

1 On-Chip Petahertz Electronics for Single-Shot Phase Detection

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14 Abstract

15 Attosecond science has demonstrated that electrons can be controlled on the sub-cycle time scale of an
16 optical waveform, paving the way towards optical frequency electronics. However, these experiments his-
17 torically relied on high-energy laser pulses and detection not suitable for microelectronic integration. For
18 practical optical frequency electronics, a system suitable for integration and capable of generating detectable
19 signals with low pulse energies is needed. While current from plasmonic nanoantenna emitters can be driven
20 at optical frequencies, low charge yields have been a significant limitation. In this work we demonstrate that
21 large-scale electrically connected plasmonic nanoantenna networks, when driven in concert, enable charge
22 yields sufficient for single-shot carrier-envelope phase detection at repetition rates exceeding tens of kilo-
23 hertz. We not only show that limitations in single-shot CEP detection techniques can be overcome, but also
24 demonstrate a flexible approach to optical frequency electronics in general, enabling future applications such
25 as high sensitivity petahertz-bandwidth electric field sampling or logic-circuits.

26 Introduction

27 When John A. Fleming developed the first widely usable vacuum diode based on the thermionic emission
28 of electrons from a tungsten filament and showed for the first time rectification of electronic AC signals, he

1 laid the foundation for modern electronics [1]. Around one hundred years later, in the pursuit of ever faster
2 electronics, a major advancement was made by utilizing carrier-envelope phase (CEP) controlled few-cycle
3 pulses to rectify electric fields at hundreds of terahertz at sharp metal tips [2]. This not only demonstrated
4 the generation of rectified, optical-frequency currents, but also demonstrated control over attosecond elec-
5 tron currents by controlling the optical pulse CEP. Subsequent investigations into these emission processes
6 revealed complex attosecond-fast dynamics [3, 4].

7 With the goal of achieving electronics operating at the frequency of optical waves, many methods have
8 been investigated of generating rectified femto- to attosecond currents directly in closed electric circuit ele-
9 ments. For example, by using sub-cycle interband transitions in dielectrics [5–8], or metallic nanoantennas
10 [9, 10]. These steps toward integrated circuits significantly reduced the experimental requirements from large
11 and bulky vacuum equipment to low-energy ambient operation. Applications exploiting the sub-cycle nature
12 of these currents have been demonstrated. Examples include attosecond-resolution electric field measure-
13 ments, CEP detection of few-cycle pulses, and petahertz logic gates [6, 8–17]. Specifically CEP detection
14 presents a great testbed for petahertz electronics, as previous methods have been fundamentally limited,
15 such as f-2f-interferometry lacking sensitivity for the absolute CEP or gas-ionization based methods, that do
16 provide absolute CEP sensitivity, but require microjoule level pulses. Resonant nanoantennas have emerged
17 as an attractive option, as they significantly reduce the energy required for field emission by optical pulses
18 and present a physical reference for the absolute CEP [9, 10, 14, 18–20]. This reduction can reach up to three
19 orders of magnitude, lowering the energy requirement to picojoule levels, while confining electron emission
20 to a well-defined hotspot at the sharp tip of the nanoantenna. Additionally, by exploiting the extreme spatial
21 confinement of nanoantennas, attosecond time-scale charge transport across nanometer-sized junctions has
22 been achieved [21].

23 While resonant nanoantennas offer several advantages, they also have limitations that impact their prac-
24 ticality. To the best of our knowledge, the electron yield from these nanoantennas has never exceeded one
25 electron per shot in CEP-sensitive yield[2, 9, 10, 14, 18]. As a result, thousands of individual laser shots must
26 be integrated to achieve a statistically significant signal, which means high-repetition-rate laser sources are
27 required. Ideally, enough current would be generated per laser shot for CEP-sensitive readout without the
28 need for averaging. Simply increasing the peak intensity of the laser pulse cannot scale the signal level of
29 these devices, as this would cause irreversible laser-induced damage. To circumvent damage the pulse en-
30 ergy can be distributed over a network of nanoantennas, which respond individually at a PHz bandwidth

1 to the optical-field, but collectively contribute their produced charge signal to the network, which is subse-
2 quently read out at radiofrequencies. However, scaling up the amount of nanoantennas in a single network
3 has been shown to present difficulties as fabrication variance couples to the detected CEP-signal and reduces
4 the overall signal strength [18]. Second, large variations of intensity across the network might exhibit CEP
5 vanishing points, that either cause a vanishing CEP signal, when the local intensity hits a waveform specific
6 resonant intensity, or even causes a π phase shift for intensities above that resonance[22].

