

Solitary waves and kinks in FPU lattices with soft-hard-soft trilinear interactions

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Abstract

We consider a version of the classical Hamiltonian Fermi-Pasta-Ulam (FPU) problem with a trilinear force-strain relation of soft-hard-soft type that is in general non-symmetric. In addition to the classical spatially localized solitary waves, such hardening-softening model also exhibits supersonic kinks and finite-amplitude, spatially delocalized flat-top solitary waves that acquire the structure of a kink-antikink bundle when their velocity approaches the kink limit. Exploiting the fact that traveling waves are periodic modulo shift by a lattice spacing, we compute these solutions as fixed points of the corresponding nonlinear map and investigate how their properties depend on the parameter measuring the asymmetry of the problem. In a particularly interesting case when one of the soft regimes has zero elastic modulus, we obtain explicit solutions for sufficiently slow solitary waves. In contrast to conventional delocalization in the sonic limit, the corresponding compact structures mounted on a constant background become localized at the lattice scale as their velocity tends to zero. Numerical simulations of Riemann-type initial value problem in this degenerate limit show the emergence of Whitham shocks that involve periodic trains of solitary waves. We investigate stability of the obtained solutions using direct numerical simulations and Floquet analysis. We also obtain explicit solutions for a quasicontinuum model that captures the most important features of the discrete problem.

1 Introduction

Pulse-shaped solitary waves constitute an important class of traveling waves in nonlinear systems. These localized dynamic coherent structures emerge in discrete and continuum mechanical systems due to the interplay of dispersion and nonlinearity. Stable solitary waves play an important role as building blocks in developing dynamical patterns in various nonlinear mechanical systems, ranging from granular crystals to metamaterials. They are increasingly used in applications exploiting structural nonlinearities at the scale of the periodicity cell [Yasuda et al., 2020, Raney et al., 2016, Kochmann and Bertoldi, 2017, Zhang et al., 2019]. Artificially created materials of this type can now manipulate localized mechanical signals, and the ensuing control of solitary waves is used for mechanical energy transmission, encryption of mechanical information and even activation of mechanical robots [Bertoldi et al., 2017, Yasuda et al., 2019].

Solitary waves in discrete mechanical systems and their continuum KdV-type approximations were first discovered in the pioneering work by Zabusky and Kruskal [1965] that explained the seemingly paradoxical results of the numerical investigations by Fermi et al. [1955] of the nonintegrable

Hamiltonian Fermi-Pasta-Ulam (FPU) lattice, a mass-spring chain with nonlinear nearest-neighbor interactions [Berman and Izrailev, 2005, Gallavotti, 2007]. In subsequent studies solitary waves emerged as localized, non-topological and non-dissipative coherent structures that move with supersonic speeds and form continuous families [Remoissenet, 2013, Newell, 1985, Fokas and Zakharov, 2012, Vainchtein, 2022, Ablowitz, 2011]. The most well studied case of solitary waves in discrete FPU system is when the springs are characterized by force-strain relation of either hardening or softening type, as for instance in the case of α -FPU system with quadratic nonlinearity. While weak solitary waves in such systems can be characterized as low-amplitude, completely delocalized and almost linear waves, very strong solitary waves emerge as maximally localized, lattice-scale anticontinuum mechanical signals. The most analytically transparent setting in this class of problems is the *bilinear*, soft-hard model introduced already in the original FPU study [Fermi et al., 1955]. In the present paper we consider a *trilinear*, soft-hard-soft, generalization of this classical model. Using exact solutions available in this case we show that, even without compromising the convexity of the energy, the resulting hardening-softening system can exhibit non-classical physical effects.

Specifically, we consider the prototypical discrete FPU chain whose mechanical response is represented by three linear elastic regimes which we characterize as soft, hard and again soft. This implies that the conventional hardening soft-hard response is eventually taken over by a softening hard-soft regime. No symmetry is assumed regarding the two soft regimes which in high-contrast limit would be characterized by drastically different elastic moduli. Our goal is to take advantage of the fact that the addition of the second soft regime leads to the emergence in such FPU system of rather peculiar delocalized finite-amplitude flat-top solitary wave solutions, which are intimately connected to the nontopological supersonic kink solutions. Due to the piecewise linear nature of the problem, both kinks and solitary waves can be studied analytically in a quasicontinuum approximation of the discrete system.

The choice of soft-hard-soft interactions is inspired by stress-strain laws in a range of soft biological tissues from skin to muscles [Yasenchuk et al., 2021]. For instance, in tendons and ligaments the hardening stage of the mechanical response can be linked to the straightening of crimped collagen fibers, while the softening stage may be due to the beginning of the distributed microscopic fracturing of these fibers [Yasenchuk et al., 2021, Sensini and Cristofolini, 2018]. Hardening to softening transition is also ubiquitous in elastomeric molecular composites [Millereau et al., 2018] and is sometimes mimicked in NiTi mesh implants [Yasenchuk et al., 2021].

The question of existence of traveling waves in a hardening-softening FPU system has been already addressed in the literature [Iooss, 2000, Herrmann and Rademacher, 2010, Herrmann, 2011, Gorbushin and Truskinovsky, 2019]. Two recent papers discussed the relation between solitary waves and nontopological kinks in such systems. In one of them [Gorbushin and Truskinovsky, 2021] the force-elongation relation was taken in a bilinear, soft-soft form with a degenerate infinitely hard response in between. In the other [Vainchtein and Truskinovsky, 2024] the mechanical response was chosen to be cubic with symmetric softening and hardening regimes. Both models produced a coherent description of the families of solitary waves that in a special velocity limit feature formation of supersonic kinks, or superkinks [Vainchtein and Truskinovsky, 2024, Gorbushin et al., 2022]. As this limit is approached, the waves increase in width and acquire a flat-top finite-amplitude structure of a kink-antikink bundle.

However, the emerging picture remains incomplete. Thus, the fact that the bilinear model replaced the hard section of the constitutive response by an infinitely hard one did not leave any space for the internal degrees of freedom governing the energy transfer inside the core regions of both solitary waves and superkinks. In particular, this resulted in an unrealistic prediction that such solutions may propagate with arbitrarily large speeds. In addition, to enable a simple solution procedure based on the Fourier transform, the two soft regions in the bilinear model considered

by Gorbushin and Truskinovsky [2021] were taken to be fully symmetric. For the same reason of analytical simplicity the cubic model studied by Vainchtein and Truskinovsky [2024] was also chosen to be overly symmetric, which made the repertoire of possible physical effects somewhat limited while also concealing some interesting special cases such as the high-contrast case when one of the two soft regimes has zero sound speed (a “sonic vacuum” [Vainchtein, 2022]). Of course, the important advantage of the constitutive choices made by Gorbushin and Truskinovsky [2021] and Vainchtein and Truskinovsky [2024] was that in the cubic case a quasicontinuum (QC) approximation of the discrete FPU problem yielded explicit solutions, while in the bilinear case analytical solutions could be found for both discrete and QC problems.

To complement the existing studies, we present in this paper the still missing discussion of the non-symmetric trilinear case. First, it allows us to study the case of radically different soft regimes including the limit when one of them becomes elastically degenerate. Such limit, which resembles granular response, is of interest as the model becomes non-linearizable in the corresponding strain range, and nonlinearity becomes essential. In particular, due to such degeneracy the linear waves disappear, while the conventional dispersive shock waves are replaced by Whitham shocks involving trains of compact solitary waves. The second advantage of the trilinear model is the possibility of opening up the core region of both solitary waves and kinks which is then described by a separate degree of freedom that can have its own evolution. This allows one to study interaction between the different parts of the traveling wave and results in a realistic finite velocity limit for its propagation.

We start by considering a QC approximation [Collins, 1981, Rosenau, 1986, Kevrekidis et al., 2002, Feng et al., 2004] of the discrete FPU model for which all of these effects can be demonstrated using explicit traveling wave solutions in the form of kinks and solitary waves. In particular, we show that asymmetry of the problem, measured by the non-unit ratio of the elastic moduli in the soft regimes, has a significant effect on the velocity ranges of the existence of kink solutions, as well as the values and asymptotic behavior of their limiting strains as functions of the velocity. This, in turn, affects the limiting amplitudes and velocity ranges of the associated solitary waves. We also discuss the asymptotic behavior of the obtained solutions near the boundaries of the velocity interval. In particular, we show that in the case when one of the soft regimes has zero modulus, the compressive solitary waves have a nontrivial sonic limit.

