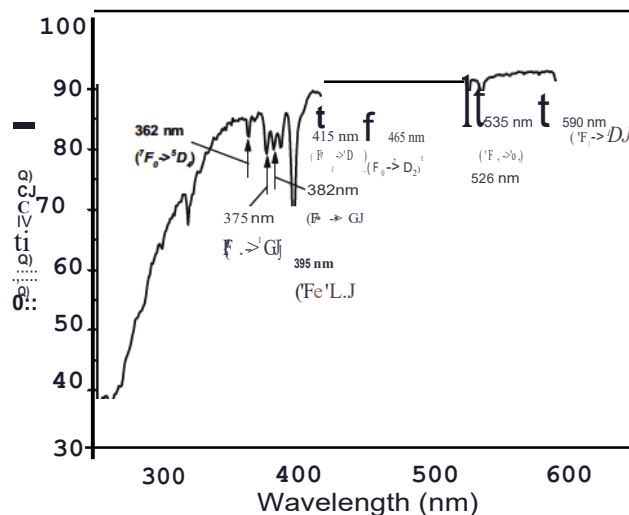


Figure 5: Diffuse reflectance spectrum of $\text{NaY}_{0.4}\text{F}_4\text{Eu}$ powder.

sun or near venus and mercury due to their surface heating). Figure 6 presents the PL spectrum of the NPs of $\text{NaY}_{0.4}\text{F}_4\text{Eu}$, illuminated with the 365 nm UV LED (its normalized emission spectrum is presented in the insert). The overall PL intensity and the intensity of individual peaks varied within no more than the 30% range from batch to batch of the synthesized $\text{NaY}_{0.4}\text{F}_4\text{Eu}$ powder. The plot in Figure 6 corresponds to the batch with the highest overall PL intensity that we used for making all the SCL samples in this study. PL peaks correspond to the transitions of the excited Eu^{3+} ions to the lower energy states in accordance with the right "Emission" part of the energy level diagram in Figure 4. Dominant spectral peaks (at 615 and 623 nm) were in

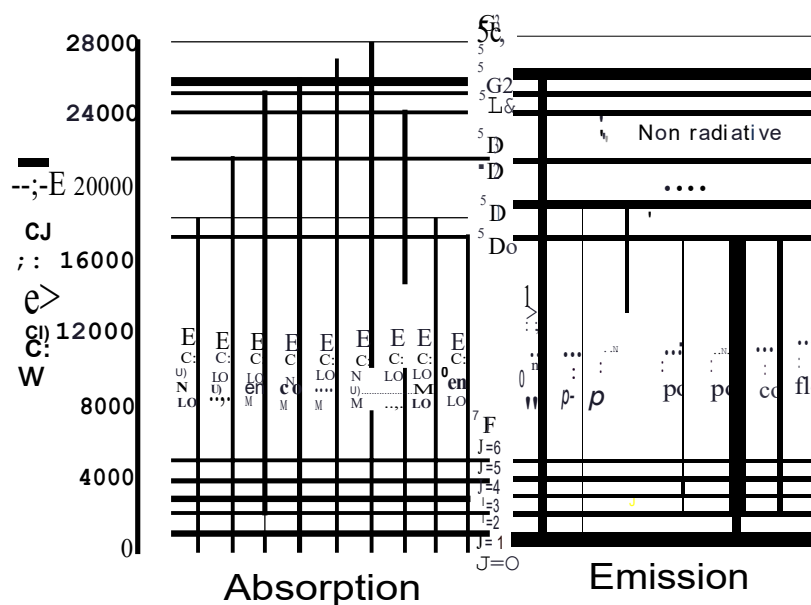


Figure 4: Energy level diagram of an Eu^{3+} ion [21].

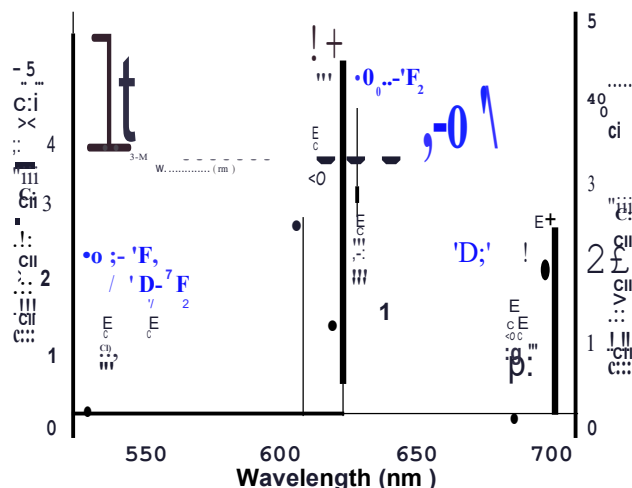


Figure 6: PL spectrum of (1) $\text{NaY}_{0.4}\text{F}_4:\text{Eu}$ powder sample and (2) the SCL over an SHJ cell illuminated by the 365 nm UV LED M365FP1 ($13.7 \text{ mW}/\text{cm}^2$ irradiance). The left vertical axis corresponds to plot 1 and the right to plot 2. The relative PL intensities of both spectra were computed by dividing actual intensities by the peak intensity of the incident UV radiation. The insert presents the normalized spectrum of the incident radiation from the UV LED. The spectrum of the UV LED simulated the UV-A spectral component of sun radiation.

the band corresponding to transition $^5\text{D}_0 \rightarrow ^7\text{F}_2$. The maximum PL quantum yield (PLQY, the ratio of the number of visible-NIR photons to the number of exiting IN photons) of the nanopowder was estimated using the method described in the study by Zhydashchuk *et al* (22) as ~69%. Figure 7 shows the PL spectrum of the nanopowder (presented in Figure 6) together with the spectrum of the IN LED radiation reflected from the powder pellet together with the spectra of Incident photon to charge carrier efficiency (IPCE) of three types of PV cells used in this work. The PL spectrum matched well with the IPCE spectra of the cells.

2.3 Polymer nanocomposite SCLs

For making SCLs, the NPs of $\text{NaY}_{0.4}\text{F}_4:\text{Eu}$ were dispersed in polymer CORIN® XLS from Nexolve (1). It is a fluorinated colorless polyimide with durability to atomic oxygen (AO) and oxygen plasma. It was designed to be a light-weight substitute material for the cover glass used in space PV arrays in low earth orbit. Polyimide molecules (Figure 8) have tethered oligomeric silsesquioxane (OS) pendant groups providing AO durability (26,27). Figure 9 presents the typical optical transmittance spectra of the film of pure CORIN and SCL on a glass substrate measured with the Shimadzu spectrophotometer. SCL had ~20% less transmittance than CORIN in visible spectral region due to stronger

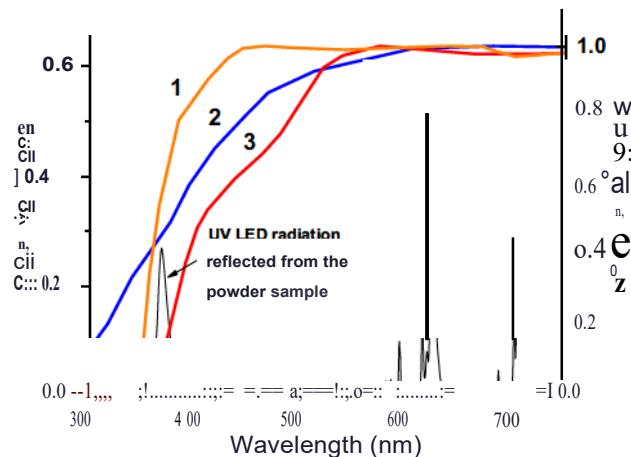


Figure 7: PL spectrum of $\text{NaY}_{0.4}\text{F}_4:\text{Eu}$ powder in Figure 6 presented together with the spectral peak of the pumping UV LED radiation reflected from the powder sample. Also shown are the normalized IPCE spectra of (1) IMM[23], (2) SHJ[24], and (3) CIGS[25] solar cells used in this study.

haziness. Haziness resulted more likely from light scattering on the large-size particles in the nanocomposite SCL. The insert in Figure 9 shows the scanning electron microscope (SEM) image of the SCL with evenly distributed NPs of the size distributed according to Figure 3. However, few large-size (>200 nm) particles can also be seen in the image. While the CORIN-coated glass sample did not transmit short-wave radiation with a wavelength shorter than 350 nm, the SCL-coated slide still transmitted radiation with a wavelength down to 300 nm. This could be because of weaker reflectance of the short-wave radiation from the interface between the SCL and the glass.

SCLs were deposited on solar cells using the open-air multi-beam multi-target pulsed laser deposition method invented by D. Darwish (28-46). The advantages of the method are low consumption of the material, potentially high accuracy of the thickness of the deposited layer (unfortunately not implemented in this work), and precise control of the concentration of the constituents along and across the deposited layer. We used two variants of the method. The first variant included preparation of a nanocomposite SCL compound by adding NPs to CORIN solution in diglyme at a proportion of approximately 0.53 mg solids per mL liquids and intense stirring. An SCL was then deposited on a moving solar cell using the ejection in open air (with flowing argon) of the liquid composition with a pulsed laser beam (46). In the second variant, SCLs were deposited on solar cells using the open-air (with flowing argon) two-beam two-target PLD (43,46). The first target was a pellet of a compressed spectrum converting nano-powder. The second target was a solution

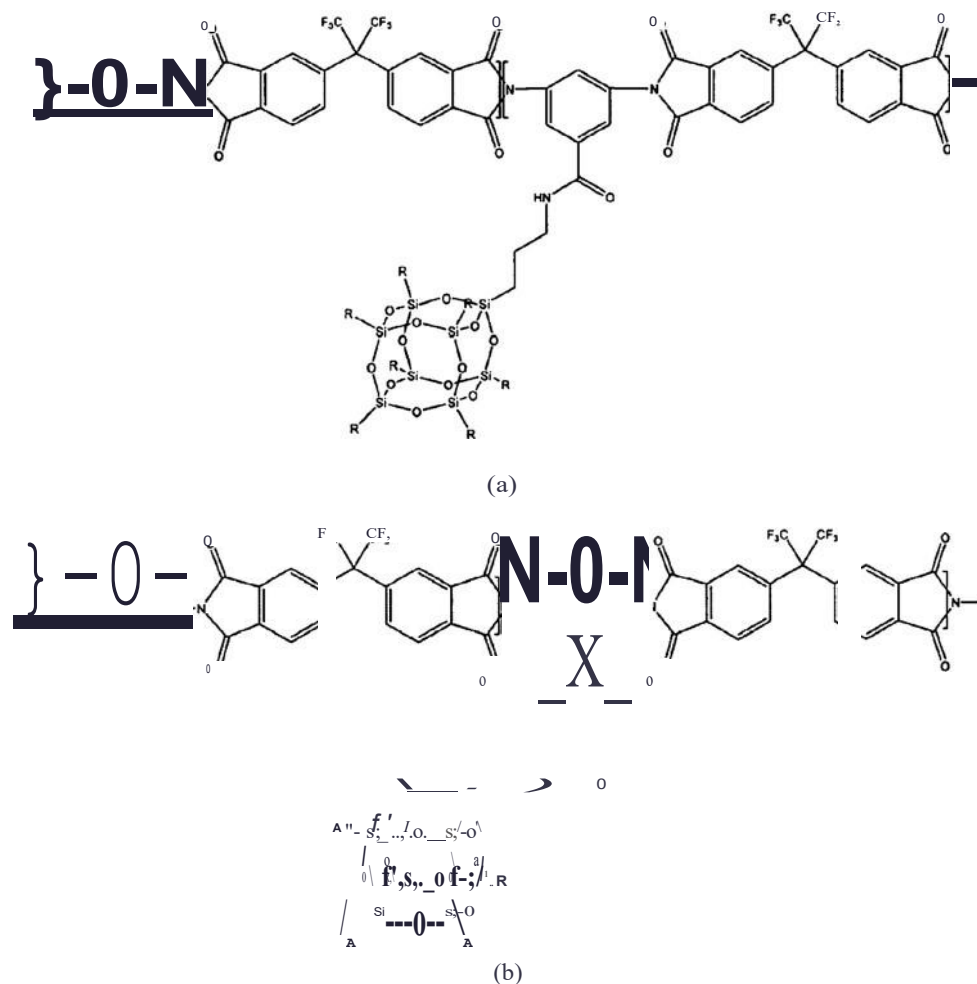


Figure8: Chemical formula of the chain link of CORIN polyimide with tethered OS pending unit connected with (a) an amide and (b) an ester.

of CORIN in diglyme. A 1,064 nm Q-switched Nd:YAG pulsed laser with 9-ns-long pulses, 0.4 J energy per pulse, and 10 pulses per second pulse rate was used as a source of laser pulses. After deposition, the polymer nanocomposite layers were heat-cured using a heat gun and overnight baking on a hot plate in ambient air at 80°C.