7 In this work, we overcome these issues and demonstrate single-shot detection of CEP dependent elec-
8 trons generated by optical tunneling in a fully on-chip nanoantenna device for shot-to-shot carrier-envelope
9 phase detection. We achieve this through simultaneous excitation of hundreds of interconnected off-resonant
10 metallic nanoantennas [18]. This approach enables coherently-driven, attosecond-timescale electron emis-
11 sion across the entire detector area of $225 \mu\text{m}^2$. Moreover, by employing a custom-developed mid-infrared
12 (MIR) sub-2-cycle laser source [23] we obtain a more than tenfold increase in charge emission per individ-
13 ual antenna compared to previous results, with a CEP-sensitive charge emission as high as 3.3 electrons per
14 shot per antenna [18]. Optical pulses with longer central wavelengths have a proportionally higher electron
15 yield per individual half-cycle compared to their shorter wavelength counterparts. Additionally, the longer
16 wavelength driver excites the nanoantenna off-resonantly, which enables the full reproduction of the incident
17 electric field at the nanoantenna tip. The off-resonant excitation is crucial, as the number of optical cycles
18 dramatically influences the amount of CEP-sensitive charge produced [18]. Through this combination of
19 short-pulse excitation and scaling of the emitter area, we achieve to the best of our knowledge the highest
20 ever recorded CEP-sensitive charge yield from an integrated petahertz electronic detector and a single laser
21 shot, achieving in excess of 2300 e per laser shot at the full repetition rate of the laser system (50 kHz). The
22 energy requirements of less than 100 nJ represents a reduction of 2 to 3 orders of magnitude compared to
23 alternative gas-phase methods, while removing the need for vacuum conditions [17, 24]. Such devices en-
24 able compact, shot-to-shot CEP detection for various attosecond experiments that require CEP diagnostics
25 [25–27]. Our work more broadly demonstrates the viability of low-energy, chip-scale petahertz-electronics
26 with single-shot readout.

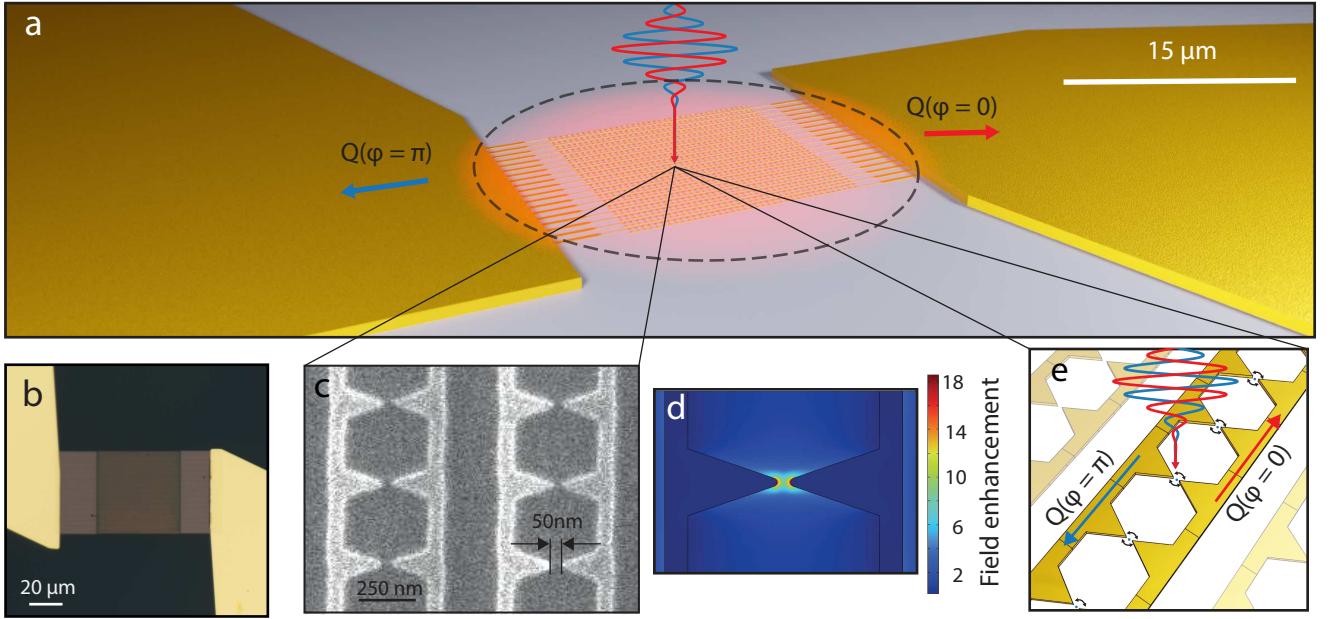


Figure 1. CEP dependent charge generation in Nanoantenna Arrays: a) Schematic of the charge generation process in the network showing two electric fields with a π CEP shift corresponding to charge generated with positive $Q(\varphi = 0)$ or negative sign $Q(\varphi = \pi)$. b) Optical microscope image of an integrated nanoantenna network contacted with gold leads. c) Scanning electron microscope image of a metallic nanoantenna array. d) Finite-element method simulation using COMSOL of the spatial field enhancement distribution of a single antenna pair. e) Schematic of the nanoscopic emission process, showing the sub-cycle electron currents generated in the antenna-vacuum junction by the driving field.