We then follow the approach of Aubry and Proville [2009], Vainchtein et al. [2020], James [2021] and Vainchtein and Truskinovsky [2024] and take advantage of the fact that traveling wave solutions of the discrete problem are periodic modulo shift by one lattice spacing to obtain such solutions of the discrete problem as fixed points of a nonlinear map. While this procedure generally requires numerical iterations, in the important case when one of the soft regimes becomes degenerate, sufficiently slow discrete solitary waves can be also computed analytically. This allows us to corroborate our numerical procedure and reveal the compact (modulo constant background) nature of the solutions in this limiting case, which is not captured by the QC model. Further comparison with traveling wave solutions of the discrete problem shows that while the QC model captures them qualitatively, the quantitative agreement is fairly good for superkinks but exists primarily near sonic and kink velocity limits for solitary waves. The discrepancy between the solutions away from these limits depends on the nature of the wave (compressive or tensile) and the value of the asymmetry parameter.

Floquet analysis of the linear stability of obtained solitary waves in the non-degenerate cases, which is enabled by their periodicity-modulo-shift [Vainchtein et al., 2020, Cuevas-Maraver et al., 2017, Xu et al., 2018] and takes advantage of the piecewise linear nature of problem, shows that near-sonic solutions with velocity below a certain threshold are unstable. Numerical simulations initiated by the unstable waves perturbed along the corresponding eigenmode show that the instability unfolds through the system approaching an apparently stable wave above the threshold. Effective

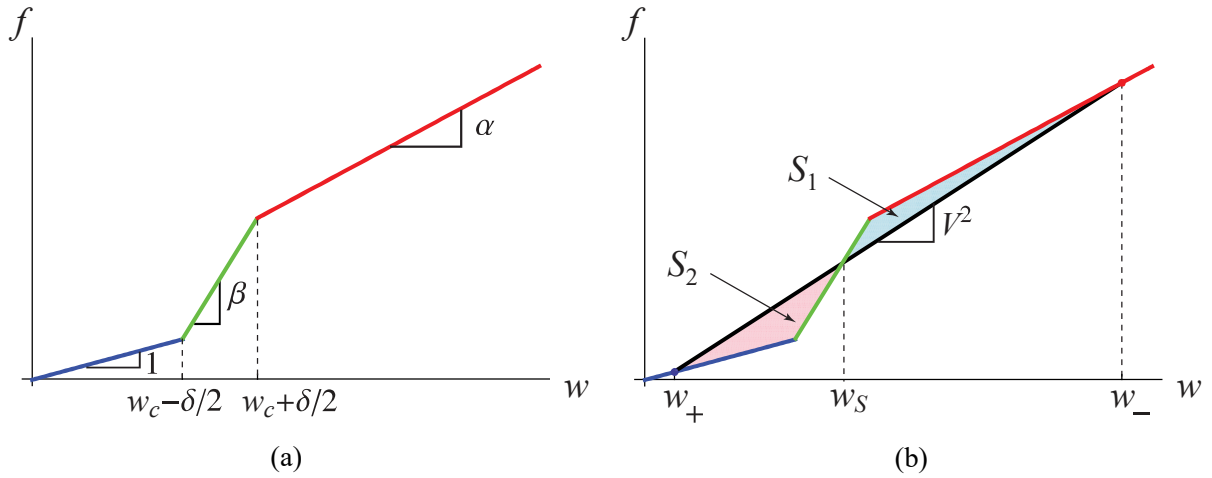


Figure 1: (a) Trilinear soft-hard-soft interaction force $f(w)$ with slopes 1, β and α along the blue (soft), green (hard) and red (soft) segments, respectively; (b) Rayleigh line connecting $(w_+, f(w_+))$ and $(w_-, f(w_-))$ (black) for a superkink transition wave with limiting states w_{\pm} and supersonic velocity V satisfying $\max\{1, \alpha\} < V^2 < \beta$. The two shaded areas cut by the Rayleigh line at $w = w_S$ are equal: $S_1 = S_2$ (see the text for details).

stability of such waves above the threshold is confirmed by direct numerical simulations, which also show robust propagation of superkinks and solitary waves in the degenerate case at the prescribed velocities. This is further corroborated by the Riemann-type simulations with piecewise-constant initial data, which also reveal other interesting phenomena, such as formation of Whitham shocks involving periodic trains of solitary waves in the degenerate case.

The paper is organized as follows. In Sec. 2 we formulate the problem and discuss the general properties of the two types of traveling waves. Explicit solutions for the QC model are constructed and discussed in Sec. 3. In Sec. 4 we describe the procedure for computing traveling wave solutions of the discrete problem, derive explicit solutions for sufficiently slow compressive waves in the degenerate case, and compare the obtained solutions with their QC counterparts. Stability of kinks and solitary waves is discussed in Sec. 5 and Sec. 6, respectively. Concluding remarks can be found in Sec. 7. Some technical results are contained in Appendix A.

2 Problem formulation

Consider a one-dimensional chain of identical masses interacting with their nearest neighbors. The dimensionless governing equations are

$$\ddot{u}_n = f(u_{n+1} - u_n) - f(u_n - u_{n-1}), \quad (1)$$

where $u_n(t)$ is the displacement of n th particle at time t , $\ddot{u}_n(t) = u_n''(t)$, and $f(w)$ is the nonlinear interaction force associated with the interaction potential $\Phi(w) = \int_0^w f(s)ds$. Introducing the strain variables $w_n = u_n - u_{n-1}$, we can rewrite (1) in the form

$$\ddot{w}_n = f(w_{n+1}) - 2f(w_n) + f(w_{n-1}). \quad (2)$$

Our main assumption concerns the choice of the particle interactions in the trilinear soft-hard-soft form:

$$f(w) = \begin{cases} w, & w \leq w_c - \frac{\delta}{2} \\ w_c - \frac{\delta}{2} + \beta(w - w_c + \frac{\delta}{2}), & |w - w_c| \leq \frac{\delta}{2} \\ \begin{cases} \alpha(w - b), & \alpha > 0 \\ w_c - \frac{\delta}{2} + \beta\delta, & \alpha = 0 \end{cases}, & w \geq w_c + \frac{\delta}{2} \end{cases}, \quad (3)$$

where we assume

$$0 \leq \alpha < \beta, \quad \beta > 1, \quad \delta > 0, \quad w_c - \frac{\delta}{2} > 0 \quad (4)$$

and define, for $\alpha > 0$,

$$b = w_c + \frac{\delta}{2} - \frac{1}{\alpha} \left(w_c - \frac{\delta}{2} + \beta\delta \right). \quad (5)$$

As illustrated in Fig. 1(a), $f(w)$ is a continuous piecewise linear function consisting of three linear segments with slopes 1 (soft, blue segment), β (hard, green segment) and α (soft, red segment). The width of the intermediate (hard) green segment is controlled by the parameter $\delta > 0$. In the limit $\delta \rightarrow 0$ its slope β tends to infinity, and we obtain a bilinear function with a jump discontinuity at $w = w_c$ that was considered by Gorbushin et al. [2022] for $\alpha > 1$ and by Gorbushin and Truskinovsky [2019, 2021] for $\alpha = 1$.

Note that since $\beta > 1$ and $\alpha < \beta$, $f(w)$ has a *hardening-softening* form that changes from convex to concave at any point along the green segment in Fig. 1(a). In the special case $\alpha = 0$ the interaction force saturates to a constant value above $w_c + \delta/2$. This inelastic state corresponds to zero sound speed (“sonic vacuum”).

In this paper we are interested in traveling waves that connect stable equilibrium states of the system (2), with constant strains w_{\pm} such that $f'(w_{\pm}) \geq 0$, and propagate with velocity V that is supersonic with respect to both limiting states:

$$w_n(t) = w(\xi), \quad \xi = n - Vt, \quad (6)$$

where

$$\lim_{\xi \rightarrow \pm\infty} w(\xi) = w_{\pm} \quad (7)$$

and $V^2 > f'(w_{\pm})$. The function $w(\xi)$ must thus satisfy the advance-delay differential equation

$$V^2 w''(\xi) = f(w(\xi + 1)) - 2f(w(\xi)) + f(w(\xi - 1)). \quad (8)$$

2.1 Superkinks

Suppose the traveling wave (TW) is a monotone front connecting two *different* limiting states, $w_- \neq w_+$ in the blue and red segments, as shown in Fig. 1. Such transition waves have been classified by Gorbushin et al. [2022] as supersonic kinks, or *superkinks*.