2.4 Experimental setup

Figure 10 presents the schematic of the experimental setup for testing SCL pro to types integrated with PV cells. A solar simulator LCS-100 model 94011A-ES from MKS-Newport with a Xe-lamp and Air Mass (AM) 0 filter (simulating solar spectrum above the atmosphere) was used as a light source. The shutter of the simulator was controlled with a shutter controller 71445 from MKS-Newport. The intensity of the light on the surface of a PV cell was adjusted by changing elevation

of the solar simulator over the cell. The irradiance in "suns," the units equivalent to the sun irradiance on the ground (100 mW/cm^2), was measured with a calibrated reference PV cell and a calibrated meter model 91150 V from MKS-Newport. The measurement of I - V characteristics was conducted automatically under computer control using LabVIEW software developed for MKS-Newport I - V Test Station PVIV-1A (47). Voltage was automatically applied to the PV cell, and the flowing electric current was measured by a computer-controlled Keithley 2400 Source and Measurement Unit. The unit was connected to the computer through GPIB-USB interface.

The uncoated and coated solar cells were exposed in vacuum to UV radiation from 50 to 100 W LED arrays from Shenzhen Chanzon Technology Co., Ltd. This radiation had a spectral band of -20 nm around the peak at 365 nm suitable to simulate UV-A component of solar UV spectrum in space. Exposure time was calibrated in the Equivalent solar hours (ESH).

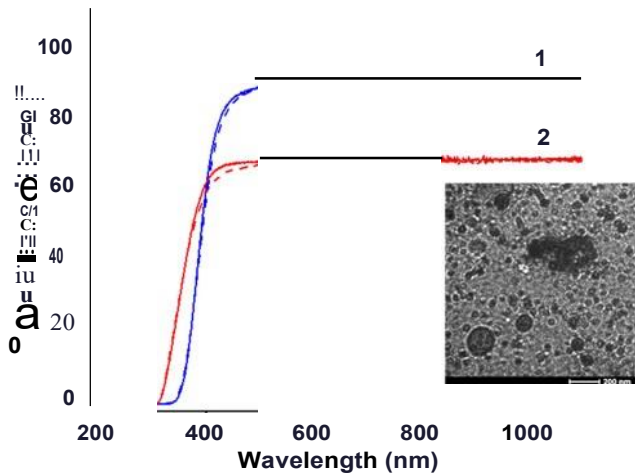


Figure 9: Typical optical transmittance spectrum of (1) the coating made of pure CORIN (thickness = $15 \pm 6.4 \mu\text{m}$) and (2) SCL (thickness = $17.1 \pm 5.9 \mu\text{m}$) on a $158 \mu\text{m}$ thick microscope cover glass. Dashed lines show the transmittance after exposure to UV radiation in vacuum for 1,600 ESH. The insert is the high-resolution SEM image of the SCL coating taken with a JEOL SEM instrument. Arrows are the NPs.

3 Results and discussion

3.1 I - V characteristics of the coated PV cells

For testing SCLs, we chose three types of solar cells: silicon heterojunction (SHJ) cells from Solestial (dimensions: $3.0 \text{ cm} \times 4.65 \text{ cm}$, $\sim 14.0 \text{ cm}^2$ area and dimensions: $3.0 \text{ cm} \times 5.2 \text{ cm}$, 15.6 cm^2 area), copper-indium-gallium-selenide (CIGS) flexible

cells (dimensions: $4.75 \text{ cm} \times 4.75 \text{ cm}$, 17.77 cm^2 active area; according to the manufacturer, the cells are "truly bare" with no protective coating over the front conductors made of silver conductive paste), and epitaxial lift-off inverted metamorphic multijunction (IMM) flexible cells from MicroLink (dimensions: $3.0 \text{ cm} \times 6.6 \text{ cm}$, 19.8 cm^2 area). Investigation of possible improvement in the PV energy conversion efficiency of PV cells and IN stability was conducted by comparing the I - V characteristics of the cells coated with SCLs against bare cells or the cells coated with pure CORIN. A total of five randomly picked SHJ, eight CIGS, and five IMM cells were used in the study. SHJ and IMM cells demonstrated no noticeable ageing for at least 8 months of storage in the lab conditions at room temperature. CIGS cells, according to manufacturer's recommendations, were stored in inert gas (argon) atmosphere at room temperature (to prevent degradation of silver front conductors) and did not show ageing for 6 months. The thicknesses of SHJ, CIGS and IMM cells were measured as 250 ± 2 , 68 ± 3 , and $30 \pm 2 \mu\text{m}$, respectively. The thickness of CORIN/SCL coating on SHJ cells was not possible to measure precisely because the polymer penetrated inside the micro-pores on the surface made by etching to reduce optical reflectance. It was estimated to be between 6 and $16 \mu\text{m}$. The thicknesses of CORIN/SCL coatings of CIGS cells after curing were measured as $15.6 \pm 8.1 \mu\text{m}$; the CORIN/SCL on IMM thicknesses were measured as $61 \pm 3.2 \mu\text{m}$. Despite being uneven, the coatings were optically smooth (roughness did not exceed ~ 0.2 – $0.3 \mu\text{m}$) since they demonstrated mirror-like reflection of incident light.

The PL spectrum of the SCL excited by the 365 nm UV LED is presented in Figure 6 (curve 2). It fully replicated the

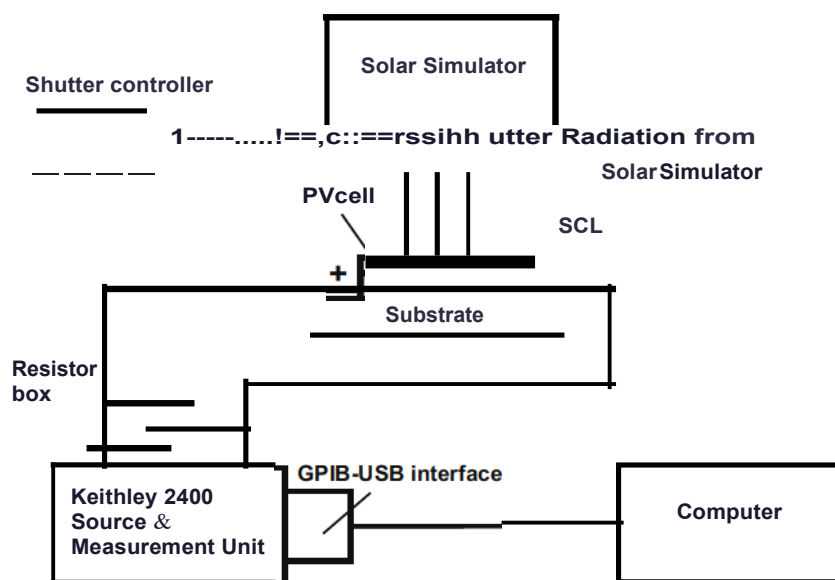


Figure 10: Schematic of the experimental setup for testing SQ prototypes deposited on PV cells.

PL spectrum of the Eu-doped nano-powder excited with the same source (Figure 6, curve 1). PLQY of the SCL was estimated as $\sim 0.5\%$, much less than that of the nano-powder. This was because the dispersion of the NPs in the solid polymer matrix at a concentration of $\sim 26.5 \text{ mg/mL}$ resulted in $\sim 6.4 \times 10^{19} \text{ cm}^{-3}$ concentration of the photoluminescent spectrum downshifting Eu^{3+} ions while their concentration in the nano-powder was $\sim 1.3 \times 10^{22} \text{ cm}^{-3}$, 203 times greater. Second, the incident UV radiation was partially absorbed in the CORIN polymer matrix of the SCL. We also inspected the spectra of the solar simulator radiation reflected from the SCL-coated PV cells in comparison with the spectra from CORIN-coated ones. Typical examples are presented in Figure 11 (SCL on an SHJ cell) and Figure 12 (SCL on an IMM cell). Zoom-in inserts in the figures show the difference between SCL-related and non-SCL spectra in the region 550–650 nm where the PL peaks at 615 and 623 nm attributed to the SCL are discernible. This extra visible/NIR PL radiation generated by the SCL joined the visible/NIR light from the solar simulator on its passage to the PV cell according to the concept illustrated in Figure 1.

Graphs in Figure 13a and b present the I - V characteristics of the SHJ cells before and after coating with no exposure to UV radiation. For the sake of comparability of the I - V characteristics regardless of the actual area of the cells, instead of photoelectric current I current density J was used in all I - V plots. Figure 13a illustrates the case

when two layers of CORIN were deposited and Figure 13b illustrates the case when one layer of CORIN and the SCL on the top as in the configuration in Figure 1 (bottom CORIN functioned as a protecting layer). In both cases the coatings brought the photogenerated current density down compared to the no-coating case, SCL brought it down more.

Figure 13c presents the photograph of a bare SHJ cell at room illumination. The cell was cut from a 5-inch (127-mm) SHJ wafer. An SHJ wafer coated with one layer of CORIN and SCL on the top and illuminated with a 365-nm UV LED is shown in Figure 13d. Red PL was produced by the SCL.

The performance parameters extracted from the I - V characteristics in Figure 13a and b (as described in the Application Note [48]) are presented in Table 1, the third and fourth columns, rows 2 through 5. Besides standard parameters, such as open circuit voltage V_{oc} , short circuit current I_{sc} , short circuit current density J_{sc} , maximum power P_{max} , and efficiency η , we also computed maximum power density $PD_{max} = P_{max}/A$, where A is the active cell area. This parameter was convenient in comparing PV power generated by different cells regardless of their actual area. As can be seen from Table 1 (the fourth column, rows 2 and 3), the 0.1% drop of η of the unexposed bare cell from 11.2 down to 11.1% brought by the double-layer CORIN coating was statistically insignificant: less than the maximal statistical spread of 1.0%. The SCL-caused 21% efficiency drop from 13.9 down to 11.8% was

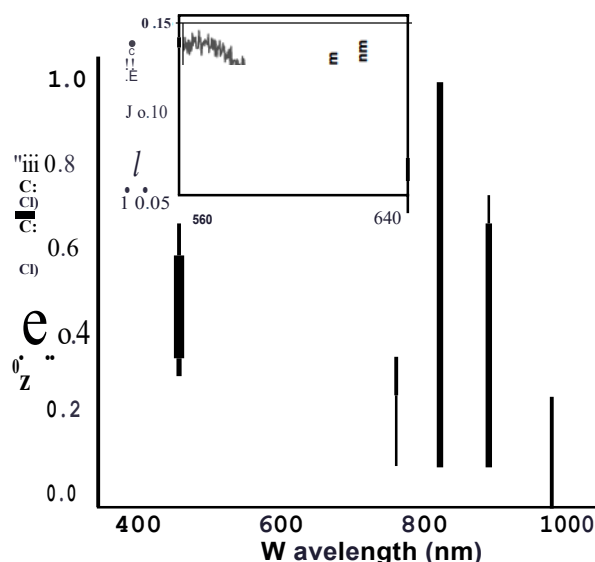


Figure 11: Normalized (to the highest peak at 824 nm) spectrum of the radiation of the solar simulator (AMO filter) reflected from (1) SHJ cell coated with two layers of CORIN and (2) SHJ cell coated with one layer of CORIN and SCL on the top. Zoom-in insert shows the difference between graphs 2 and 1 in the spectral region 550–650 nm where the PL peaks at 615 and 623 nm attributed to the SCL are visible.