1 Results

2 0.1. Device Design

3 Our devices, as seen in Fig. 1 a, consist of 722 interconnected metallic (Au) bow-tie nanoantennas embedded
4 in a $15\text{ }\mu\text{m}$ by $15\text{ }\mu\text{m}$ network. The device is integrated into an off-chip readout circuit using conventional
5 electronics. The individual bow-tie nanoantennas, as shown in the scanning electron microscope image in
6 Fig. 1 c, have designed dimensions of 530 nm in length, 142 nm in width and 20 nm in thickness, resulting
7 in an antenna density of $3.2\text{ }\mu\text{m}^{-2}$. Fig. 1 d shows the finite element electromagnetic simulation of the field
8 distribution, showing a peak enhancement of up to ~ 18 -fold for 111 THz ($2.7\text{ }\mu\text{m}$ wavelength) localized
9 at the tips of the bow-tie structure. The sharp antenna tip creates a spatially-confined hot spot for electron
10 emission to occur. When the whole network is illuminated with a few-cycle infrared laser pulse with a
11 peak electric field on the order of 1 V nm^{-1} , highly nonlinear tunnel ionization of electrons occurs at these

1 hotspots at the tip of the bow-tie antennas. Additionally, theoretical models predict that the tunnel ionization
2 is temporally confined to the peak regions of the strongest half-cycles of the exciting field[3, 4, 14, 21, 22,
3 28–30].

4 *0.2. Theoretical Model*

5 In the case of sufficiently strong electric fields, with a Keldysh parameter $\gamma \ll 1$ the tunneling emission for
6 a metal-vacuum boundary is described by the quasi-static Fowler-Nordheim tunneling current $\Gamma_{FN}(E) =$
7 $\theta(E)\alpha E^2 \exp\left(-\frac{f_t}{|E|}\right)$ [28–31], with $\theta(E)$ noting the Heaviside function, $f_t = 78.7 \text{ V nm}^{-1}$ the characteristic
8 tunneling field strength for gold and α a material and geometry dependent scaling factor. Since a single bow-
9 tie is, in fact, a symmetric system consisting of two metal surfaces facing each other with a 50 nm vacuum
10 gap, we can approximate the total instantaneous currents at the junction with $\Gamma(E) = \Gamma_{FN}(E) - \Gamma_{FN}(-E)$,
11 as experimentally shown in [9, 18, 21]. A CW laser would lead to fully symmetric charge injection and
12 transport across the gap. In such a case, the time average of the residual charge in the network is zero.
13 However, for the case of a few- to single-cycle pulse, the highly nonlinear dependence of the tunnelling
14 current with respect to the electric field amplitude does result in a residual net charge. The residual net
15 charge is caused by the significant amplitude differences between the individual half-cycles of the pulse,
16 effectively breaking the symmetry of emission and transport [9]. To understand the symmetry breaking,
17 it is useful to look at the detailed instantaneous tunneling rates as a function of the electric fields for a
18 metal-vacuum boundary.

19 The instantaneous current response of this nanoantenna configuration, shown in Fig. 2a, is equivalent to
20 the response of two parallel diodes in opposing directions. The quantitative current response is adapted from
21 [32, 33] and considers the frequency resolved field enhancement, while also averaging over the antenna tip
22 surface area of 628 nm^2 , resulting in an effective field enhancement of 8.2 for the considered excitation field.
23 When calculating the instantaneous currents of the nanoantenna, the local field at the tip of the nanoantenna
24 is relevant. Therefore, we need to consider the antenna's complex transfer function [14]. The antenna is
25 designed to have a resonance wavelength of 1500 nm and be off-resonant with the exciting field centered at
26 $2.7 \mu\text{m}$ for two main reasons; the first is to transfer the full bandwidth of the optical pulse to the antenna tip,
27 as a sharp resonance would increase the local pulse duration and reduce the CEP-dependent charge yield
28 drastically. The second reason is that the fabrication process is not fully uniform throughout the detector
29 area, resulting in small spectral shifts of the antenna resonance [18]. When designed on-resonance, small