One can show [Serre, 2007, Aubry and Proville, 2009, Herrmann and Rademacher, 2010, Herrmann, 2011, Gorbushin and Truskinovsky, 2019, 2021, Gorbushin et al., 2022] that in addition to the classical Rankine-Hugoniot jump condition

$$f(w_+) - f(w_-) = V^2(w_+ - w_-), \quad (9)$$

which states that the slope of the *Rayleigh line* connecting $(w_+, f(w_+))$ and $(w_-, f(w_-))$ equals V^2 , as shown in Fig. 1, such solutions must satisfy the condition

$$\Phi(w_+) - \Phi(w_-) - \frac{1}{2}(w_+ - w_-)(f(w_+) + f(w_-)) = 0. \quad (10)$$

This additional condition constitutes a *kinetic relation* for a superkink. More precisely, it states that the *driving force* $G = \Phi(w_+) - \Phi(w_-) - \frac{1}{2}(w_+ - w_-)(f(w_+) + f(w_-))$ [Truskinovskii, 1987] on the moving front is zero, and thus there is no dissipation associated with its motion. Geometrically it means that the two areas cut by the Rayleigh line from $f(w)$ must be equal, as shown in Fig. 1(b). Due to the trilinear form (3) of $f(w)$, it follows that the superkink velocity V must satisfy

$$\max\{1, \alpha\} < V^2 < \beta. \quad (11)$$

The conditions (9) and (10) imply that in the case of superkinks, only one of the values w_- , w_+ and V can be prescribed independently. In particular, they determine $|V|$ and w_- for a given w_+ . Global existence of superkinks in the FPU problem with smooth hardening-softening interactions was proved by Herrmann and Rademacher [2010] and Herrmann [2011] under the area condition (10). Local analysis by Iooss [2000] has shown that for smooth $f(w)$ small-amplitude superkinks bifurcate from local maxima of $f'(w)$ connecting convex and concave parts of $f(w)$. Exact superkink solutions in the problem with bilinear interactions ($\delta = 0$ in (3)) were constructed by Gorbushin and Truskinovsky [2019, 2021] and Gorbushin et al. [2022]. Note that for each superkink solution propagating with velocity V , there exists a solution of the same form but velocity $-V$. In addition, for each kink solution with $w_- > w_+$, i.e., a front with $w'(\xi) < 0$, there is an *antikink* solution $\tilde{w}(\xi) = w(-\xi)$ with the limiting states interchanged, so that $\tilde{w}'(\xi) > 0$, and the same velocity. Thus, it suffices to consider kink solutions with $V > 0$.

2.2 Solitary waves

As discussed by Gorbushin and Truskinovsky [2019, 2021] and Vainchtein and Truskinovsky [2024], superkinks are closely related to *solitary waves*, pulse-like solutions of (8) connecting *identical* limiting states, $w_- = w_+$, and propagating with supersonic velocities. Existence of solitary wave (SW) solutions has been shown by Friesecke and Wattis [1994]; see also a recent review by Vainchtein [2022]. Note that such solutions automatically satisfy (9) and (10). Solitary waves can be *tensile*, $w(\xi) > w_+$, or *compressive*, $w(\xi) < w_+$. Similar to the superkinks, for each solitary wave moving with velocity V , there is a wave of the same form moving with velocity $-V$, so it suffices to consider positive velocities.

Importantly, the speed of the solitary wave solutions that tend to w_+ at plus and minus infinity is bounded from below by the sonic limit and from above by the superkink speed: $f'(w_+) < V^2 < V_{\text{SK}}^2$, where V_{SK} is the velocity of the superkink with the state w_+ ahead. As the superkink limit is approached, solitary wave solutions increase in amplitude and become wider and more flat in the middle, with the two boundary layers on the left and on the right that approximate monotone superkink solutions. Thus, for velocities just below the superkink limit, solitary waves acquire a structure where a kink and an antikink move in tandem. This will be further illustrated by explicit solutions constructed in the next section for a QC model. Solitary waves of this type, sometimes referred to as “flat-top solitons”, have been recently obtained for first-order nonlinear systems including the extended Gardner-like equations [Rosenau and Oron, 2020, 2022] and oscillator chains [Rosenau and Pikovsky, 2020, 2021]. In the context of the FPU problem, such solutions and the limiting superkinks were obtained by Vainchtein and Truskinovsky [2024] for cubic interactions and by Gorbushin and Truskinovsky [2019, 2021] for the special case of bilinear interactions with equal slopes that enables analytical treatment of the discrete problem.

As shown by Gorbushin and Truskinovsky [2019, 2021] and Vainchtein and Truskinovsky [2024], one can also construct solitary wave solutions above the superkink limit. Such solutions have velocity-dependent background state at infinity and tend to a bound kink-antikink structure as the

superkink limit is approached from above. In this work, however, we limit our attention to solitary waves below the superkink limit.

3 Exact solutions for a quasicontinuum model

In view of the complexity of the original discrete problem represented by an infinite system (1) of nonlinear ordinary differential equations, we first turn first to a model representing its analytically transparent QC approximation that yields exact TW solutions. The QC model we consider is described by the regularized Boussinesq partial differential equation

$$u_{tt} - \frac{1}{12}u_{xxtt} = (f(u_x))_x, \quad (12)$$

which can be obtained from (1) using the (2, 2) Padé approximation, $4\sin^2(k/2) \approx k^2/(1 + k^2/12)$, of the discrete Laplacian in Fourier space [Rosenau, 1986]. The associated Lagrangian density

$$\mathcal{L} = \frac{1}{2} \left(u_t^2 + \frac{1}{12}u_{tx}^2 \right) - \Phi(u_x), \quad (13)$$

contains an additional “microkinetic” energy term $(1/24)u_{tx}^2$.

One can show [Vainchtein and Truskinovsky, 2024] that in this model the traveling wave equation for $w(\xi) = u_x(x, t)$, $\xi = x - Vt$, reduces to

$$-\frac{V^2}{12}w'' + V^2w - f(w) = V^2w_+ - f(w_+), \quad (14)$$

where the boundary condition at $\xi \rightarrow \infty$ in (7) was used. Together with the boundary condition at $\xi \rightarrow -\infty$ in (7), this yields the Rankine-Hugoniot condition (9). Integrating (14) results in the first-order ordinary differential equation

$$-\frac{V^2}{24}(w')^2 = \Phi(w) - \Phi(w_+) - f(w_+)(w - w_+) - \frac{V^2}{2}(w - w_+)^2, \quad (15)$$

where the boundary condition at $\xi \rightarrow \infty$ in (7) was used again. In view of the boundary condition at $\xi \rightarrow -\infty$ in (7), this yields

$$\Phi(w_-) - \Phi(w_+) - f(w_+)(w_- - w_+) - \frac{V^2}{2}(w_- - w_+)^2 = 0,$$

which together with (9) implies that the equal-area condition (10). For a superkink solution of (14), the limiting states w_{\pm} satisfy (9) and (10) for a given V . For solitary waves, we can independently prescribe the background state w_+ and supersonic velocity V with magnitude below the superkink limit.

In the case of trilinear interactions (3), equation (14) can be solved analytically in each segment (blue, green and red) where the elastic modulus is constant and the corresponding ordinary differential equation is linear. The obtained solutions can then be matched using the continuity conditions, as described below.

3.1 Superkinks

Consider first the superkink solutions (14) with $f(w)$ given by (3) that connect the states w_+ and w_- in the blue and red segments in Fig. 1, respectively ($w_+ < w_c - \delta/2$ and $w_- > w_c + \delta/2$) and propagate with velocity $V > 0$ that satisfies (11). Observe that in this case we have $f(w_+) = w_+$, so (14) simplifies to

$$-\frac{V^2}{12}w'' + V^2w - f(w) = (V^2 - 1)w_+, \quad (16)$$

while (9) becomes

$$w_- = \frac{(V^2 - 1)w_+ - \alpha b}{V^2 - \alpha} \quad (17)$$

for $\alpha > 0$ and

$$w_- = \frac{(V^2 - 1)w_+ + w_c + \beta\delta - \delta/2}{V^2} \quad (18)$$

for $\alpha = 0$. We seek monotone kink solutions such that $w(\xi) > w_c + \delta/2$ (red linear segment of $f(w)$ in Fig. 1) for $\xi < -z$, where $z > 0$ is to be determined, $|w(\xi) - w_c| < \delta/2$ (green segment) for $-z < \xi < z$ and $w(\xi) < w_c - \delta/2$ (blue segment) for $\xi > z$. Solving the corresponding linear equations in each interval yields

$$w(\xi) = \begin{cases} w_+ + Ae^{-r\xi}, & \xi \geq z, \\ w_S + B\cos(q\xi) + C\sin(q\xi), & |\xi| \leq z, \\ w_- + De^{s\xi}, & \xi \leq -z, \end{cases} \quad (19)$$

where w_- is related to w_+ via (17) for $\alpha > 0$ and (18) for $\alpha = 0$,

$$w_S = \frac{(w_c - \delta/2)(\beta - 1) - w_+(V^2 - 1)}{\beta - V^2} \quad (20)$$

is the intersection of $f(w)$ and the Rayleigh line in the hard (green) linear regime (see Fig. 1(b)), and the roots r , q and s are given by

$$r = \frac{\sqrt{12(V^2 - 1)}}{V}, \quad q = \frac{\sqrt{12(\beta - V^2)}}{V}, \quad s = \frac{\sqrt{12(V^2 - \alpha)}}{V}. \quad (21)$$

Note that at $\alpha = 0$ we have $s = \sqrt{12}$.