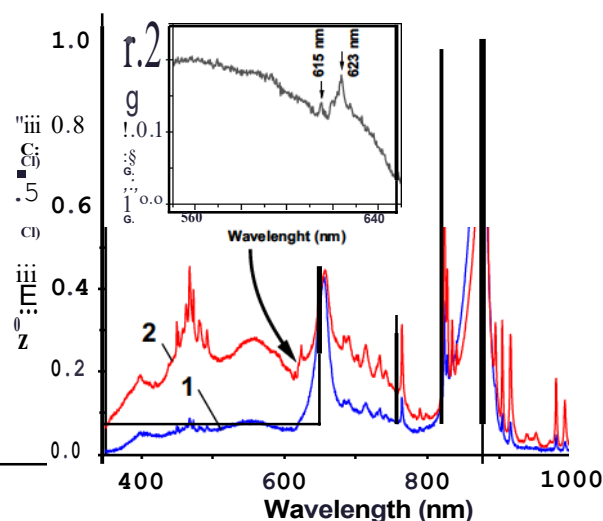


Figure 12: Normalized (to the highest peak at 873 nm) spectrum of the radiation of the solar simulator (AMO filter) reflected from (1) IMM cell coated with CORIN and (2) IMM cell coated with SCL. Zoom-in insert shows the difference between graphs 2 and 1 in the spectral region 550–650 nm where the PL peaks at 615 and 623 nm attributed to the SCL are visible.

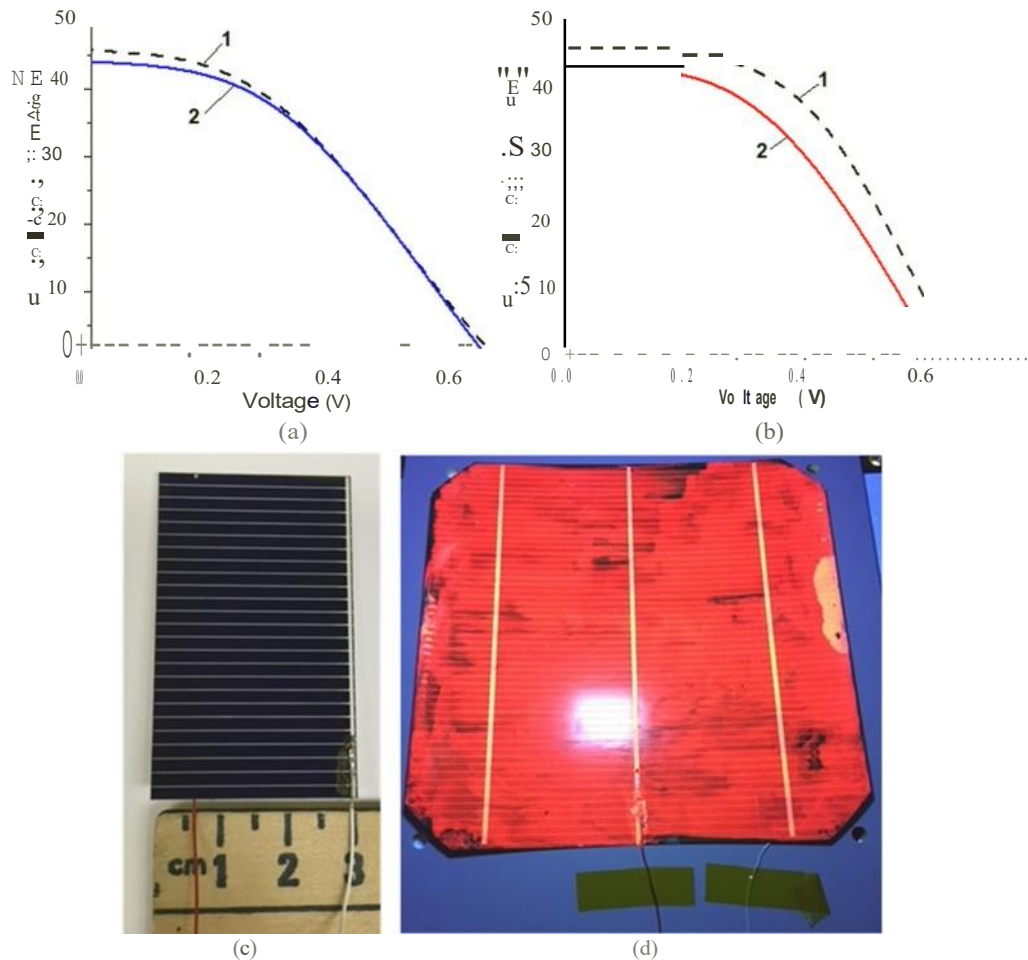


Figure 13: (a) I - V characteristics of an unexposed SHJ cell before coating (curve 1) and after coating with two layers of CORIN (curve 2). (b) I - V characteristics of an unexposed SHJ cell before coating (curve 1) and after coating with one layer of CORIN and SCL on the top (curve 2). During I - V measurements, the cells were illuminated by the solar simulator with an intensity equivalent to 1.367 Sun (AMO filter), the so-called solar constant - solar irradiance above the atmosphere. (c) General view of a bare SHJ cell. It was cut from an SHJ wafer. (d) An SHJ wafer coated with one layer of CORIN and SCL on the top illuminated with a 365nm UV LED. Red PL in (d) was produced by the SQ.

greater than the 15% spread. Correspondingly, the same applied to P_{max} and PD_{max} (q was proportional to P_{max} and PD_{max}). As was verified by the reflectance measurements, both coatings reduced the so-called optical coupling of the incident light to the cells (6) or, in other words, increased the reflection of the incident light. This happened primarily because the polymer smoothened the surface texture of the cells intentionally etched to minimize reflectance. In the case of the SCL, another negative factor was the increased light scattering mentioned above (when the optical transmittance data in Figure 9 was discussed). The spectrum downshifted PL did not compensate for the loss of the visible solar radiation reaching the cell.

We exposed the SHJ cell to LN radiation in vacuum (simulating solar LN in space) for a duration varying from 5,000 to 7,000 ESH, measured I - V characteristics for different exposure

durations t , and extracted P_{rrwo} $PD =$ and q from each measured I - V characteristic. The change in q caused by LN exposure was evaluated using the dimensionless relative efficiency change $Ar_{rel} = (q - q_{00}) / q_{00} \times 100\%$ to compare different cells regardless of the absolute values of the efficiency; q_{00} was the Beginning-of-Life (BOL) efficiency before exposure ($t = 0$ ESH). In Table 1 q_{BOL} is presented in the fourth column. Experimental plots of rel_{15} duration t in ESH for the exposed cells are presented in Figure 14. Plots in Figure 14a and b were fitted with function $rel_{15}(t) = [\exp(Rt) - 1] \times 100\%$, where fitting parameter R had the meaning of the efficiency evolution rate. Plot in Figure 14c was fitted with function $rel_{15}(t) = A(1 - \exp(Rt)) \times 100\%$. The graphs of the fitting functions are presented by the sets of three lines: the middle, thicker line is the evolution graphs corresponding to the mean values of the fitting parameters $X_{mean} (i = 1, 2, 3; X = R, J_{fl-I} = A, \frac{J_{fl-I}}{X} = R/J$.

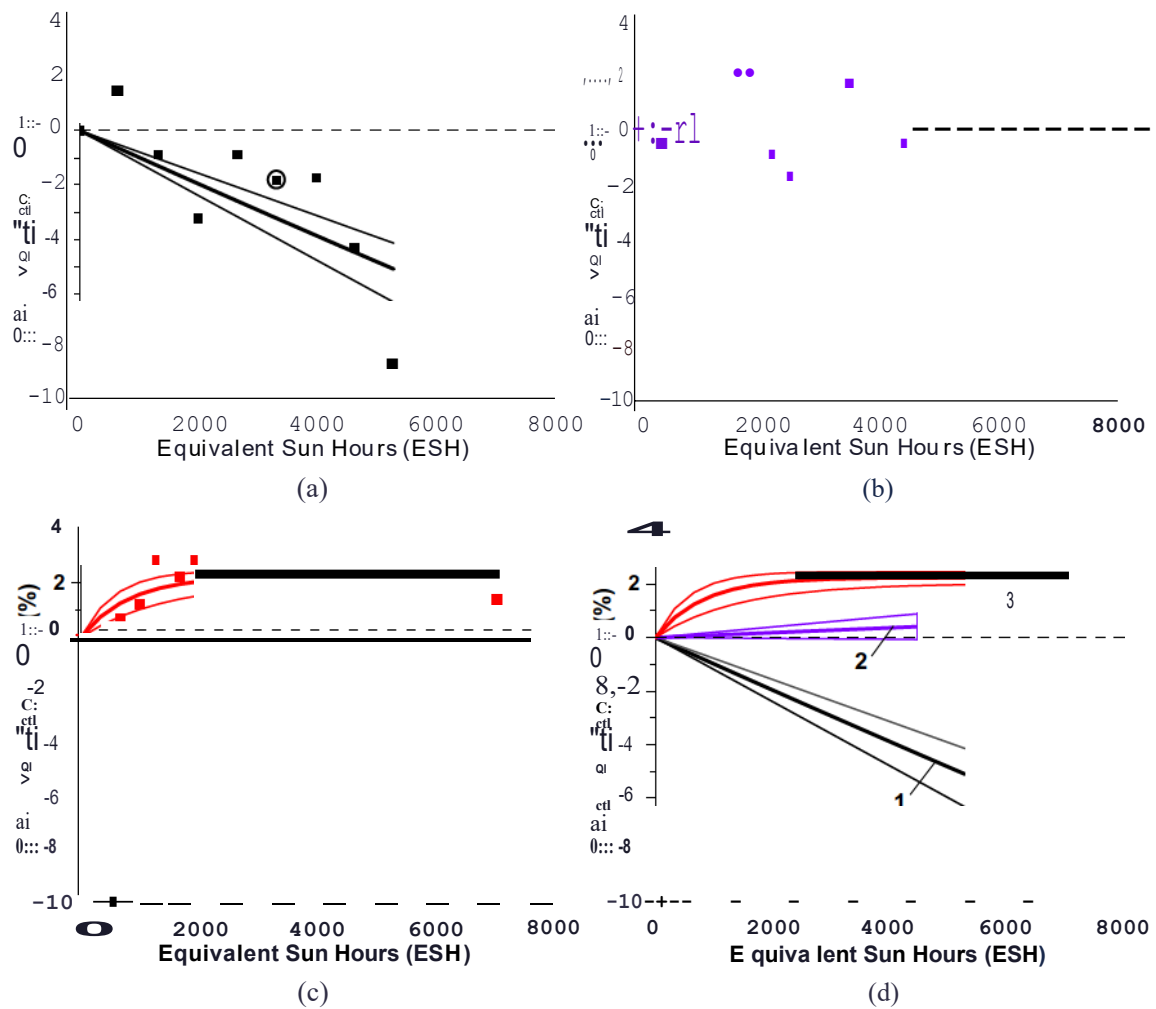


Figure 14: Experimental evolution plots of the relative efficiency change $\frac{\Delta \eta}{\eta_0}$ (a) bare SHJ cell, (b) SHJ cell coated with two layers of CORIN, and (c) SHJ cell coated with one layer of CORIN and SCL on the top. Solid lines are the graphs of the functions fitting the experimental points. The middle thick lines are the graphs of the fitting functions corresponding to the mean values of the fitting parameters. The marginal, thinner lines correspond to the marginal values equal to the mean values plus/minus standard deviations determined during fitting computations. Circles mark the experimental points corresponding to the data in Table 1 for ~3,000 ESH exposure duration. A square marks the experimental point corresponding to the data in Table 1 for ~6,000 ESH exposure duration. For convenience of comparison, fitting graphs for all the cells are presented together in (d). Set of fitting lines 1 corresponds to bare SHJ cell, Set of fitting lines 2 corresponds to SHJ coated with two layers of CORIN, and Set of fitting lines 3 corresponds to SHJ coated with CORIN and SCL on the top.