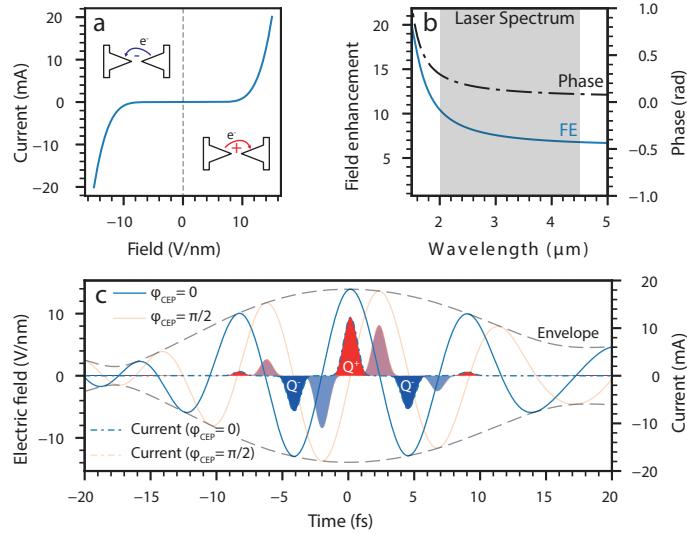


Figure 2. Theoretical description of the antenna gap currents: a, Effective instantaneous tunneling rate for two opposing gold surfaces in the nanoantenna junction, assuming scaling parameters from [32] with an effective emission area of 628 nm^2 . b, The response function of the local electric field at the tip of the nanoantenna to an exciting electric field simulated using a FEM electromagnetic solver. The simulation shows the wavelength-dependent field enhancement and phase. The effective field-enhancement of the incident pulse is ~ 8.2 . c, The electric field as a function of time and the calculated instantaneous current as a function of the electric field for a CEP of $\varphi = 0, \pi/2$. The electric field is the calculated local antenna field using the characterized optical pulse and the simulated antenna response (see Supplementary Sec. S2 and S3.1). The solid lines note the electric field and the dashed lines the current. The shaded areas underneath the current curves show the total charge yield, with red areas contributing positively and blue areas contributing negatively.

1 variations will result in large phase differences between individual antennas, as the phase response has a
 2 steep slope at resonance. Considering the collective phase response of all antennas, variations in individual
 3 phases will reduce the collective CEP response of the detector [18]. Therefore, when the antennas are driven
 4 off-resonance, small variations in the fabrication will not translate into large phase changes of the optical
 5 field at the antenna tip. Additionally, a reduced variance of the device-induced phase shift is critical to
 6 improved precision in measuring the absolute CEP value. Any well known phase offset induced by the
 7 antenna can simply be removed from the detected phase. The local field enhancement and the phase response
 8 of an off-resonance antenna for wavelengths above $2 \mu\text{m}$ is shown in Fig. 2 b. The local field at the antenna tip
 9 E_{loc} is therefore the frequency domain multiplication of the incident pulse $\tilde{E}(\omega)$ and the antennas complex
 10 frequency response $\tilde{H}(\omega)$, $E_{\text{loc}}(t) = \mathcal{F}^{-1}\{\tilde{E}(\omega) \cdot \tilde{H}(\omega)\}$. The calculated instantaneous current response of

1 the system to such a pulse with a peak field of $\sim 13 \text{ V nm}^{-1}$ is shown in Fig. 2c. The employed optical pulse
 2 shape is the reconstructed optical pulse used in the experimental apparatus, combined with the simulated
 3 local field enhancement (see Supplementary Sec. 2 and Sec 3.1 for details). This implies that the central half-
 4 cycle with the highest field amplitudes generates the largest peak current with up to 12 mA for a duration
 5 of 1.1 fs (FWHM). The neighboring half-cycles generate substantially smaller currents with the opposite
 6 sign. Since conventional electronics do not support the petahertz bandwidth currents, the device acts as
 7 an integrator, and the net charge deposited by the optical pulse resides in the circuit network, similar to a
 8 photodiode. The mathematical description of these charges Q as a function of the pulse CEP φ is simply the
 9 integral over the instantaneous currents;

$$Q(\varphi) = \int_{-\infty}^{\infty} \Gamma(A(t) \cdot \cos(\omega_0 t + \varphi)) dt \quad (1)$$

$$= \underbrace{\int_{-\infty}^{\infty} \Gamma_{FN}(A(t) \cdot \cos(\omega_0 t + \varphi)) dt}_{:= Q^+(\varphi)} - \underbrace{\int_{-\infty}^{\infty} \Gamma_{FN}(-A(t) \cdot \cos(\omega_0 t + \varphi)) dt}_{:= Q^-(\varphi)} \quad (2)$$

$$= Q^+(\varphi) - Q^-(\varphi). \quad (3)$$

10 The CEP dependence of the charge now stems from the small difference of $Q^+(\varphi)$ and $Q^-(\varphi)$. For the
 11 case of a cosine pulse ($\varphi = 0$) the charge yield becomes maximal, and for the case of a sine pulse ($\varphi = \pi/2$)
 12 the charge components cancel out to zero. Based on the results shown in [18] with 0.1 e per antenna, one
 13 can anticipate CEP-dependent charge amplitudes of around 1.4 e per antenna for the optical pulses used in
 14 our experiments and a peak field of 1.7 V nm^{-1} . The resulting charge increase is due to a reduced number
 15 of cycles (from 2.5 to 2), and the use of a longer central wavelength [32]. With the known charge yield
 16 per antenna, one can extrapolate the charge yield of an array of interconnected antennas to a charge that is
 17 within the reach of reasonable detection limits.