Before providing further details about the solution (19), we discuss a physical interpretation of its structure. One can think of the frontal part of the superkink solution ($\xi > a$, $|a| < z$) as a portion of the structured shock wave propagating with velocity V that has the strain w_+ in front and oscillations around the average strain w_S with wave number q . In the non-dispersive continuum limit the transition layer and the oscillations disappear from the shock's structure, and it becomes a moving discontinuity that dissipates energy at the rate VS_2 , where S_2 is the shaded pink area in Fig. 1(b). As discussed by Gorbushin et al. [2022], this energy release rate can equivalently be computed on the microscopic level by accounting for the energy radiated in form of the dispersive wave propagating behind the shock. Note, however, that only a portion of this shock solution is included in (19). Meanwhile, the back part of the superkink ($\xi < a$) can be represented by a portion of the structured shock wave that has oscillations around w_S ahead and w_- behind. This second wave is not an admissible shock wave because it is supersonic with respect to the state behind and thus violates the Lax condition. It absorbs energy at the rate VS_1 , where S_1 is the blue shaded area in Fig. 1(b), which, as we discussed above, equals VS_2 , the rate at which the energy

is released. A superkink can thus be thought of as a bundle of admissible and inadmissible shock waves, where the energy released in the front is transported to the back, where it is absorbed, by the mode q . Indeed, observing that the dispersion relation in the hard linear regime is given by $\omega^2 = \beta k^2 / (1 + k^2/12)$ in the QC model, one can show that the energy is carried with the group velocity $\omega'(q) = V^3/\beta$, which is less than the phase velocity V since $V^2 < \beta$, and thus the energy is transported from front to back. Inside the superkink bundle, the energy sink (inadmissible shock wave) is stabilized by the elastic radiation from the energy source (admissible shock wave), which is sometimes called the “feeding wave” [Slepyan, 2001, Gorbushin et al., 2020].

To find the six unknown variables in z , w_+ and the coefficients A , B , C and D (19), for given V , we apply the continuity conditions for $w(\xi)$ and $w'(\xi)$ at $\xi = \pm z$ (four conditions) and the two switch conditions $w(\pm z) = w_c \pm \delta/2$. In the generic case $0 \leq \alpha \neq 1$ this yields

$$w(\xi) = w_+ + \frac{\delta e^{-r(\xi-z)}}{\alpha - 1} \left[\beta - \alpha - \frac{\sqrt{(\beta - 1)(\beta - \alpha)(V^2 - \alpha)}}{\sqrt{V^2 - 1}} \right], \quad \xi \geq z, \quad (22)$$

$$w(\xi) = \frac{\delta \sqrt{(\beta - \alpha)(\beta - 1)}}{\sqrt{(\beta - \alpha)(V^2 - 1)} + \sqrt{(\beta - 1)(V^2 - \alpha)}} \cos(q\xi - \phi) + \frac{(\beta - 1)(w_c - \delta/2) - (V^2 - 1)w_+}{\beta - V^2}, \quad |\xi| \leq z, \quad (23)$$

where

$$\phi = \pi\theta(\alpha - 1) + \arctan \frac{\sqrt{(\beta - \alpha)(V^2 - 1)} + \sqrt{(\beta - 1)(V^2 - \alpha)}}{\sqrt{\beta - V^2}(\sqrt{\beta - 1} - \sqrt{\beta - \alpha})},$$

and

$$w(\xi) = w_- + \frac{\delta e^{s(\xi+z)}}{\alpha - 1} \left[\beta - 1 - \frac{\sqrt{(\beta - 1)(\beta - \alpha)(V^2 - 1)}}{\sqrt{V^2 - \alpha}} \right], \quad \xi \leq -z. \quad (24)$$

Here

$$z = \frac{V}{4\sqrt{3}\sqrt{\beta - V^2}} \left\{ \arctan \frac{\sqrt{\beta - V^2}(\sqrt{V^2 - \alpha} + \sqrt{V^2 - 1})}{\beta - V^2 - \sqrt{(V^2 - \alpha)(V^2 - 1)}} + \pi\theta(\sqrt{(V^2 - \alpha)(V^2 - 1)} - \beta + V^2) \right\}, \quad (25)$$

where $\theta(x) = 1$ for $x > 0$ and zero otherwise, and the limiting states are given by

$$w_+ = w_c + \frac{\delta}{2(\alpha - 1)} \left\{ 1 + \alpha - 2\beta + \frac{2\sqrt{(\beta - \alpha)(\beta - 1)(V^2 - \alpha)}}{\sqrt{V^2 - 1}} \right\} \quad (26)$$

and

$$w_- = w_c + \frac{\delta}{2(\alpha - 1)} \left\{ 1 + \alpha - 2\beta + \frac{2\sqrt{(\beta - \alpha)(\beta - 1)(V^2 - 1)}}{\sqrt{V^2 - \alpha}} \right\}. \quad (27)$$

Some examples of strain profiles are shown in Fig. 2. The particle velocity is given by $v(\xi) = -Vw(\xi)$.

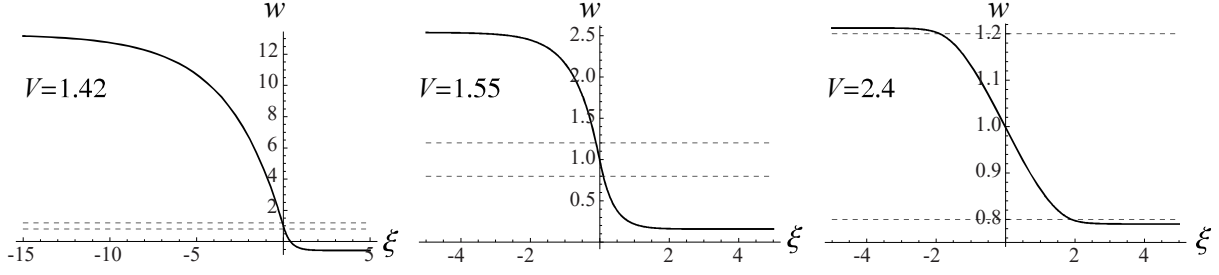


Figure 2: Strain profiles at different velocities when $\alpha = 2$, $\delta = 0.4$, $b = -0.4$, $w_c = 1$. The left panel shows the superkink traveling with velocity just above the lower limit $\sqrt{\alpha} \approx 1.41$, and the right panel the one with velocity slightly below the upper limit $\sqrt{\beta} \approx 2.45$. Dashed horizontal lines mark $w = w_c \pm \delta/2$.

In the symmetric case $\alpha = 1$ (equal slopes of the red and blue segments), we have $s = r$, and the solution is given by

$$w(\xi) = \begin{cases} w_+ + \frac{\delta(\beta - V^2)}{2(V^2 - 1)} e^{-r(\xi - z)}, & \xi \geq z \\ \frac{(\beta - 1)(w_c - \delta/2) - (V^2 - 1)w_+}{\beta - V^2} - \frac{\delta\sqrt{\beta - 1}}{2\sqrt{V^2 - 1}} \sin(q\xi), & |\xi| \leq z \\ w_- - \frac{\delta(\beta - V^2)}{2(V^2 - 1)} e^{r(\xi + z)}, & \xi \leq -z, \end{cases} \quad (28)$$

with

$$z = \frac{V}{4\sqrt{3}\sqrt{\beta - V^2}} \left\{ \arctan \frac{2\sqrt{\beta - V^2}\sqrt{V^2 - 1}}{\beta - 2V^2 + 1} + \pi\theta(2V^2 - \beta - 1) \right\} \quad (29)$$

and

$$w_{\pm} = w_c \mp \frac{\delta(\beta - 1)}{2(V^2 - 1)} = w_c \pm \frac{b}{2(V^2 - 1)}, \quad (30)$$

so that the limiting strains are independent of δ (note that (5) implies that $b = \delta(1 - \beta) < 0$ in this case).

The effect of α on $z(V)$, $w_+(V)$ and the solution profiles is shown in Fig. 3. Recall that by (11) the upper velocity limit is $\sqrt{\beta}$ in all cases. As this limit is approached, z tends to infinity:

$$z \approx \frac{\pi\sqrt{\beta}}{8\sqrt{3}\sqrt{\beta - V^2}} \quad \text{as } V \rightarrow \sqrt{\beta}, \quad (31)$$

while the two limiting strains approach the boundaries of the intermediate linear segment: $w_{\pm} \rightarrow w_c \mp \delta/2$. Thus, as the upper velocity limit is approached ($V \rightarrow \sqrt{\beta}$), the superkink becomes infinitely wide ($z \rightarrow \infty$), while its amplitude $w_- - w_+$ tends to δ . This is illustrated in Fig. 2(c). Therefore, in contrast to the case of smooth $f(w)$ [Vainchtein and Truskinovsky, 2024], where solutions delocalize to a constant value (a kink of zero amplitude) at the bifurcation point, here they approach a kink of finite amplitude but infinite width. Thus, in the trilinear case the bifurcation is degenerate.