Two marginal thin lines on both sides from the middle are the graphs corresponding to the marginal values of the fitting parameters X_0 and X_1 equal to the mean values plus/minus the standard deviations ΔX of fitting $X = X_0 + X_1$. For convenience of comparison, the fitting evolution graphs for all three types of the SHJ cells are presented together in Figure 14d. According to Figure 14, the uncoated SHJ cell experienced performance degradation (Figure 14a and evolution graph 1 in Figure 14d) while the CORIN-coated cell had a slight performance increase (Figure 14b and graph 2 in Figure 14d), and the SCL-coated cell got a performance increase followed by saturation (Figure 14c and graph 3 in Figure 14d). The evolution

graphs (Figure 14d) are so different that their error margins do not overlap. The IN degradation of bare SHJ cells has been explained in the literature by an increase in hydrogen concentration near the Si/passivation interface and, as a result, a drop of short circuit current I_{sc} and open circuit voltage V_{oc} [SO]. Improved IN stability caused by CORIN (graph 2) could be a result of blocking IN by CORIN. The SCL-caused performance improvement (graph 3) could be assumed to originate from the growing acceptance of IN solar light (confirmed by our measurements of the optical reflectance of the SCL-coated cells) and the downshifted PL (indicated by 615 and 623 nm peaks in Figure 11).

Table 1: Performance parameters of the SHJ cells extracted from their I - V characteristics

Number of the row	Time of exposure	0 ESH		-3,000 ESH	-6,000 ESH
	Parameter	V_{oc} (I,c) U_{sc}	P_{max} (P_{Dmax}) [q]"	P_{max} (P_{Dmax}) [7]	P_{max} (P_{Dmax}) [7]
	Unit	V (mA) [mA/cm ²]	mW (mW/cm ²) [%]	mW (mW/cm ²) [%]	mW (mW/cm ²) [%]
2	Uncoated SHJ cell	0.681 ± 0.007 (708 ± 8) [45.3 ± 0.5]	176 ± 10 (11.3 ± 0.6) [10.5 ± 0.5]	173 ± 10 ^b (11.1 ± 0.6) [10.2 ± 0.5]	170 ± 12 ^c (10.9 ± 0.8) [10.0 ± 0.8]
	SHJ cell before coating with two layers of CORIN	0.681 ± 0.007 (711 ± 8) [45.6 ± 0.5]	190 ± 10 (12.2 ± 0.6) [11.2 ± 0.5]	184 ± 11 ^d (11.8 ± 0.6) [10.8 ± 0.6]	178 ± 13 ^d (11.4 ± 0.8) [10.5 ± 0.8]
3	SHJ cell coated with two layers of CORIN	0.664 ± 0.007 (685 ± 7) [43.9 ± 0.4]	188 ± 10 (12.1 ± 0.6) [11.1 ± 0.5]	188 ± 10 ^e (12.1 ± 0.6) [11.1 ± 0.5]	189 ± 11 ^c (12.2 ± 0.7) [11.2 ± 0.7]
	SHJ cell before coating with one layer of CORIN and one SCL on the top	0.654 ± 0.007 (645 ± 7) [46.2 ± 0.5]	211 ± 12 (15.1 ± 0.9) [13.9 ± 0.9]	204 ± 14 ^d (14.6 ± 1.0) [13.4 ± 0.9]	199 ± 1 ^r (14.3 ± 12) [13.1 ± 1.1]
5	SHJ cell coated with one layer of CORIN and one SCL on the top	0.681 ± 0.007 (604 ± 6) [43.3 ± 0.4]	180 ± 10 (12.9 ± 0.7) [11.8 ± 0.6]	189 ± 11 ¹ (13.5 ± 0.8) [12.3 ± 0.8]	184 ± 11 ⁹ (13.2 ± 0.8) [12.1 ± 0.7]

•Efficiency was measured at an irradiance of 1.367 Sun (136.7 mW/cm^2) with AMO filter in the solar simulator and at the temperature in the lab varying between 22 and 27°C. It was corrected to the true efficiency that, according to ASTM E948-16 Standard [49], had to be measured at an irradiance of 1.0 Sun (100.0 mW/cm^2) with AM 1.5 G filter at a temperature of 25°C. ^bExact exposure time was 3,321 ESH. ^cDue to the lack of experimental data, the values were estimated using the results of fitting experimental data in Figure 14. ^dExpected values estimated using the results of fitting experimental data in Figure 14. ^eExact exposure time was 3,147 ESH. ¹Exact exposure time was 2,981 ESH. ⁹Exact exposure time was 6,205 ESH.

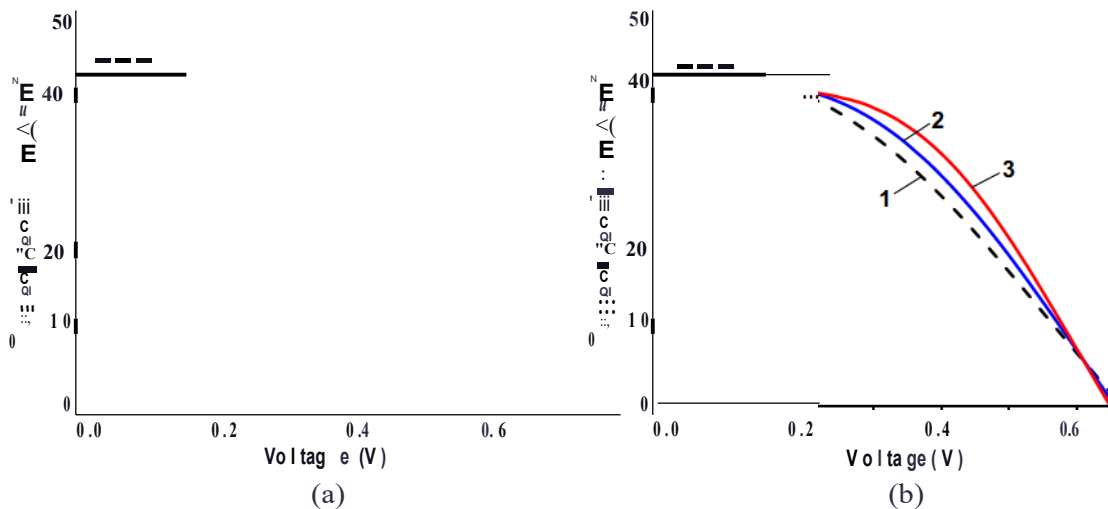


Figure 15: I - V characteristics of three different SHJ cells (a) before UV exposure and (b) after UV exposure for -3,000 ESH. Curve 1 corresponds to the bare cell, curve 2 corresponds to the cell coated with two layers of CORIN, and corresponds to curve 3 corresponds to the cell coated with one layer of CORIN and SCL on the top. Actual exposure time of the bare cell was 3,321 ESH, CORIN-only-coated cell - 3,147 ESH, CORIN+ SCL-coated- 2,981 ESH. During I - V measurements, the cells were illuminated by the solar simulator with an intensity of 1.367 Sun (AMO filter).

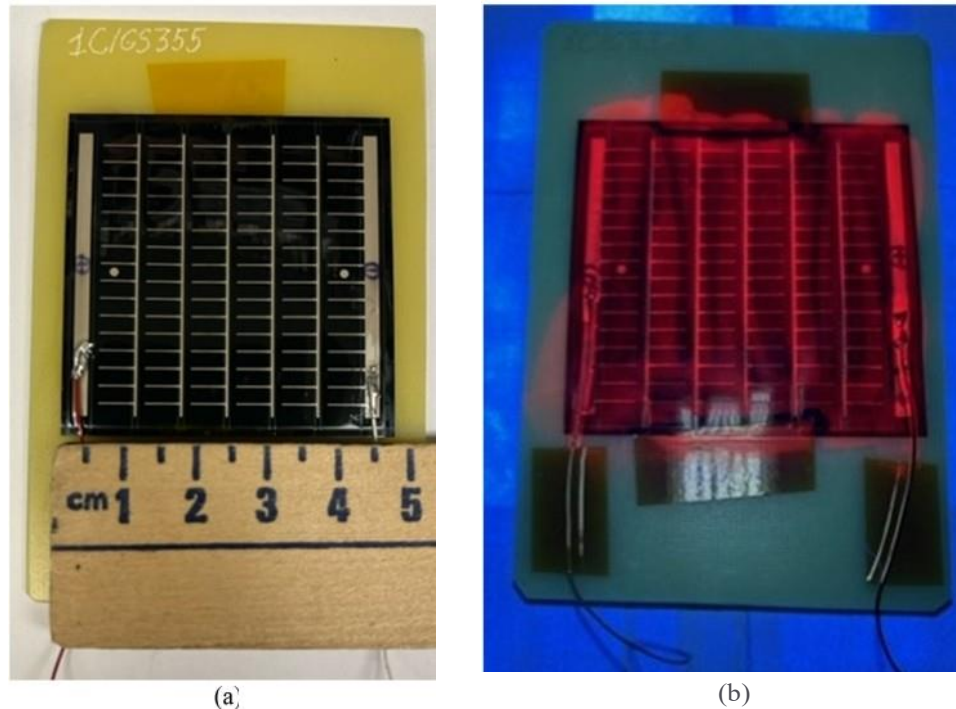


Figure 16: (a) General view of a CIGS cell coated with SCL. (b) The same cell illuminated with UV light from a 365 nm UVLED. Red PL was produced by the SQ.

We also compared the I - V characteristics of three different SHJ cells, bare, double CORIN-, and CORIN + SCL-coated, before and after UV exposure for -3,000 ESH as shown in Figure 15. The values of P_{max} , PD_{max} , and J extracted from these characteristics are presented in Table 1,

columns 4 and 5, rows 1, 3, and 5. The corresponding experimental points of A_{Jre1} we re marked with circles in the plots in Figure 14a- c. They were located (with the exception in Figure 14a) close to the fitting graphs. The bare cell initially performed less than the other two, and the CORIN + SCL-

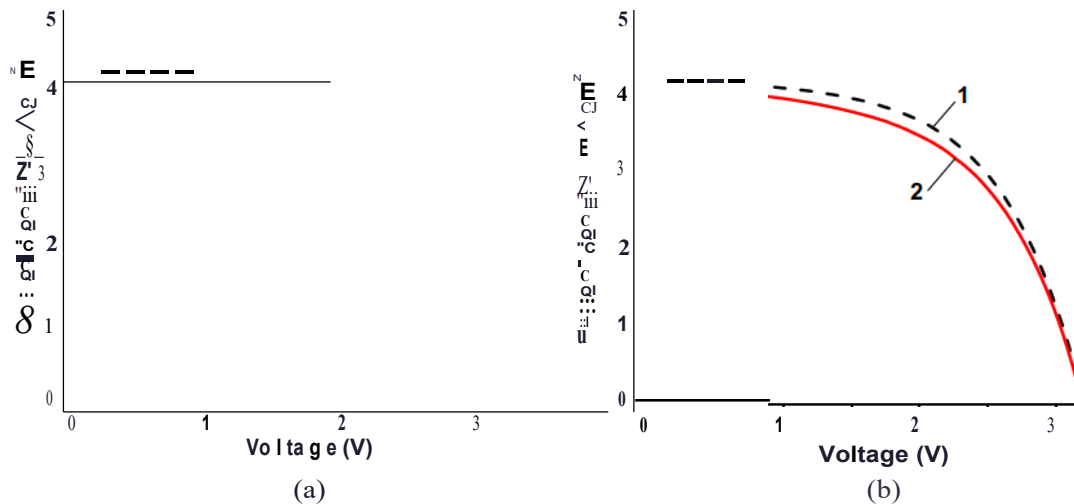


Figure 17: (a) I - V characteristics of an unexposed CIGS cell before coating (curve 1) and after coating with CORN layer (curve 2). (b) I - V characteristics of an unexposed CIGS cell before coating (curve 1) and after coating with SQ (curve 2). During I - V measurements, the cells were illuminated by the solar simulator with an intensity of 1.367 Sun (AMO filter). After the article was prepared for publication the manufacturer of CIGS cells suggested that the active area of the cell was 17.77 cm^2 instead of 22.5625 cm^2 used in the computations. Correspondingly, the current density in (a) and (b) should be increased 1.27 times.

coated one was the highest achiever. After - 3,000 ESH of exposure, the performance gap between the underperformer (bare cell) and the frontrunner (CORIN+SCL-coated one) widened. The performance of the CORIN-coated cell did not noticeably change. Using the available experimental data or the estimates derived from the fitting functions in Figure 14 (if the experimental data were not available,) we also obtained the performance parameters of three SHJ cells for -6,000 ESH exposure duration. They are presented in Table 1, sixth column, rows 1, 2, and 4. The corresponding experimental point of η_{rel} was marked with a square in the plot in Figure 14c. It was located close to the fitting graph. The gap between the performance parameters of the bare cell and the CORIN-only and CORIN-SCL cells continued to widen. However, the change in the performance of individual cells with time was less or comparable to the statistical spread

(statistically insignificant). Comparison of the expected performance parameters of the would-be coated cells (that were double CORIN- or CORIN+SCL-coated) for -3,000 and -6,000 ESH in Table 1, columns 5 and 6, rows 2 and 4 with the parameters of the true uncoated cell in row 1 show their correlation in terms of degradation with exposure time.