18 *0.3. Experiment*

19 The optical pulses used in this work were generated with a home-built laser source based on optical para-
 20 metric amplification and difference frequency generation that delivers passively CEP stable pulses with a
 21 FWHM duration down to 16 fs at a center wavelength of $2.7 \mu\text{m}$. The pulse energy was $> 84 \text{ nJ}$ at a repetition
 22 rate of 50 kHz. The CEP of the laser was controlled by adjusting the pump-seed delay in the difference fre-

1 quency generation stage. The delay adjustment was implemented by controlling the pump beam path length
2 via a retro-reflector mounted on a piezo-actuated linear stage. For a detailed description of the source, see
3 the methods section A and Ref. [23].

4 To illuminate the nanoantenna network, we focused the incident pulse down to $\sim 21 \mu\text{m}$ (FWHM) with an
5 off-axis parabola of focal length 25.4 mm. The nanoantenna arrays were placed in the center of the focus. To
6 achieve single-shot charge readout, we used a custom transimpedance amplifier with a gain of 1 GVA^{-1} and
7 a -3 dB -bandwidth of 50 kHz (WiredSense GmbH). The RMS noise floor of our detection was measured
8 to be $\sim 1100 \text{ e}$ per shot. To overcome this noise, we illuminated a network consisting of 722 antennas in a
9 rectangular area of $15 \mu\text{m}$ by $15 \mu\text{m}$ to generate in excess of 1000 e per shot.

10 After interaction with the nanoantenna arrays, pulse energies were measured by a pyroelectric photodetec-
11 tor with the same -3 dB -bandwidth of 50 kHz as the transimpedance amplifier. This arrangement allowed
12 for the simultaneous recording of shot-to-shot pulse energy fluctuations. The pyroelectric detector uses
13 an identical transimpedance amplifier to the one used for the nanoantenna read-out to ensure comparable
14 statistics of the two signals. More details on the acquisition and digitization of the signal are given in the
15 Supplementary Information Sec. 3.1.

16 In this experiment, each dataset consisted of the measured charge from the nannoantenna array and the
17 corresponding pulse energy, recorded for around 50 000 shots (1 s). In each dataset, the CEP of the laser
18 was linearly ramped for 600 ms with a speed of $20 \pi \text{ rad s}^{-1}$, starting at $\sim 120 \text{ ms}$. For different datasets, the
19 pulse energy was systematically varied by more than a factor of ten.

20 A single dataset is presented in Fig. 3, including both the single-shot data and the moving average calcu-
21 lated over 150 shots (dark line). The upper panel shows the recorded charge produced by the nanoantenna
22 array, with an average yield of 25 000 e per shot. From 120 ms to 720 ms the CEP is linearly ramped over
23 a 12π range. The data points show a clear sinusoidal CEP dependence with an amplitude of 2370 e and a
24 signal-to-noise ratio (SNR) of 4.6, while the pulse energy does not show modulation. Additionally, we esti-
25 mated the CEP noise of our measurement to be 0.75 rad rms (see supplementary Sec. 4.4 for the details of
26 the estimation). When considering the number of illuminated antennas, the individual CEP-sensitive yield
27 per antenna and shot is 3.3 e, we estimated peak currents through the nanoantenna gap of up to a 95 e/fs,
28 corresponding to $\sim 15 \text{ mA}$. Given the surface area of a single nanoantenna tip, $\sim 628 \text{ nm}^2$, the estimated
29 current density reaches a remarkable 2.4 GA cm^{-2} . At $t = 370 \text{ ms}$ and 620 ms , sharp changes are visible in
30 the charge yield of the detector element. These features, which are 250 ms apart, are caused by the specific