The lower velocity limits are different for $\alpha > 1$ and $0 \leq \alpha \leq 1$. In the case $\alpha > 1$ (11) yields $\sqrt{\alpha} < V < \sqrt{\beta}$. In the limit $V \rightarrow \sqrt{\alpha}$ the half-width z of the transition region approaches a finite positive value, as illustrated by the blue curve in Fig. 3(a):

$$z \rightarrow \frac{\sqrt{\alpha}}{4\sqrt{3}\sqrt{\beta - \alpha}} \arctan \sqrt{\frac{\alpha - 1}{\beta - \alpha}} \quad \text{as } V \rightarrow \sqrt{\alpha}. \quad (32)$$

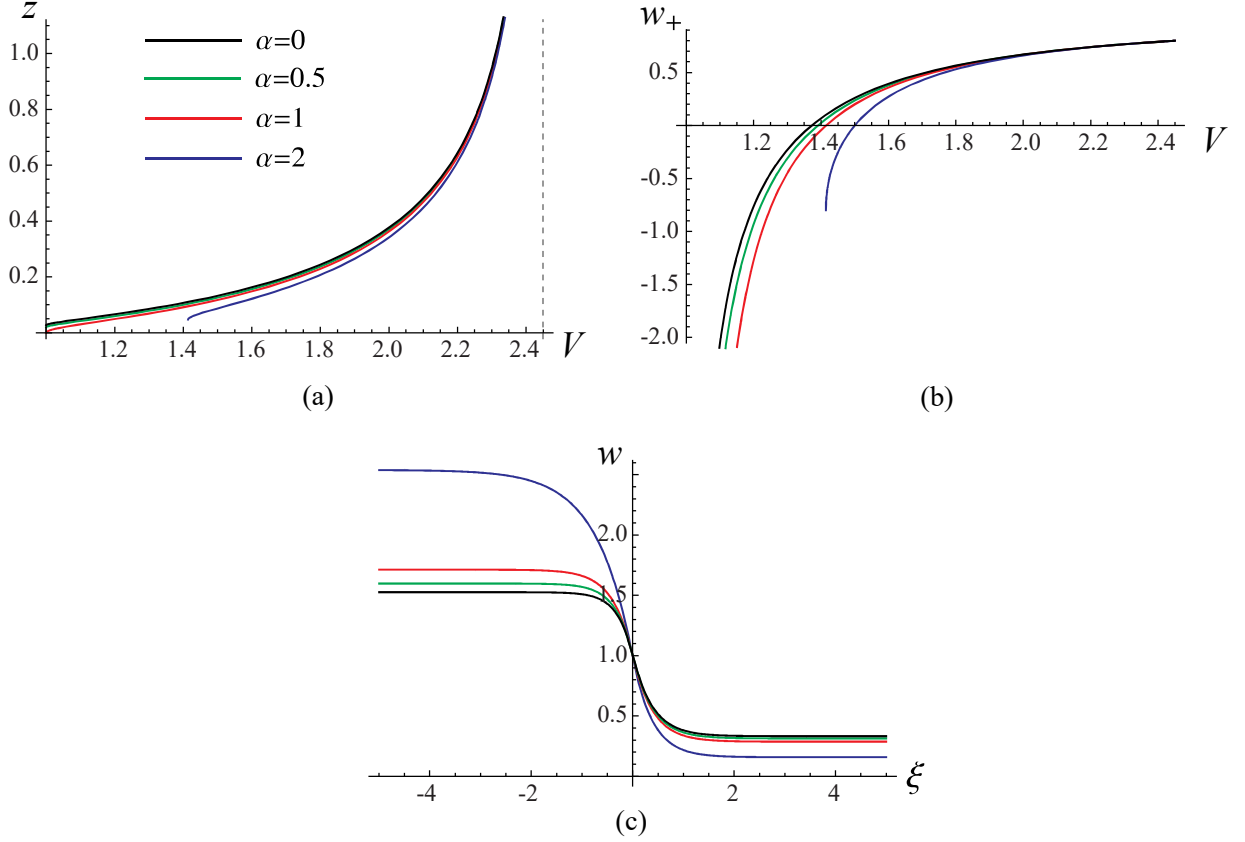


Figure 3: (a) The functions $z(V)$, which tend to infinity as $V \rightarrow \sqrt{\beta}$ (dashed vertical line), for different α . For $\alpha > 1$ (blue curve), the lower velocity bound is $\sqrt{\alpha}$. (b) Plots of $w_+(V)$. Note that w_+ tends to $-\infty$ as $V \rightarrow 1$ for $\alpha \leq 1$ (black, green and red curves), while for $\alpha > 1$ (blue curve) it has a finite value at $V = \sqrt{\alpha}$. (c) Strain profiles at $V = 1.55$. The legend in panel (a) applies to all four panels. Here $\beta = 6$, $\delta = 0.4$ and $w_c = 1$.

The limiting strain w_+ is finite in the limit (see the blue curve in Fig. 3(b)), while w_- tends to infinity:

$$w_+ \rightarrow w_c + \frac{\delta(1 + \alpha - 2\beta)}{2(\alpha - 1)} = \frac{\alpha b}{\alpha - 1}, \quad w_- \approx \frac{\delta \sqrt{(\beta - \alpha)(\beta - 1)}}{\sqrt{\alpha - 1} \sqrt{V^2 - \alpha}} \quad \text{as } V \rightarrow \sqrt{\alpha},$$

where we used (5) in the first limit. See Fig. 2(a) for an example of a superkink near the lower velocity limit.

In the case $0 \leq \alpha \leq 1$ we have $1 < V < \sqrt{\beta}$. As the lower limit of unit velocity is approached, we have

$$z \rightarrow \frac{1}{4\sqrt{3}\sqrt{\beta - 1}} \arctan \sqrt{\frac{1 - \alpha}{\beta - 1}} \quad \text{as } V \rightarrow 1, \quad (33)$$

which yields a finite positive value for $\alpha \neq 1$ (see the black and green curves in Fig. 3(a)) and zero at $\alpha = 1$ (red curve in Fig. 3(a)). For $0 \leq \alpha < 1$ w_+ tends to $-\infty$ (see the black and green curves in Fig. 3(b)), while w_- is finite in the limit:

$$w_+ \approx -\frac{\delta \sqrt{(\beta - \alpha)(\beta - 1)}}{\sqrt{1 - \alpha} \sqrt{V^2 - 1}}, \quad w_- \rightarrow w_c + \frac{\delta(1 + \alpha - 2\beta)}{2(\alpha - 1)} \quad \text{as } V \rightarrow 1.$$

In contrast, in the symmetric case $\alpha = 1$, illustrated by the red curve in Fig. 3(b), both limiting strains become infinite in the sonic limit (recall (30)). Note also that the magnitude of strain grows faster in this case (inversely proportional to $V^2 - 1$, rather than $(V^2 - 1)^{1/2}$).

3.2 Solitary waves

We now turn to SW solutions in the QC problem (14) with $f(w)$ given by (3). Recall that such solutions satisfy

$$w(\xi) \rightarrow w_+ \quad \text{as } \xi \rightarrow \pm\infty \quad (34)$$

and propagate with supersonic velocities V bounded by the superkink velocity $V_{\text{SK}}(w_+)$ for given w_+ . The waves can be tensile or compressive, depending on whether w_+ is in the lower ($w_+ < w_c - \delta/2$) or the upper ($w_+ > w_c + \delta/2$) linear regime.