Figure 16 presents the photographs of an SCL-coated CTGS cell illuminated with room and IN light. SCL being IN illuminated produced red PL attributed to the Europium doped downshifting NPs. The $I-V$ characteristics of the CIGS cells, uncoated and coated, before IN exposure are presented in Figure 17. The performance parameters of the cells are presented in Table 2, columns 3 and 4, rows 2 through 5. In this case, CORIN coating brought a slight increase in η (by 0.4%) with respect to the bare cell. SCL reduced η by 0.4%. But these changes in performance in

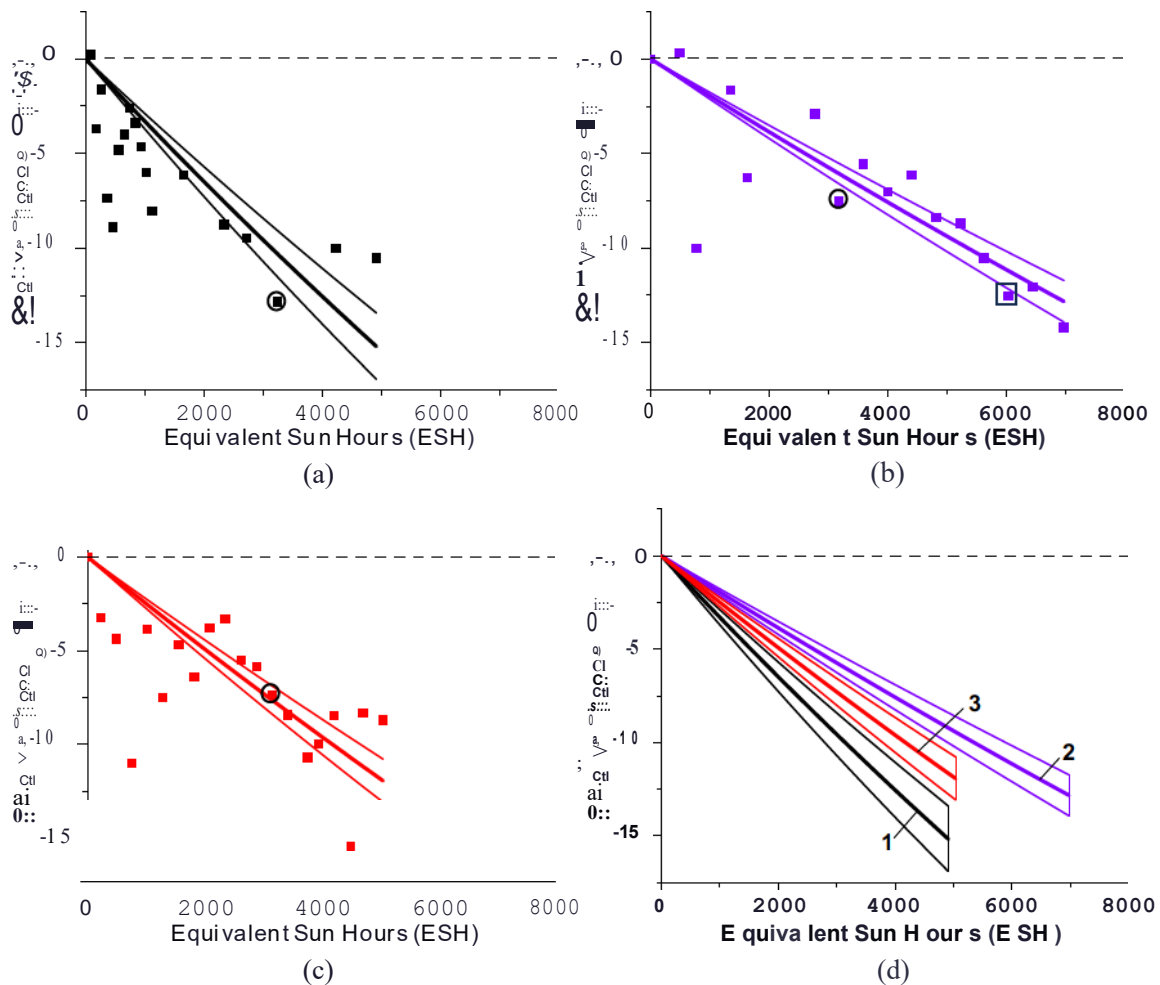


Figure 18: Experimental evolution plots of the relative efficiency change η_{rel} of (a) bare CIGS cell, (b) CIGS cell coated with CORIN, and (c) CIGS cell coated with SCL. Solid lines are the graphs of the functions fitting the experimental points. Circles mark the experimental points corresponding to the data in Table 2 for ~3,000 ESH exposure duration. A square marks the experimental point corresponding to the data in Table 2 for ~6,000 ESH exposure duration. (d) For convenience of comparison, fitting graphs for all the cells are presented together in. Set of lines 1 corresponds to bare CIGS cell, while 2 corresponds to CIGS coated with CORIN, and 3 corresponds to CIGS coated with SCL.

both cases are less than 1.0% statistical spread of q . The effect of the coatings on the performance of unexposed CIGS cells could thus be considered statistically insignificant.

After the article was prepared for publication the manufacturer of CIGS cells suggested that the active area of the cell was 17.77 cm^2 instead of 22.5625 cm^2 used in the computations. Correspondingly, the current density in Figure 17 and Table 2 as well as power density and efficiency in Table 2 should be increased 1.27 times.

Experimental evolution plots of η , J , P of the UV-exposed CIGS cells are presented in Figure 18. All the plots were fitted with function $\ln(f, e^{1Ct}) = [\exp(Rt) - 1] \times 100\%$, where fitting parameter R had the meaning of the efficiency evolution rate. Like in Figure 14, the graphs of the fitting functions were presented by the sets of three lines: the middle, thicker line and two thin marginal lines corresponding to the marginal values of $R \pm$ equal to the mean value R_{mean} plus/minus the standard deviations σR of fitting $R \pm = R_{\text{mean}} \pm \sigma R$. For convenience of comparison, the fitting evolution graphs for all three types of CIGS cells were presented together in Figure 18d. The uncoated CIGS cell (Figure 18a and set 1 in Figure 18d) experienced significant performance degradation while the CORIN-coated (Figure 18b and set 2 in Figure

18d) and SCL-coated (Figure 18c and set 3 in Figure 18d) cells degraded less. UV caused performance degradation of the bare CIGS cell (Figure 18a and set 1 in Figure 18d) was explained in the literature by the erosion of the front electric conductors followed by the increase in their sheet resistance (51.) Photographs of the microscopic images of the front conductors of the studied CIGS cells in Figure 19e-h confirmed this hypothesis. UV exposure of the bare front conductors of SHJ (Figure 19a-d) and IMM cells (Figure 19i-l) resulted in fluffy edges. But the white electroconductive (made of silver paste) layer of the front conductor of a bare CIGS cell (Figure 19e) completely changed its color to dark yellow after -5,000 ESH of UV exposure (Figure 19f). This was more likely due to oxidation of silver. The CORIN-coated CIGS cell remained almost intact after -7,000 ESH (Figure 19g). The conductor of the SCL-coated cell remained partially intact after -5,000 ESH (Figure 19h). Slowing UV degradation down by CORIN and the SCL could thus be due to counter-UV shielding of the front conductors. The fact that the SCL provided weaker shielding of the front conductors than CORIN explains why the SCL-coated cell degraded a bit faster (but still slower than the bare cell). The SCL was less effective on the CIGS technology more likely due to the formation of pinholes in the

Table 2: Performance parameters of the CIGS cells extracted from their 1-V characteristics•

Number of the row	Time of exposure	0 ESH			
		-3,000 ESH			
	Parameter	V_{oc} (I, cl U_{sc})	P_{max} (PDmax) (I, J)	P_{max} (PDmax) (I, J)	P_{max} (PDmax) (I, J)
	Unit	V (mA) [mA/cm ² J]	mW (mW/cm ²) [%]	mW (mW/cm ²) [%]	mW (mW/cm ²) [%]
2	Uncoated CIGS cell	3.14 ± 0.09 (92.4 ± 1.9) [4.10 ± 0.09]	155 ± 11 (6.8 ± 0.5) (6.2 ± 0.4)	135 ± 10 ^a (5.9 ± 0.4) (5.4 ± 0.3)	137 ± 13 ^b (6.0 ± 0.6) (5.5 ± 0.5)
	CIGS cell before coating with CORIN layer	3.34 ± 0.10 (98.8 ± 2.0) [4.38 ± 0.09]	179 ± 13 (7.9 ± 0.6) (7.2 ± 0.5)	162 ± 15 ^c (7.1 ± 0.7) (6.5 ± 0.6)	146 ± 17 ^d (6.4 ± 0.7) [5.9 ± 0.7]
	CIGS cell coated with CORIN layer	3.41 ± 0.10 (97.4 ± 2.0) [4.32 ± 0.09]	185 ± 14 (8.2 ± 0.6) (7.6 ± 0.5)	171 ± 13 ^d (7.6 ± 0.6) (7.0 ± 0.5)	162 ± 12 ^e (7.2 ± 0.5) [6.7 ± 0.5]
	CIGS cell before coating with SCL	3.20 ± 0.09 (95.6 ± 2.0) [4.24 ± 0.09]	173 ± 13 (7.7 ± 0.6) (7.1 ± 0.5)	156 ± 15 ^c (6.9 ± 0.7) [6.4 ± 0.6]	142 ± 17 ^c (6.3 ± 0.8) [5.8 ± 0.7]
5	CIGS cell coated with SCL	3.19 ± 0.09 (93.4 ± 1.9) [4.14 ± 0.08]	163 ± 12 (7.2 ± 0.5) [6.7 ± 0.5]	151 ± 11 ^f (6.7 ± 0.5) [6.2 ± 0.5]	143 ± 14 ^b (6.3 ± 0.6) [5.9 ± 0.6]

• due to the corrections provided by the manufacturer after the article was prepared for publication current density J_{sc} , power density PD_{max} , and efficiency η must be increased 1.27 times. • Exact exposure time was 3,245 ESH. ^b Due to the lack of experimental data, the values were estimated using the results of fitting experimental data in Figure 18. ^c Expected values were estimated using the results of fitting experimental data in Figure 18. ^d Exact exposure time was 3,176 ESH. • Exact exposure time was 6,037 ESH. ^f Exact exposure time was 3,126 ESH.