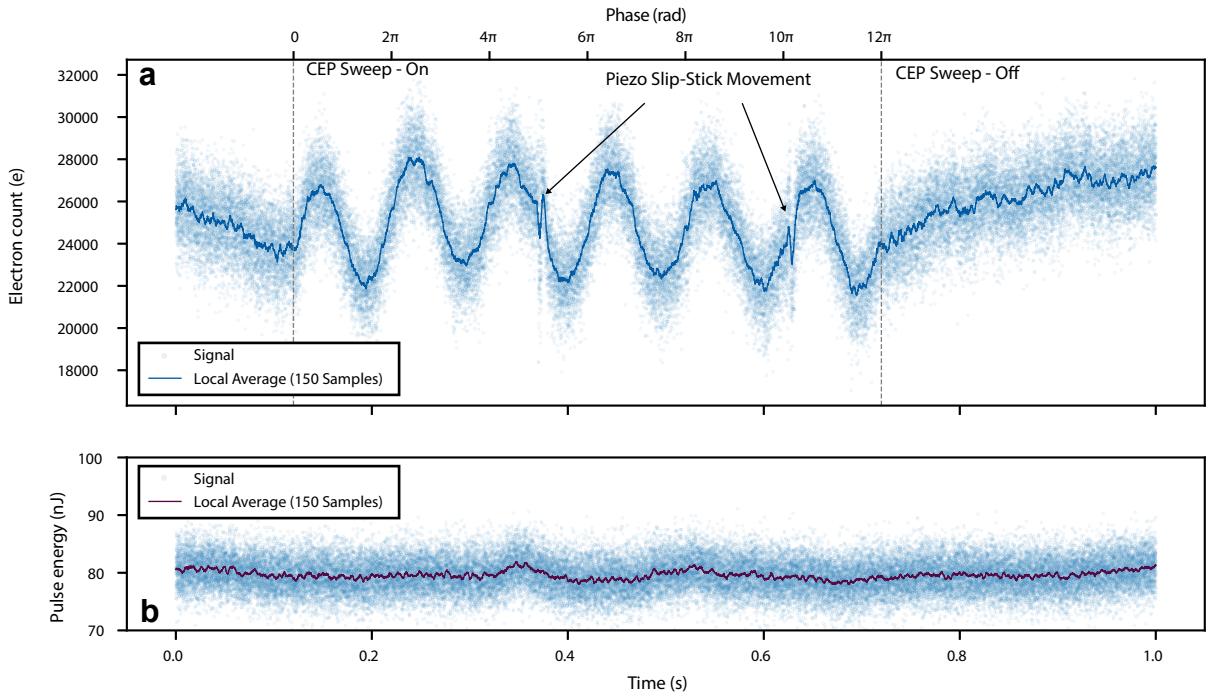


Figure 3. Single-shot charge readout: single dataset recording of 50 000 laser shots for the charge yield of the nanoantenna detector (upper panel a) and the laser energy recorded by the pyroelectric detector (bottom panel b). The peak field of the incident laser pulse on the array is 1.6 V nm. From 120 ms to 720 ms the CEP was linearly ramped over 6 cycles. The instantaneous phase was interpolated with the scan speed of $2\pi\text{s}^{-1}$.

1 movement pattern of the closed-loop slip-stick piezo stage used to control the CEP, that recenters the piezo
 2 position every 1.3 μm .
 3 To isolate the CEP-dependent signal from readout noise and pulse energy fluctuations, we Fourier trans-
 4 formed the dataset between $t = 120$ ms and $t = 620$ ms and compared it to the frequency spectrum obtained
 5 without any optical input; see Fig. 4. The spectrum of the antenna array shows a clear peak at 10 Hz corre-
 6 sponding to the $2\pi \cdot 10$ Hz modulation of the CEP. This signal amplitude is around two orders of magnitude
 7 (40 dB) higher than the readout noise floor. The noise in the measured spectrum is dominated from DC to
 8 ~ 250 Hz by $f^{-3/4}$ scaling, which is typical for field emission devices and is attributed to Brownian noise
 9 of the work function due to dynamical changes of adsorbates on the surface [18, 34]. At frequencies higher
 10 than 250 Hz the spectrum is limited by shot noise, with a substantial component originating from the de-
 11 tection noise of the transimpedance amplifier. The calculated shot noise of the signal is ~ 160 e rms. We
 12 also want to note, that we did not observe noticeable degradation of the devices, in comparison to studies

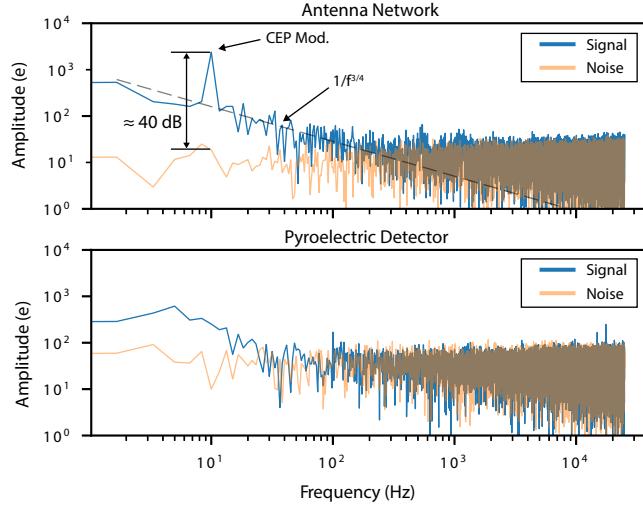


Figure 4. Frequency Domain of the single-shot data: The respective data from Fig. 3 $t = 370$ ms to $t = 620$ ms is Fourier transformed and shown in charge amplitude as a function of frequency. For comparison, the electronic noise floor is shown in orange for both spectra. a) the frequency-resolved signal of the nanoantenna network. The 10 Hz CEP modulation is separated by 40 dB from the noise floor. b) the frequency-resolved pulse energy fluctuation, detected with the pyroelectric detector.