Tensile waves. We start with tensile solitary waves ($w(\xi) > w_+$), which arise when $w_+ < w_c - \delta/2$. In this case $1 < V < V_{\text{SK}}(w_+)$, where

$$V_{\text{SK}}(w_+) = \sqrt{1 + \frac{4(\beta - \alpha)(\beta - 1)\delta^2}{(1 - \alpha)(2(w_c - w_+) - \delta)^2 + 8(\beta - \alpha)\delta(w_c - w_+)}} \quad (35)$$

is obtained by solving (26) for $V = V_{\text{SK}}$ as a function of w_+ . In the symmetric case $\alpha = 1$ we have $b = -(\beta - 1)\delta$, and (35) has the much simpler form

$$V_{\text{SK}}(w_+) = \sqrt{1 - \frac{b}{2(w_c - w_+)}}.$$

There are two velocity regimes that need to be considered. In the first regime, we have $1 < V \leq V_{\text{cr}}(w_+)$, where $V_{\text{cr}}(w_+)$ is the critical velocity value such that $w(\xi) \leq w_c + \delta/2$ for velocities below it, i.e., the solitary wave remains confined to the first and second (intermediate) linear regimes, switching from one to another at $\xi = \pm z_1$, where $z_1 > 0$ depends on V . Continuity of $w(\xi)$ and $w'(\xi)$ and the switch conditions $w(\pm z_1) = w_c - \delta/2$ then yield

$$w(\xi) = \begin{cases} w_+ + (w_c - \delta/2 - w_+)e^{-r(|\xi| - z_1)}, & |\xi| \geq z_1, \\ w_S + \frac{\sqrt{(\beta - 1)(V^2 - 1)}}{\beta - V^2}(w_c - \delta/2 - w_+)\cos(q\xi), & |\xi| \leq z_1, \end{cases} \quad (36)$$

where w_S is given by (20), and

$$z_1 = \frac{1}{q} \left(\pi - \arctan \frac{q}{r} \right). \quad (37)$$

Setting $w(0) = w_c + \delta/2$, we obtain the upper velocity bound for this regime:

$$V_{\text{cr}}(w_+) = \sqrt{1 + \frac{\delta^2(\beta - 1)}{(w_c - w_+ + \delta/2)^2}}. \quad (38)$$

For $V_{\text{cr}}(w_+) < V < V_{\text{SK}}(w_+)$, the solution involves all three linear regions and has the form

$$w(\xi) = \begin{cases} w_+ + Ae^{-r(|\xi| - z_1)}, & |\xi| \geq z_1, \\ w_S + B \cos(q\xi) + C \sin(q|\xi|), & z_2 \leq |\xi| \leq z_1, \\ w_- + D \cosh(s\xi), & |\xi| \leq z_2, \end{cases} \quad (39)$$

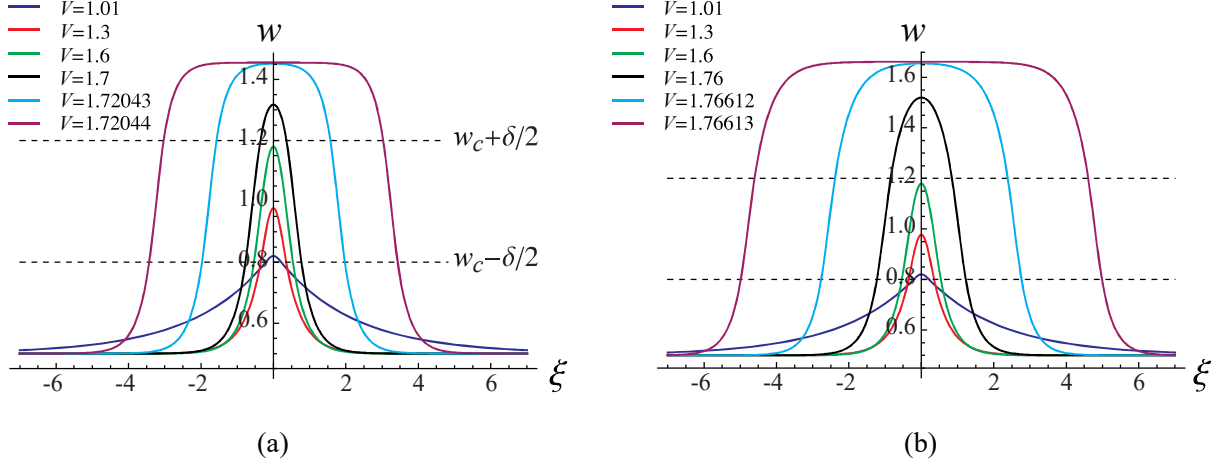


Figure 4: Tensile solitary waves in the trilinear model (3) at different velocities at $w_+ = 0.5$ and (a) $\alpha = 0.5$; (b) $\alpha = 2$. Here $\beta = 6$, $w_c = 1$, $\delta = 0.4$.

where the coefficients A, B, C, D listed in (A.1) in Appendix A are found by imposing the continuity of the strain and its derivative, w_- is given by (17) for $\alpha > 0$ and by (18) for $\alpha = 0$, and w_S is given by (20). Imposing $w(\pm z_1) = w_c - \delta/2$ and $w(\pm z_2) = w_c + \delta/2$ then yields

$$z_2 = \frac{1}{s} \operatorname{arctanh} \frac{\sqrt{(V^2 - 1)(w_c - w_+ + \delta/2)^2 - (\beta - 1)\delta^2}}{\sqrt{V^2 - \alpha}(w_- - w_c - \delta/2)} \quad (40)$$

and

$$z_1 = z_2 + \frac{1}{q} \left(\arccos \frac{(V^2 - 1)(w_c + \delta/2 - w_+) - (\beta - 1)\delta}{\sqrt{(\beta - 1)(V^2 - 1)(w_c - \delta/2 - w_+)}} - \arctan \frac{q}{r} \right). \quad (41)$$

Note that $z_2 = 0$ at $V = V_{\text{cr}}(w_+)$ and that $z_2 \rightarrow \infty$ as $V \rightarrow V_{\text{SK}}(w_+)$, which means that the width of the solitary waves tends to infinity as the upper velocity limit is approached. One can also verify that in this limit $w(0) \rightarrow w_-$ and $z_1 - z_2 \rightarrow 2z$, where we recall that z , given by (25) for $\alpha \neq 1$ and (29) for $\alpha = 1$, is the half-width of the transition interval for a superkink solution. This is consistent with the SW solution approaching a kink-antikink bundle, as discussed by Gorbushin and Truskinovsky [2019, 2021] and Vainchtein and Truskinovsky [2024], at velocities just below the superkink limit. Examples of tensile solitary waves illustrating this are shown in Fig. 4. Observe also that the near-sonic solutions, which are given by (36) and are independent of α , delocalize to the constant strain $w(\xi) = w_c - \delta/2$ as $V \rightarrow 1$ because $r \rightarrow 0$ in (21) tends to zero in this limit.

Compressive waves. Similarly, we can obtain compressive SW solutions, which arise when $w_+ > w_c + \delta/2$ and $\sqrt{\alpha} < V < V_{\text{SK}}(w_+)$, where

$$V_{\text{SK}}(w_+) = \sqrt{\alpha + \frac{4(\beta - \alpha)(\beta - 1)\delta^2}{(\alpha - 1)(2(w_+ - w_c) - \delta)^2 + 8(\beta - 1)\delta(w_+ - w_c)}} \quad (42)$$

is obtained by setting the right hand side of (27) equal to w_+ and solving the resulting equation for $V = V_{\text{SK}}$ as a function of w_+ . The superkink velocity simplifies to

$$V_{\text{SK}}(w_+) = \sqrt{1 - \frac{b}{2(w_+ - w_c)}}$$

in the case $\alpha = 1$.

In this case we also have two velocity regimes. In the first, $\sqrt{\alpha} < V \leq V_{\text{cr}}(w_+)$, where

$$V_{\text{cr}}(w_+) = \sqrt{\alpha + \frac{\delta^2(\beta - \alpha)}{(w_+ - w_c + \delta/2)^2}}, \quad (43)$$

and we have

$$w(\xi) = \begin{cases} w_+ - (w_+ - w_c - \delta/2)e^{-s(|\xi| - z_1)}, & |\xi| \geq z_1, \\ w_S - \frac{\sqrt{(\beta - \alpha)(V^2 - \alpha)}}{\beta - V^2}(w_+ - w_c - \delta/2)\cos(q\xi), & |\xi| \leq z_1, \end{cases} \quad (44)$$

with

$$w_S = \frac{(\beta - 1)(w_c - \delta/2) - (V^2 - 1)w_-}{\beta - V^2}, \quad (45)$$

$$z_1 = \frac{1}{q} \left(\pi - \arctan \frac{q}{s} \right) \quad (46)$$

and

$$w_- = \frac{(V^2 - \alpha)w_+ + \alpha b}{V^2 - 1}.$$

In the second regime, $V_{\text{cr}}(w_+) < V < V_{\text{SK}}(w_+)$, the solution has the form

$$w(\xi) = \begin{cases} w_+ + Ae^{-s(|\xi| - z_1)}, & |\xi| \geq z_1, \\ w_S + B\cos(q\xi) + C\sin(q|\xi|), & z_2 \leq |\xi| \leq z_1, \\ w_- + D\cosh(r\xi), & |\xi| \leq z_2, \end{cases} \quad (47)$$

where w_S is provided in (45), the coefficients A , B , C and D are given by (A.2), and we have

$$z_2 = \frac{1}{r} \operatorname{arctanh} \frac{\sqrt{(V^2 - \alpha)(w_+ - w_c + \delta/2)^2 - (\beta - \alpha)\delta^2}}{\sqrt{V^2 - 1}(w_c - \delta/2 - w_-)} \quad (48)$$

and

$$z_1 = z_2 + \frac{1}{q} \left(\pi - \arctan \frac{q}{s} - \arccos \frac{(V^2 - 1)(w_c - \delta/2 - w_-)}{\sqrt{(\beta - \alpha)(V^2 - \alpha)}(w_+ - w_c - \delta/2)} \right). \quad (49)$$

Similar to the tensile SW solutions, we have $z_2 \rightarrow \infty$, $z_1 - z_2 \rightarrow 2z$ and $w(0) \rightarrow w_-$ in the limit $V \rightarrow V_{\text{SK}}(w_+)$, with solutions just below the limit have the kink-antikink structure, as illustrated in Fig. 5.