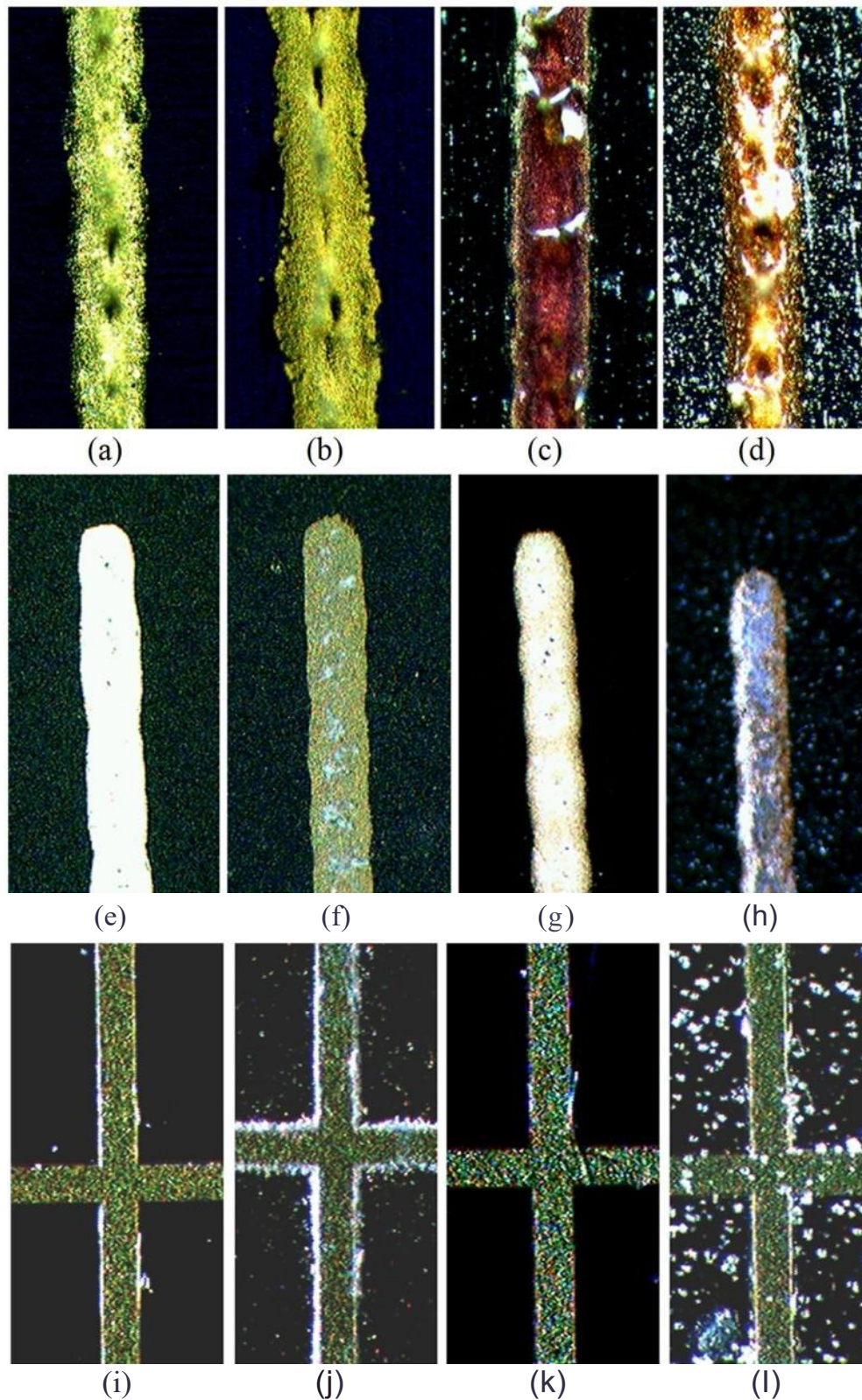


Figure 19: Microscopic images (40x magnification) of the front conductor of (a) bare unexposed SHJ cell, (b) bare SHJ cell UV-exposed for 5,294 ESH, (c) SHJ cell coated with two layers of CORIN and UV-exposed for 4,453 ESH, (d) SHJ cell coated with one layer of CORIN and SCL on the top and UV-exposed for 7,058 ESH, (e) bare unexposed CIGS cell, (f) bare CIGS cell UV-exposed for 4,913 ESH, (g) CORIN-coated CIGS cell exposed for 6,977 ESH, (h) SCL-coated OGS cell exposed for 5,038 ESH, (i) bare unexposed IMM cell, (j) bare IMM cell UV-exposed for 6,870 ESH, (k) CORIN-coated IMM cell exposed for 6,736 ESH, and (l) SCL-coated IMM cell exposed for 5,693 ESH. Images (e)-(h) are enlarged -1.5 times with respect to images (a)-(d), images (i)-(l) are enlarged -2 times.

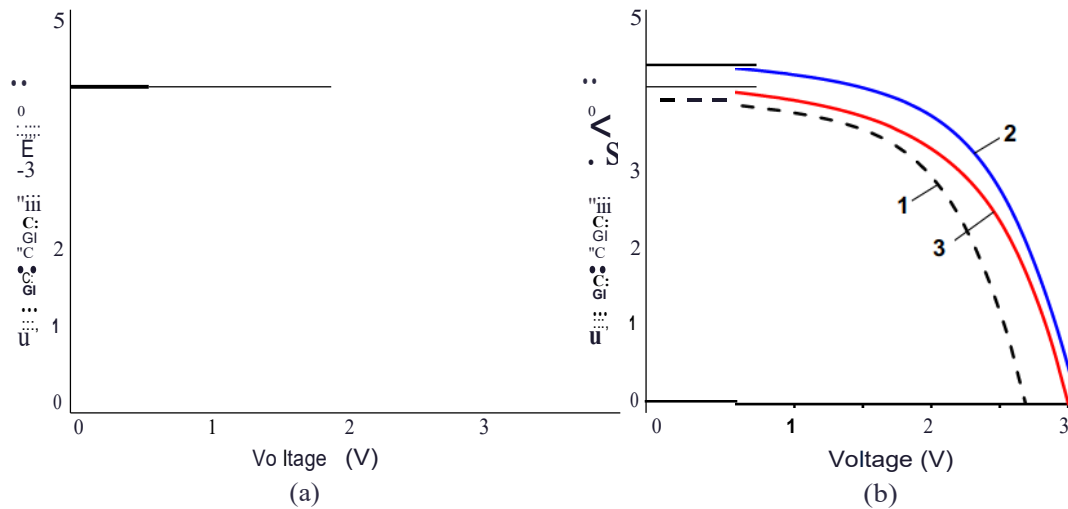
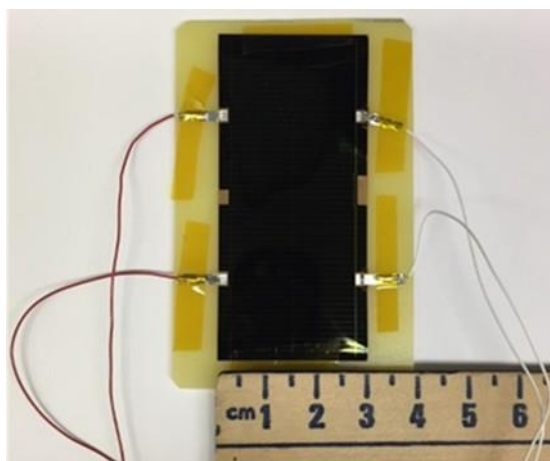


Figure 20: I - V characteristics of three different CIGS cells (a) before UV exposure and (b) after UV exposure for $\sim 3,000$ ESH. Curves 1 correspond to the bare cell, curves 2 correspond to the cell coated with one layer of CORIN, and curves 3 correspond to the cell coated with the SCL. The actual exposure time of the bare cell was 3,245 ESH, CORIN-coated cell was 3,176 ESH, and SCL-coated cell was 3,126 ESH. During I - V measurements, the cells were illuminated by the solar simulator with an intensity of 1.367 Sun. Due to the corrections provided by the manufacturer after the article was prepared for publication, current density in (a) and (b) must be increased 1.27 times.

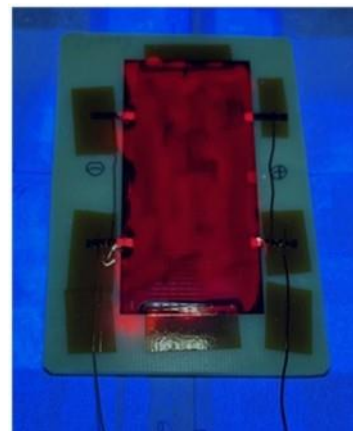
CORIN because of the NP deposition, which would re-expose the silver top contacts. The silver contacts on the CIGS only experienced degradation due to the lack of a protective coating, as evidenced by the CORIN-coated module. SHJ and IMM cells might have initial anti-IN coating preventing front conductors from complete degradation.

We also compared the I - V characteristics of three different CIGS cells, bare, CORIN-, and SCL-coated, before and after IN exposure for $\sim 3,000$ ESH as shown in Figure 20.

Due to corrections provided by the manufacturer, the current density in Figure 20 should be increased 1.27 times. The values of P_{max} , PD , and q extracted from these characteristics are presented in Table 2, columns 4 and 5, rows 1, 3, and 5 (they must also be increased 1.27 times). Relative change $\Delta \eta$ was negative for all three types of cells due to IN-induced aging, but the performance gap between the exposed bare CIGS cell and the coated cells (especially the CORIN-coated one) widened. Additionally, we put the experimental data for the



(a)



(b)

Figure 21: (a) General view of a bare IMM cell from Microlink; (b) an SCL-coated IMM cell illuminated with a 365 nm UV LED. Red PL in (b) was produced by the SCL.

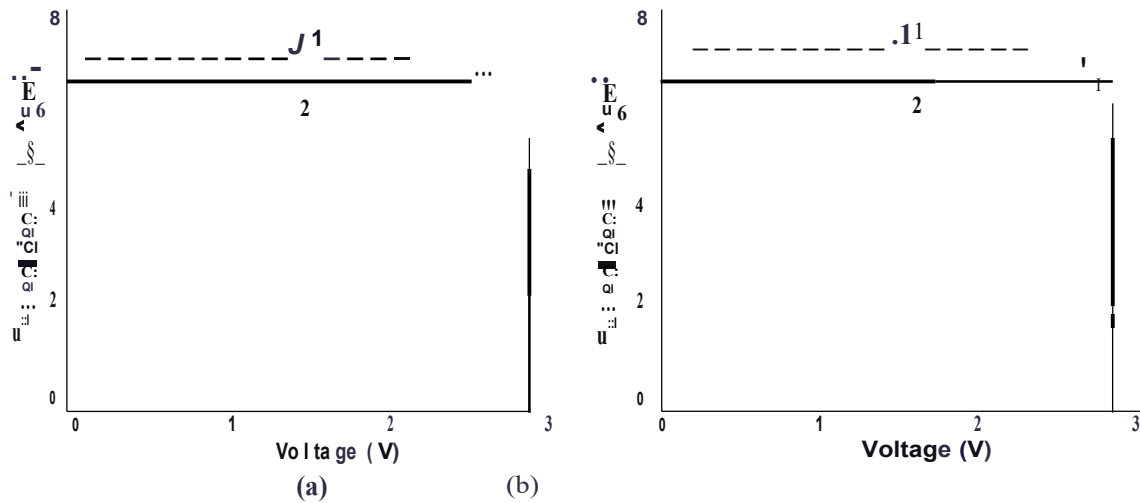


Figure 22: (a) 1-V characteristics of an unexposed IMM cell before coating (curve 1) and after coating with one layer of CORIN (curve 2). (b) 1-V characteristics of an unexposed IMM cell before coating (curve 1) and after coating with the SCL (curve 2). Considering greater (relative to SHJ and CIGS) IMM cell dimensions (3.0 cm × 6.6 cm), the cells were illuminated at a maximal achievable for the solar simulator irradiance of 0.875 Sun (AMO filter). This was less than 1.367 Sun used for SHJ and CIGS cells.