1 using oscillator type laser sources with MHz-level repetition-rates, where degradation was present on the
 2 few minute time scale[18]. However, detailed studies of durability and lifetime are certainly warranted, as
 3 has been carried out at DC field emission with comparable devices over 2500 hours [35]. When evaluating
 4 the recorded pulse energy fluctuations at the photodetector, no 10 Hz modulation is distinguishable from
 5 the background (see Fig. 4 b). Above 100 Hz the pulse energy spectrum is dominated by detector noise.
 6 Systematic investigation of signal strength as a function of peak electric field has shown that at ~ 1 Hz res-
 7 olution bandwidth a signal distinguishable from noise can be observed down to 0.6 V nm^{-1} (corresponding
 8 to $\sim 10 \text{ nJ}$). See Supplementary Sec. 4.1 for details.

9 Discussion

10 We have demonstrated single-shot readout of CEP-dependent charge signals at 50 kHz repetition rate, under-
 11 lying sub-cycle current generation across a macroscopic device area of $225 \mu\text{m}^2$ integrating more than 700
 12 individual antenna pairs. This was made possible by improving the average CEP-dependent charge yield per
 13 single antenna by a factor of ~ 30 [18, 21], now reaching 3.3 e per shot, and by illuminating hundreds of
 14 antennas simultaneously. The enhanced antenna yield implies a remarkable peak current density estimated

1 to reach up to 2.4 GA cm^{-2} [9, 18, 21]. With this result, we show that metallic nanoantenna networks, fab-
2 ricated via state-of-the-art lithographic methods, are a flexible and scalable approach to optical-frequency
3 electronics that allows the designing of individual circuit elements, similar to conventional microelectronics.
4 Thanks to this advance, we demonstrated off-resonant antennas that are sensitive to pulse energies two or-
5 ders of magnitude lower than any other photemission-based single-shot absolute CEP detection techniques
6 [17, 24, 36] and comparable to or lower than f-2f interferometry [37], enabling absolute CEP detection
7 of optical pulses with only tens of nanojoules of energy. Further optimization of the network density (see
8 supplementary Sec. S2) combined with a reduced number of optical cycles in the pulse would potentially
9 increase the total yield by an additional two orders of magnitude [18, 32]. As the measurement is domi-
10 nated by read-out noise, further noise reduction of electronics downstream of the detector element will have
11 a significant impact on SNR with potential for another 5- to 10-fold improvement[38]. It is generally ex-
12 pected that when using optimised detector circuits the SNR will also be dictated by the performance of the
13 transimpedance amplifier. Transimpedance amplifiers generally provide less noise and higher gain at lower
14 bandwidth operation typically resulting in higher SNR when using lower repetition rate laser sources. In
15 contrast, when using higher repetition rates laser sources the transimpedance amplifier will exhibit higher
16 noise levels and reduced gain, reducing the SNR. Additionally, very high repetition rates may also lead
17 to increased heat load on the devices requiring a reduced pulse energy to avoid damage which limits the
18 overall single-shot SNR performance. With these improvements and technical optimisations the measured
19 phase noise of 0.75 rad will be lowered down to tens of milliradians and soon competitive with established
20 techniques, but integrated fully on a chip and with a compact detector footprint.

21 Given the exceptional current densities generated in these nanometer-sized devices, further studies will be
22 necessary to elucidate the role of electron-electron interaction during the sub-cycle emission process [39].
23 Based on this platform, many different experiments and applications can be developed either based on single
24 nanoantennas or larger network structures. Specifically single antennas are interesting for the investigation
25 of petahertz-bandwidth logic gates and memory cells [11, 12]. For network structures, the small device
26 size, comparable to the pixel size in modern Si-based CMOS detectors, combined with the reduced pulse
27 energy requirements, enables the integration of multiple nanoantenna arrays in a larger pixel matrix. This
28 will allow for a CEP-sensitive camera with further improved noise performance [40]. Absolute single-shot
29 CEP tagging can also be implemented by adapting I/Q detection with two separate networks recording $\pi/2$
30 phase-shifted currents. The previously demonstrated techniques of attosecond-resolved field sampling can

1 be extended to single-shot readout, by making large line arrays of individual networks [14, 41]. Another area
2 of progress will be the adaptation of the fabrication process to become fully CMOS-compatible by replacing
3 gold with aluminum or copper.

4 More broadly, pushing the boundaries in petahertz electronics will require future investigations of new
5 device classes such as transistors and logic circuits and also new material platforms. With our results we
6 illustrate a path towards scalable and directly applicable petahertz electronics.