Sonic limit and the singular $\alpha = 0$ case. In the case of compressive solitary waves the near-sonic behavior depends on α . When $\alpha > 0$, solutions (44) delocalize to the constant strain $w(\xi) = w_c + \delta/2$ in the sonic limit. Indeed, observe that $s \rightarrow 0$ as $V \rightarrow \sqrt{\alpha}$, so that $w(\xi) \rightarrow w_c + \delta/2$ for $|\xi| \geq z_1$, while $(V^2 - 1)w_- \rightarrow \alpha b$, which together with (5) yields the limit $w(\xi) \rightarrow w_c + \delta/2$ for $|\xi| \leq z_1$. Note that in this case z_1 in (46) is nonzero in the sonic limit.

However, when $\alpha = 0$, the exponent $s = \sqrt{12}$ in (44) is independent of V . Note also that in this case $z_1 \rightarrow 0$ in (46) as $V \rightarrow 0$ because q in (21) tends to infinity in this limit. Thus, in this case we have a *nontrivial sonic limit*: as $V \rightarrow 0$, and thus $\xi = x - Vt \rightarrow x$, the solution approaches

$$w(x) = w_+ - (w_+ - w_c - \delta/2)\exp(-\sqrt{12}|x|). \quad (50)$$

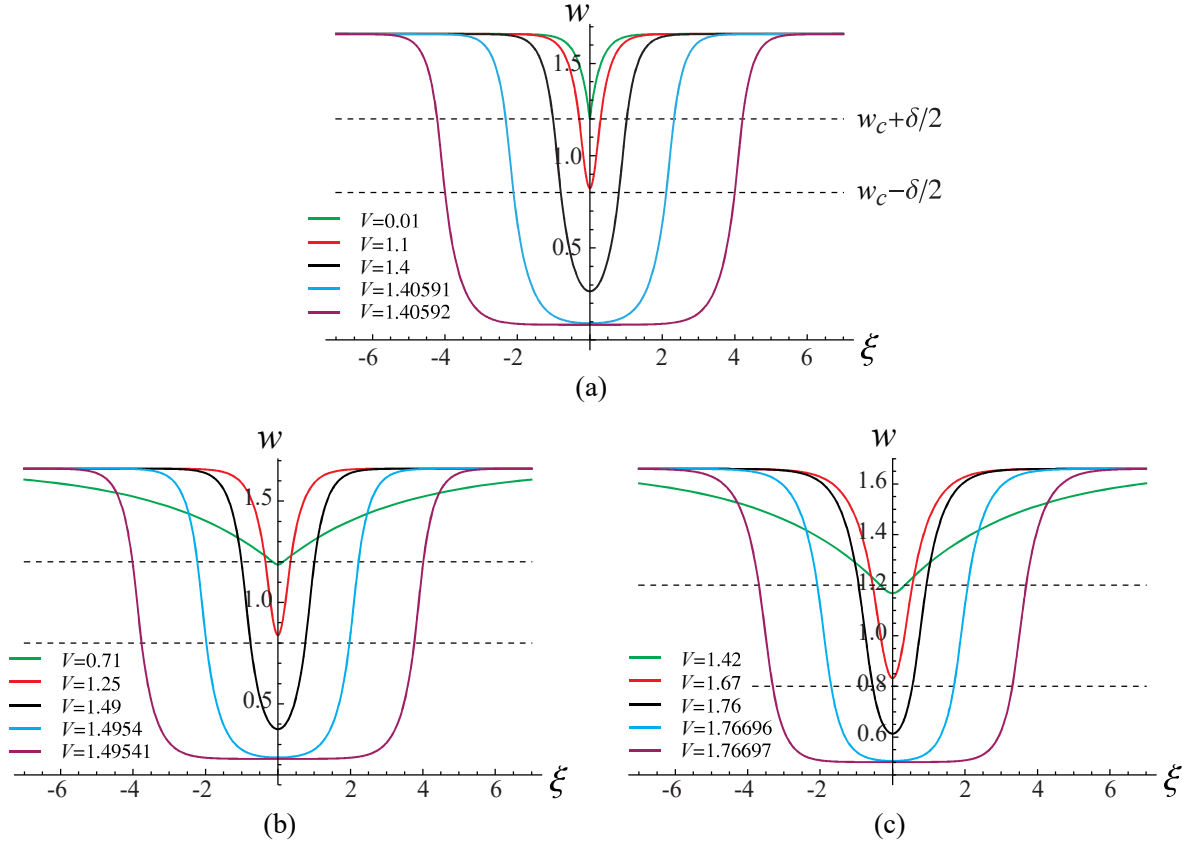


Figure 5: Compressive solitary waves in the trilinear model (3) at different velocities at $w_+ = 1.66$ and (a) $\alpha = 0$; (b) $\alpha = 0.5$; (c) $\alpha = 2$. Here $\beta = 6$, $w_c = 1$, $\delta = 0.4$.

This is a manifestation of the fact that in the case $\alpha = 0$ the sound speed is zero, and slowly moving solitary waves are effectively replacing the conventional linear elastic waves as a elementary “quanta” of mechanical information. Similar effects were first discovered in Hertzian granular chains without precompression [Nesterenko, 2001, Sen et al., 2008, Chong et al., 2017].

4 Traveling wave solutions of the discrete problem

We now turn our attention to traveling wave solutions of the discrete problem (2). As in the QC case, it suffices to consider $V > 0$. To compute these solutions, we follow the approach of Aubry and Proville [2009], Vainchtein et al. [2020], James [2021] and Vainchtein and Truskinovsky [2024] that exploits the fact that traveling waves satisfy (6) and hence are periodic modulo shift:

$$w_{n+1}(t + T) = w_n(t), \quad T = 1/V. \quad (51)$$

This implies that such solutions are fixed points of the nonlinear map

$$\begin{bmatrix} \{w_{n+1}(T)\} \\ \{\dot{w}_{n+1}(T)\} \end{bmatrix} = \mathcal{N} \left(\begin{bmatrix} \{w_n(0)\} \\ \{\dot{w}_n(0)\} \end{bmatrix} \right), \quad (52)$$

where \mathcal{N} is defined by integrating (2) over one period for given initial data over the period T and then shifting the obtained solution by one lattice space. This nonlinear map approach dates back to computation of discrete breathers [Marín and Aubry, 1996].

4.1 Superkinks

To compute the superkink solutions of the discrete problem (2) propagating with given velocity V , we use Newton-Raphson iteration procedure with finite-difference Jacobian to solve

$$\begin{aligned} w_{n+1}(T) &= w_n(0), \quad n = -N/2, \dots, N/2 - 1, \\ \dot{w}_{n+1}(T) &= \dot{w}_n(0), \quad n = -N/2, \dots, N/2 - 2, \quad w_1(T) = w_*, \end{aligned} \quad (53)$$

where $T = 1/V$ and $N \geq 400$ is an even number, for $\{w_n(0), \dot{w}_n(0)\}$, $n = -N/2, \dots, N/2 - 1$. At each iteration, $w_n(T)$ and $\dot{w}_n(T)$ are obtained for given $w_n(0)$ and $\dot{w}_n(0)$ by using Dormand-Prince algorithm (Matlab's ode45 routine) to integrate (2) on the finite chain with the boundary conditions

$$w_{-N/2-1}(t) = w_-, \quad w_{N/2}(t) = w_+,$$

where w_{\pm} are given by (26), (27) for $0 \leq \alpha \neq 1$ and (30) for $\alpha = 1$. The last equation in (53) is a pinning condition, which is necessary to eliminate the non-uniqueness due to the time-translational invariance. To enable the comparison with superkink solutions $w_{QC}(\xi)$ of the QC model, which are also used to obtain an initial guess for the Newton-Raphson procedure, we set $w_* = w_{QC}(0)$, so that $w_0(0) = w_1(T) = w_{QC}(0)$ and thus the traveling wave $w(\xi)$ for the discrete problem satisfies $w(0) = w_{QC}(0)$. To obtain a system of $2N$ nonlinear equations for $2N$ unknowns while prescribing the pinning condition, we drop the equation for $\dot{w}_{N/2}(T)$ in (53). Due to the large size of the computational domain, the equation is automatically satisfied for the computed solutions within the numerical tolerance of 10^{-13} .