Table 3: Performance parameters of the IMM cells extracted from their 1-V characteristics

Number of the row	Time of exposure	0 ESH		-3,000 ESH	-6,000 ESH
	Parameter	V _{oc}	P _{mu}	P _{mu}	P _{max}
		(I _{sc} , J _{sc})	(PD _{max})	(PD _{max})	(PD _{max})
		$\frac{V_{oc}}{I_{sc}}$	111	111	111
Unit		V	mW	mW	mW
		(mA)	(mW/cm ²)	(mW/cm ²)	(mW/cm ²)
		[mA/cm ² J]	[%]	[%]	[%]
2	Uncoated IMM cell	2.91 ± 0.02	376 ± 13	365 ± 13b	364 ± 13c
		(143.5 ± 2.4)	(18.9 ± 0.7)	(18.4 ± 0.7)	(18.3 ± 0.7)
		[7.23 ± 0.12]	[27.2 ± 1.0]	[26.5 ± 1.0]	[26.4 ± 0.9]
	IMM cell before coating with CORIN layer	2.88 ± 0.02	353 ± 13	346 ± 14d	336 ± 16d
3		(140.1 ± 2.3)	(17.8 ± 0.7)	(17.4 ± 0.7)	(17.0 ± 0.8)
		[7.07 ± 0.12]	(25.6 ± 1.0]	(25.1 ± 1.0]	(24.4 ± 1.1]
	IMM cell coated with CORIN layer	2.93 ± 0.02	339 ± 12	327 ± 12"	321 ± 11t
		(132.3 ± 2.1)	(17.1 ± 0.6)	(16.5 ± 0.6)	(16.2 ± 0.5)
4		(6.68 ± 0.11]	(24.6 ± 0.9]	(23.8 ± 0.9]	(23.3 ± 0.9]
	IMM cell before coating with SCL	2.89 ± 0.02	376 ± 13	369 ± 15d	359 ± 16d
		(144.9 ± 2.3)	(19.0 ± 0.7)	(18.6 ± 0.8)	(18.1 ± 0.8)
		[7.32 ± 0.12]	[27.3 ± 1.0]	[26.7 ± 1.1]	[26.1 ± 1.1]
5	IMM cell coated with SCL	2.91 ± 0.02	350 ± 13	350 ± 12g	351 ± 16h
		(134.1 ± 2.2)	(17.7 ± 0.7)	(17.7 ± 0.6)	(17.8 ± 0.8)
		[6.6 ± 0.11]	[25.5 ± 1.0]	(25.5 ± 0.9]	[25.6 ± 1.2]

•Efficiency was measured at an irradiance of 0.875 sun (87.5 mW/cm²) with AMO filter in the solar simulator and at the temperature in the lab varying between 22 and 27°C. It was corrected to the true efficiency based on ASTM E948-16 Standard [49]. bExact exposure time was 3,026 ESH. cExact exposure time was 6,269 ESH. dExpected values were estimated using the results of fitting experimental data in Figure 23. eExact exposure time was 3,020 ESH. fExact exposure time was 6,037 ESH. gExact exposure time was 3,298 ESH. hDue to the lack of experimental data, the values were estimated using the results of fitting experimental data in Figure 23.

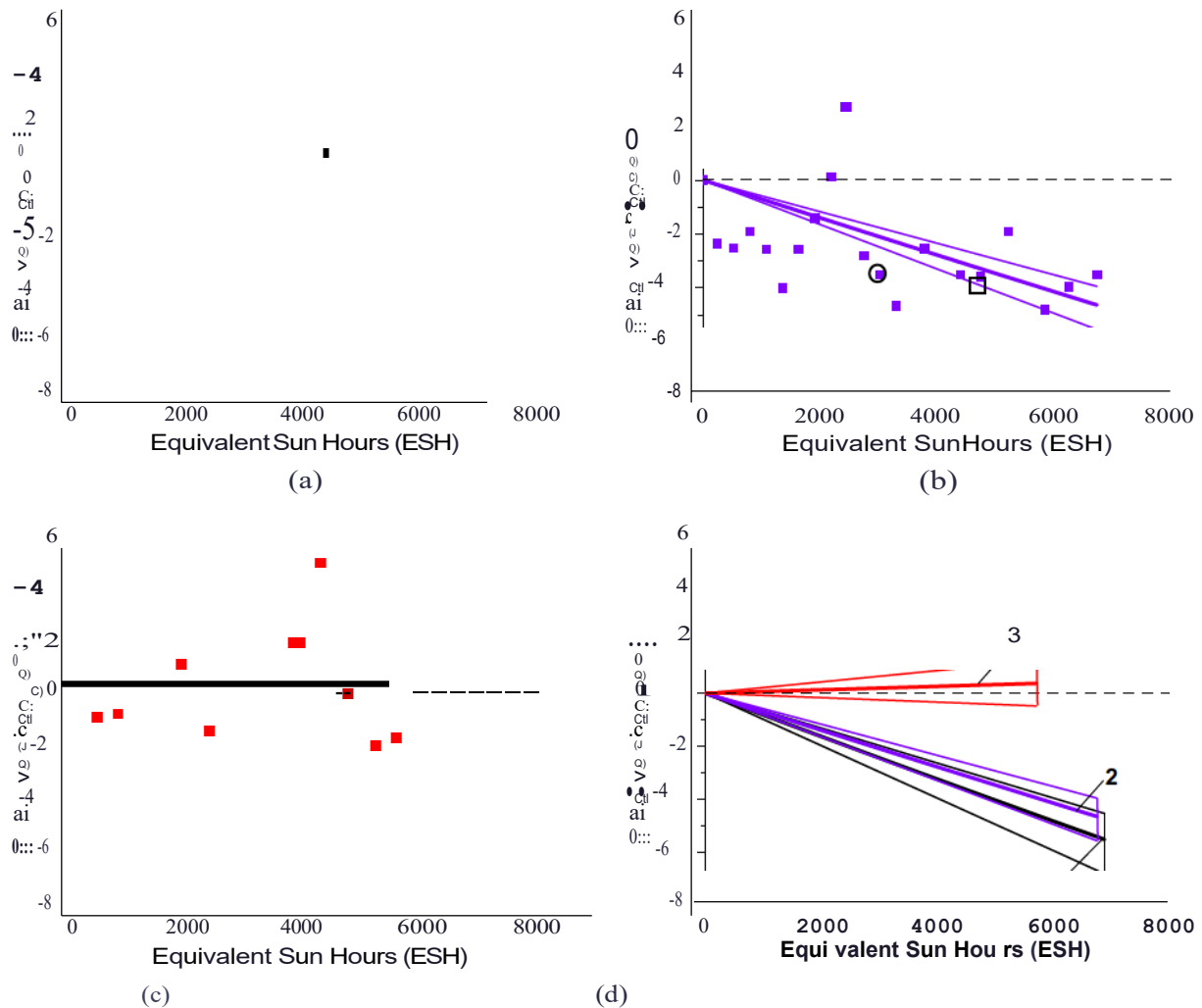


Figure 23: Experimental evolution plots of the relative efficiency change of (a) bare IMM cell, (b) IMM cell coated with CORIN, and (c) IMM cell coated with SCL. Solid lines are the graphs of the functions fitting the experimental points. Circles mark the experimental points corresponding to the data in Table 3 for -3,000 ESH exposure duration. Squares mark the experimental points corresponding to the data in Table 3 for -6,000 ESH exposure duration. (d) For convenience of comparison, fitting graphs for all the cells are presented together. Set of lines 1 corresponds to bare IMM cell, while 2 corresponds to IMM coated with CORIN, and 3 corresponds to IMM coated with SCL.

CORIN-coated CTGS cell exposed for -6,000 ESH (data point marked with a square in Figure 18b) and the performance parameters of the would-be-uncoated and the true uncoated and coated cells for -3,000 and -6,000 ESH (estimated using the fitting functions in Figure 18) in Table 2, columns 5 and 6, rows 1-5. The data for the would-be-uncoated and the true W-coated cells showed good correlation.

Figure 21 shows the photographs of a bare IMM cell at room illumination and the SCL-coated one under IN illumination. SCL on the top of the latter cell produced red PL attributed to the spectrum downshifting in the embedded NPs. The I - V characteristics of the IMM cells, uncoated and coated, before UV exposure are presented in Figure 22. The performance parameters of the cells extracted from the

I - V characteristics are presented in Table 3, columns 3 and 4, rows 2-5. Both coatings brought down the photocurrent and the efficiency of the cells (though not significant relative to the statistical spread). Like in the case of the SHJ cells, reflectance measurements indicated that the coating-caused performance drop could be due to the increased reflection and scattering (especially in the case of the SCL) of the incident light.

Figure 23 presents the experimental evolution plots of the I - V of the UV-exposed IMM cells. All the plots were fitted with function $I(t) = [\exp(Rt) - 1] \times 100$ (%), with evolution rate R as a fitting parameter. Like in Figures 14 and 18, the graphs of the fitting functions were presented by the sets of three lines: the middle, thicker line and two thin

marginal lines corresponding to the marginal values of R . For convenience, the fitting evolution graphs for all three types of IMM cells are presented together in Figure 23d. The uncoated IMM cell (Figure 23a and set 1 in Figure 23d) experienced performance degradation. The CORIN-coated (Figure 23b and set 2 in Figure 23d) experienced slightly less degradation while the SCL-coated one (Figure 23c and set 3 in Figure 23d) demonstrated performance stability.

Figure 24 presents the I - V characteristics of different bare, CORIN-, and SCL-coated IMM cells before and after IN exposure for -3,000 ESH. The short circuit current density J_{sc} of the bare cell remained relatively high and stable before and after exposure. But the open circuit voltage V_{oc} of the bare cell as well as that of the CORIN-coated one degraded compared to the SCL-coated cell. Our measurements revealed that the SCL-coated cell reflected solar IN three to five times greater than the CORIN-coated and bare one, respectively. The stabilizing effect of the SCL on the IMM cell could thus be explained by fending off solar IN and keeping V_{oc} from decreasing. Downshifted PL (indicated by 615 and 623nm peaks in the spectrum in Figure 12) could also contribute to the SCL's performance stabilizing role in the case of an IMM cell. The drop of V_{oc} in PV cells has been explained in the literature by the generation of parasitic defect-related traps in the energy gap of the p-n junctions (our IMM cells had three p-n junctions) and narrowing the gap [52]. Answering why such phenomena took place in our case would require detailed investigation beyond the scope of this work. The values of P_{max} , PD_{max} ,

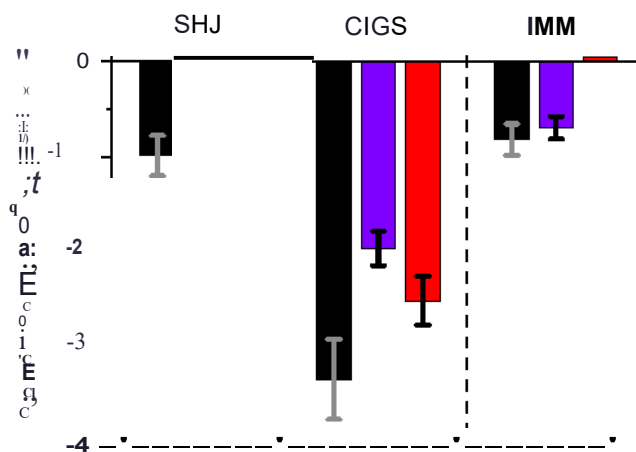


Figure 25: Chart diagram of the rates of the relative efficiency change $[Y]_{-1}$ of the uncoated and coated solar cells studied in this work. The bars of black color (left from the center of each solar cell group) correspond to the bare cells, blue bars (center) correspond to CORIN-coated (two layers of CORIN in the case of SHJ) cells, red (right from the center) correspond to SCL-coated (CORIN layer and SQ on the top in the case of SHJ) ones. The error bars are presented by thin grey/black lines. Thin bars near zero correspond to the cases when there is no efficiency degradation of the cells.