7 **A. Methods**

8 *Laser source*

9 The two-cycle MIR source used to illuminate the nanoantenna networks is a home-built system based on
10 adiabatic difference frequency generation (DFG) [42] and details can be found in [23]. The setup is based
11 on a commercial Yb:KYW regenerative amplifier with a center wavelength of 1.03 μm , a pulse duration of
12 425 fs, delivering up to 120 μJ at a repetition rate of 50 kHz. The first stage of the optical setup consists of
13 a non-collinear optical parametric amplifier seeded with white light and pumped by the second harmonic
14 of the pump laser [43]. The amplified seed has an energy of approximately 1.8 μJ at a center wavelength
15 of 740 nm. After the amplification, the seed is stretched for pre-compensation of the later acquired MIR
16 dispersion, and the pulse energy is controlled by an anti-reflection-coated metallic neutral-density-filter
17 wheel. For generation of the passively CEP stable DFG output in the MIR, the amplified seed and the
18 stretched pump laser of $\sim 10\text{ps}$ propagate collinear through an adiabatically poled Mg:LiNbO₃ crystal with
19 an identical design to Krogen et al. [42]. The generated broadband MIR pulse covers the spectral range of
20 2 μm to 4.5 μm at an energy of up to 84 nJ and is compressed through dispersion in BaF₂ and silicon. The
21 generated pulse has a duration down to 16 fs (FWHM) at a center wavelength of 2.7 μm , characterized by a
22 two-dimensional spectral shearing interferometry setup. The passive CEP stability of the MIR pulse inherent
23 to the difference frequency generation process is measured with an f-2f interferometer to 190 mrad rms over
24 15 min.

25 *Nanofabrication*

26 A fused silica wafer was purchased from MTI Corporation and cut with a die saw. The substrates were
27 cleaned by sonicating in acetone and isopropyl alcohol for 5 minutes each. Subsequently, the pieces were
28 cleaned using an oxygen plasma. Poly(methyl methacrylate) A2 was spun at 2,500 revolutions per minute

1 and baked at 180 °C, then DisCharge H2O (DisChem Inc.) was spun at 1,000 revolutions per minute so that
2 charging did not occur during the electron beam lithography write.

3 Electron beam lithography was performed using an electron-beam energy of 125 keV with doses varying
4 from 4000-6000 $\mu\text{C cm}^{-2}$ with an applied proximity effect correction. After exposure, the resist was devel-
5 oped in a 3:1 isopropyl alcohol/methyl isobutyl ketone solution for 50 seconds at 0 °C. Subsequently, the
6 antenna deposition was performed using an electron beam evaporator operating below $9 \cdot 10^{-7}$ Torr. First,
7 a 2 nm adhesion layer was deposited, then 20 nm of gold. Lift-off was performed in a 65 °C-70 °C bath of
8 N-methylpyrrolidone.

9 After antenna fabrication, contacts were patterned by photolithography using a bilayer of PMGI and
10 S1838 both spun at 4,500 revolutions per minute. The deposition was performed by electron beam evapora-
11 tion with a 40 nm adhesion layer and 160 nm of gold so that they could be wire-bonded to a printed circuit
12 board.

13 **A. Extended Data Figures**

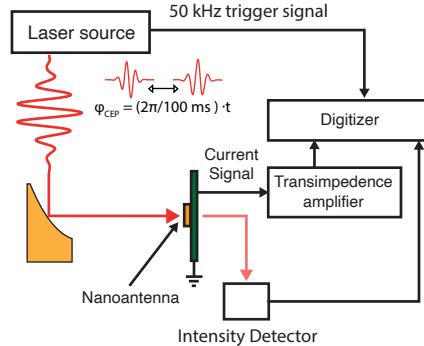


Figure 5. Experimental setup: The experimental setup consists out of a home-built laser source, delivering 18 fs pulses at a center wavelength of 2.7 μm with up to 84 nJ of energy at a repetition-rate of 50 kHz, a 25.4 mm focal length off-axis parabola and the nanoantenna detector element at the focal spot. For detection of the charge signal, we use a custom transimpedance amplifier with a gain of 1 GV A^{-1} and a -3 dB -bandwidth of 50 kHz. For detection of the single shot intensity signal of the laser pulse, we use a 50 kHz bandwidth pyroelectric detector in transmission after the detector. The charge and the intensity signals are digitized with an 8-bit oscilloscope at a sampling rate of 20 MSa/s. To retrieve the individual single-shot events, the digitized pulses are integrated and sorted based on the timing signal of the 50 kHz trigger signal provided by the laser source. To produce a CEP-dependent signal, the CEP of the laser source is linearly swept at a rate of $2\pi/100 \text{ ms}$ for 600 ms.

¹ **Data Availability**

² The measurement data generated in this study have been deposited in the [figshare](#) database under accession
³ code 10.6084/m9.figshare.25114634.v2 [Link](#).

⁴ **Code Availability**

⁵ The code to process the data and to prepare the data plots of the main-text and the supplementary information
⁶ is available in form of Python jupyter notebook at [github](#).

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³ Author Contributions

⁴ FR, MY, FK and PK conceived the experiments. The samples were fabricated by MY with guidance from
⁵ PK and KB. The experimental setup was constructed by FR with assistance from EB, GR, RM, and HC. The
⁶ readout electronics were set up by FR, TG, MB and TM. The data was taken by FR. The data was analyzed
⁷ by FR with input from MY and PK. The electromagnetic simulations were done by EB with input from FR,
⁸ MY and PK. The manuscript was written by FR with significant contributions from MY, PK, GR and editing
⁹ from all authors.

¹⁰ Competing Interests

¹¹ The authors declare no conflict of interest.

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