and II extracted from I - V characteristics in Figure 24 are presented in Table 3, columns 4 and 5, rows 3 and 5. Additionally, we put the experimental data for the bare and CORIN-coated IMM cells exposed for -6,000 ESH (data points marked with squares in Figure 23a and b) and the performance parameters of the would-be-uncoated and the true uncoated and coated cells for -3,000 and -6,000 ESH

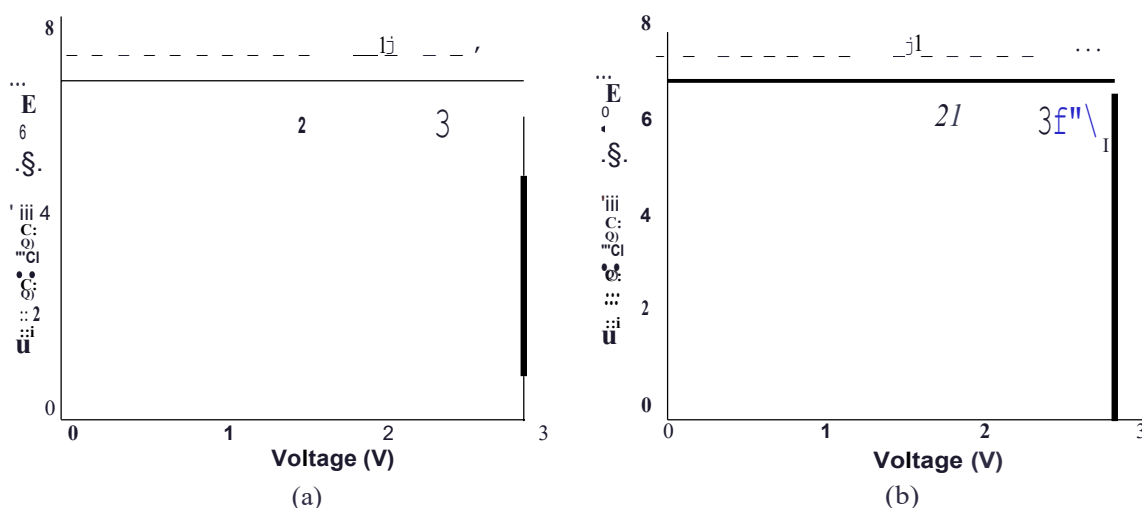


Figure 24: I - V characteristics of three different IMM cells (a) before UV exposure and (b) after UV exposure for -3,000 ESH. Curves 1 correspond to the bare cell, curves 2 correspond to the cell coated with one layer of CORIN, and curves 3 correspond to the cell coated with the SCL. The actual exposure time of the bare cell was 3,026 ESH, while the CORIN-coated cell was 3,020 ESH and SCL-coated was 3,298 ESH. During I - V measurements, the cells were illuminated by the solar simulator with an intensity of 0.875 Sun.

Table 4: Degradation rates of the η , of the UV exposed solar cells

Type of solar cell	UV degradation rate R of $41 \text{ J/cm}^2 \text{ (ESH)} \times 10^{-6}$		
	No coating	CORIN	SCL
SHJ	$-(9.9 \pm 2.1)$	No degradation	No degradation
GGS	$-(33.5 \pm 4.2)$	$-(19.7 \pm 1.8)$	$-(25.2 \pm 2.6)$
IMM	$-(8.2 \pm 1.7)$	$-(7.0 \pm 1.2)$	No degradation

• In the case of SHJ cells, "CORIN" coating meant two layers of CORIN and "SCL" coating meant one layer of CORIN and SCL on the top.

(estimated using the fitting functions in Figure 23) in Table 3, columns 5 and 6, rows 1-5. The data for the would-be-uncoated and the true uncoated cells correlated well in terms of performance degradation with time of exposure.

In summary, Figure 25 presents the chart diagram of the degradation (negative) rates of the relative efficiency change $\Delta \eta / \eta_{\text{rel}}$ of all the investigated solar cells. Thin bars near zero correspond to the cases when there was no efficiency degradation of the cells. The rates are also presented in Table 4. All the bare cells tended to degrade

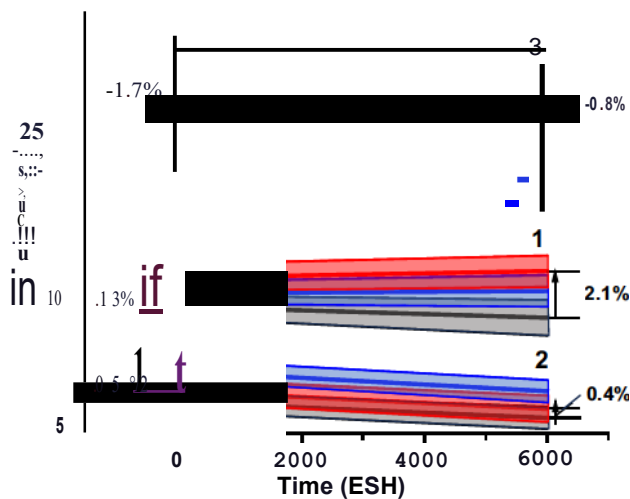


Figure 26: Evolution of the efficiency η of (1) SHJ, (2) GGS, and (3) IMM cells with the time of UV exposure. Grey bars correspond to the uncoated cells while blue bars correspond to the cells coated with CORIN (two layers of CORIN in the case of SHJ cell) and red bars correspond to the cells coated with SCL (CORIN layer and SCL on the top in the case of SHJ cell). The middle thick lines inside the bars correspond to the average efficiency. The border lines of the bars mark the statistical spreads. The graph is constructed by aggregating the data of Tables 1-3. Numerical values on both sides of the bars are equal to difference $\Delta \eta$ between the efficiency of the SCL-coated cells (η_{scl}) and the efficiency of the bare cells (η_{bare}): $\Delta \eta = \eta_{\text{scl}} - \eta_{\text{bare}}$. Vertical arrows up correspond to positive $\Delta \eta$, arrows down correspond to negative $\Delta \eta$. Due to the corrections provided by the manufacturer after the article was prepared for publication, the current density efficiency η of GGS cells must be increased 27 times.

under UV exposure. Bare IMM had the lowest degradation rate. CIGS cells, even coated, were prone to the fastest degradation probably due to UV-activated erosion of the front conductors. However, there might be a complication to account for that depends on the layer structure and composition of a particular type of CIGS. This relates to the UV/deep-blue activation or "boosting" of the front ZnO layer (s) which need UV to be sufficiently conductive (53). CORIN or SCL might slow down the erosion of the front conductor by blocking UV but increase the loss of the UV-activated front ZnO conductivity. In the case of the CIGS cells used in this study, the front layer was indium tin oxide.

The performance stabilizing effect of the SCL was observed for all the three types of cells and always beyond the statistical spread of the rate. For the SHJ and IMM cells, the SCL turned degradation into zero or slight growth. For the CIGS cell, the SCL reduced the degradation rate by -25%. For the CIGS cell, CORIN performed as a better stabilizer than the SCL.

The data in Tables 1-3, columns 4 and 6 are aggregated and presented in Figure 26 in the form of schematic evolution plots of the efficiency η of all three types of solar cells. Numbers to the left from the plots are equal to the differences $\Delta \eta_{\text{BOL}}$ between the Beginning-of-Life (BOL) efficiencies η_{BOL} and η_{bare} of the SCL-coated and bare cells, respectively: $\Delta \eta_{\text{BOL}} = \eta_{\text{BOL}} - \eta_{\text{bare}}$. Numbers to the right are equal to the difference between the End-of-Life (EOL) efficiencies (after 6,000 ESH or -1.37 years of UV exposure): $\Delta \eta_{\text{EOL}} = \eta_{\text{EOL}} - \eta_{\text{bare}}$. The best improvement over time due to SCL in terms of absolute value of efficiency was in the case of IMM cell: $\Delta \eta_{\text{BOL}}$ was -1.7% (negative due to initial deposition of SCL according to Figure 22b and the data in Table 3, column 4, rows 4 and 5) and grew up by 0.9% to $\Delta \eta_{\text{EOL}} = -0.8\%$. It could be expected that after -12,000 ESH, the efficiency will break even ($\Delta \eta_{\text{EOL}}$ will become zero), i.e., the initial efficiency loss due to SCL will be compensated by the efficiency gain over time. In the case of SHJ cell, $\Delta \eta_{\text{BOL}}$ was 1.3% and grew up by 0.8% to $\Delta \eta_{\text{EOL}} = 2.1\%$. According to Figure 13b and the data in Table 1, column 4, rows 4 and 5, $\Delta \eta_{\text{BOL}}$ would be expected to be negative due to SCL. But, as can be seen from the data in Table 1, column 4, rows 1, 4, and 5, because of the natural random variation, the efficiency of a particular uncoated SHJ cell turned out to be so high (row 4 compared to row 1) that $\Delta \eta_{\text{BOL}}$ remained positive even after SCL deposition. In the case of GGS $\Delta \eta_{\text{BOL}}$ (based on the experimental data) dropped by 0.1% with respect to $\Delta \eta_{\text{BOL}}$. In the case of IMM, the efficiency growth was slightly greater than the statistical spread (the width of the evolution bars). For the other two types, it was less or comparable to the spread.

It must be mentioned that the SCL can also potentially protect solar cells from high-energy particles (electrons and protons) in space. The study of these features will be conducted soon.

4 Conclusion

The obtained results indicated that a polymer nanocomposite SCL made of a colorless and atomic-oxygen-stabilized polyimide with the embedded NPs of an Eu-doped fluoride could improve the UV stability of the coated SHJ, CIGS, and IMM solar cells. Hypothesis testing was conducted in an environment simulating open space (exposure to the sun-like UV in vacuum and performance testing with a solar simulator using AMO filter). The UV exposure time varied from 0 to up to 7,000 ESH (corresponding to more than a year in space). All the tested solar cells are considered as good candidates for space power applications. The mechanism of converting solar UV in visible-Nm light was downshifting with -69 and -05% PLQY for the nano-JJowder and the SCL, respectively. The improvement of UV stability (in terms of reduction of the efficiency degradation rate) by the SCL was finally (beyond the statistical spread) observed for all three types of the cells. The degradation of the SHJ and IMM cells was reversed to zero or slight growth while the degradation of the CIGS decreased by -25%. Possible mechanisms of improvement included absorption and reflection of harmful solar IN, shielding UV-sensitive front conductors (as in the case of CIGS cells), and the gradual improvement of the optical coupling over time. The positive impact of the downshifted PL on PV efficiency was shaded by the loss of the incident visible solar light due to reflection and scattering from the SCL. Possible but small, positive contribution of the downshifted PL was indirectly observed in the case of the SHJ and IMM cells. To further improve the stabilizing effect and implement the increase in PV efficiency of the coated cells, the SCL will have to be set free of large-size light scattering impurities. The layer has also to be textured and antireflection-coated to minimize reflection of the incident visible solar light.

Qualitatively different behavior of each cell material visible in Figure 25 suggests that phenomenological compatibility of cell base compound and coating properties might be the most important "ingredient" of the combination; maybe each cell material has its own best coating. For instance, CORIN worked better for CIGS than SCL as a UV stabilizer but SCL was better than CORIN for SHJ and IMM. The future work will focus on the search for an optimal protective SCL coating for each type of PV cell. This will include the selection of suitable polymer base, spectrum

downshifting phosphor, composition, concentration, and layer structure.

Since most space and low-orbit vehicles (such as Elon Musk's Starlink constellation) rely on solar power, the proposed polymer nanocomposite layers that increase the operational lifetime and power efficiency of the coated solar panels have a great commercial potential.

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