The computed strain profiles $w_n(0) = w(n)$ for are shown in Fig. 6 together with the corresponding profiles $w(x)$ obtained from the exact solutions of the QC model. One can see that in the cases shown superkink solutions there is a very good agreement between the discrete and QC models, particularly near the sonic limits (panels (a) and (b)), where the solutions largely involve the long-wave contributions that are well captured by the QC model. Closer inspection of panel (c), however, reveals some discrepancies between solutions of the two models inside the transition layer ($x = \pm 1$).

4.2 Solitary waves

To compute SW solutions with prescribed far-field strain w_+ and velocity V , we use the approach we employed in the case of superkinks, except that in this case the boundary conditions are $w_{-N/2-1}(t) = w_{N/2}(t) = w_+$, and the pinning condition is $\dot{w}_1(T) = 0$. The latter ensures that the maximum of a tensile solitary wave (or the minimum of a compressive one) is at $n = 0$ when $t = 0$. We use parameter continuation in V to compute solutions in the entire velocity range.

The results for tensile waves at $\alpha = 0.5$ and $\alpha = 2$ are shown in Fig. 7-9, while the corresponding results for the compressive waves can be seen in Fig. 10-12. In addition to direct comparison of the discrete and QC solitary waves in Fig. 7 and Fig. 10, we show amplitude-velocity plots in Fig. 8 and Fig. 11, as well as energy-velocity plots in Fig. 9 and Fig. 12. Since the energy of the waves with nonzero background is infinite, we renormalize it by subtracting the energy of the background, as in Vainchtein and Truskinovsky [2024]. For the discrete model this yields

$$E_{\text{ren}}^D(V) = \sum_n \left\{ \frac{1}{2} v_n^2 + \frac{1}{2} (\Phi(w_n) + \Phi(w_{n+1})) - \Phi(w_+) - \frac{1}{2} V^2 w_+^2 \right\} \quad (54)$$

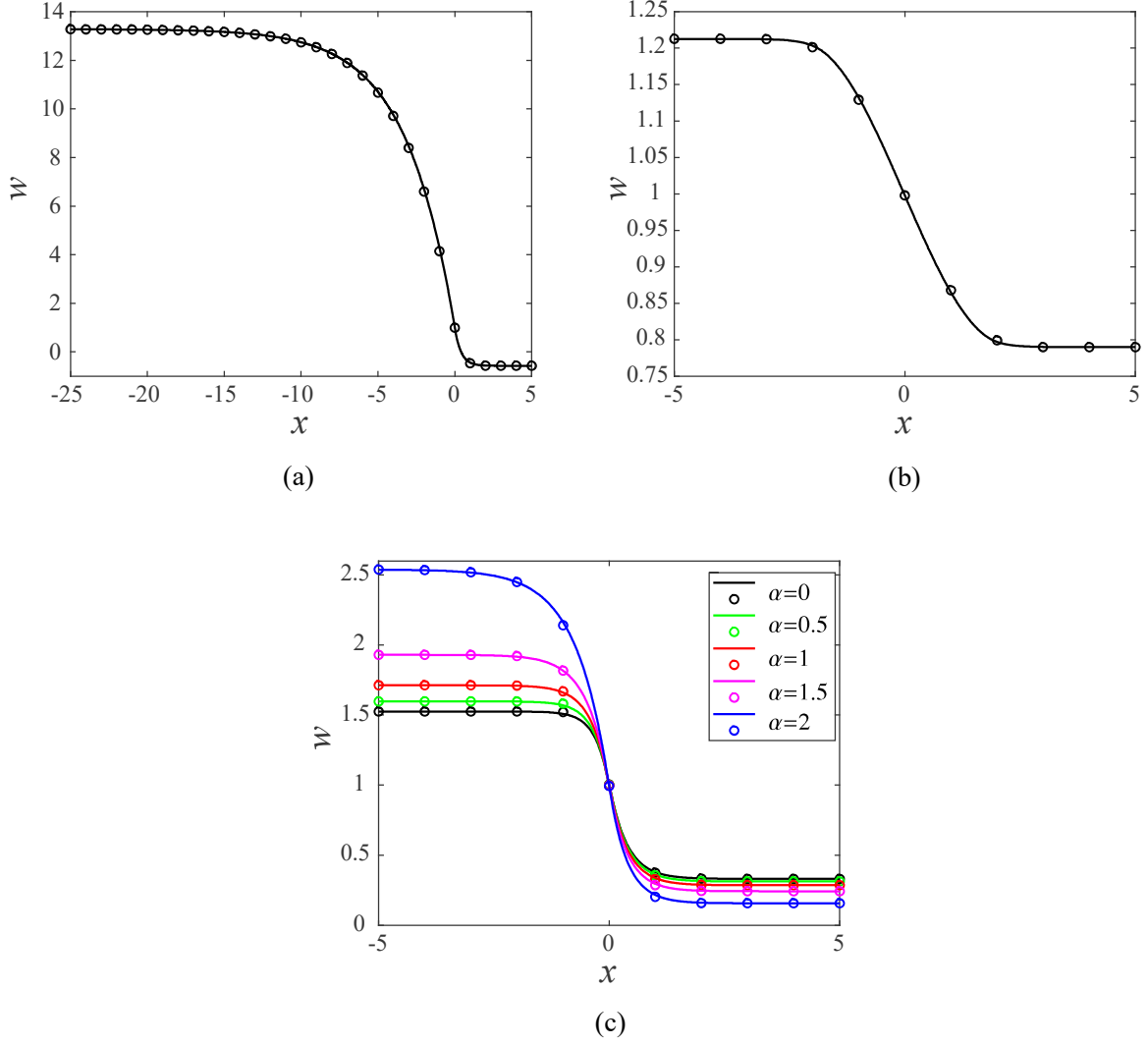


Figure 6: Superkink solutions $w_n(0) = w(n)$ of the discrete problem (8) (circles) with trilinear $f(w)$ and the corresponding solutions $w(x)$ for the QC model (14) (solid curves) evaluated at $t = 0$ for (a) $V = 1.42, \alpha = 2$; (b) $V = 2.4, \alpha = 2$; (c) $V = 1.55$ at different values of α , as indicated in the legend. Here $\beta = 6, \delta = 0.4, w_c = 1$.

in the discrete case, where v_n are the particle velocities, and all values are evaluated at $t = 0$ due to the energy conservation. For the QC model we have

$$E_{\text{ren}}^{\text{QC}}(V) = \int_{-\infty}^{\infty} \left\{ \frac{1}{2} V^2 w^2(\xi) + \frac{1}{24} V^2 (w'(\xi))^2 + \Phi(w(\xi)) - \Phi(w_+) - \frac{1}{2} V^2 w_+^2 \right\} d\xi, \quad (55)$$

where we used the fact that for a traveling wave solution $w(\xi) = w(x - Vt)$ we have $v(\xi) = -Vw(\xi)$.

One can see that the discrepancy between discrete and QC solutions is much more pronounced in the case of solitary waves. For tensile waves, the disagreement between the two models is greater for $\alpha = 0.5$, while for compressive waves there is more discrepancy at $\alpha = 2$. In addition to overestimating the amplitude of solitary waves away from the superkink limit, the QC model does not correctly predict their width. Nevertheless, the QC model captures the evolution of the SW solutions of the discrete problem qualitatively, and one can see quantitative agreement near the sonic and superkink limits.

To gain some insight into the origin of the parameter-dependent quantitative differences between SW solutions of the discrete problem and their QC counterparts, we observe that the QC solutions depend in a rather nontrivial way on the approximations of the characteristic roots of the discrete problem in the three linear regimes. More precisely, the V -dependent roots r , q and s defined in (21) approximate nonzero roots r_D , q_D and s_D of the characteristic equations $4 \sinh^2(r_D/2) - r_D^2 V^2 = 0$, $4\beta \sin^2(q_D/2) - q_D^2 V^2 = 0$ and $4\alpha \sinh^2(s_D/2) - s_D^2 V^2 = 0$ for the discrete problem in the first, second and third linear regime, respectively, that are closest to zero. These characteristic equations can be obtained by taking the Fourier transform of (8) in each linear regime and setting the wave number k to $k = ir_D$, $k = q_D$ and $k = is_D$, respectively. The approximations of their near-zero roots by (21) become progressively worse away from the corresponding sonic limits 1 , $\sqrt{\beta}$ and $\sqrt{\alpha}$. Fig. 13(a-b) shows the roots r , q and s contributing to the QC tensile SW solutions (35)-(41) presented in Fig. 7-9 along with their discrete counterparts r_D , q_D and s_D . For $1 < V \leq V_{\text{cr}}$, only the roots r and q contribute to these solutions, while for $V_{\text{cr}} < V < V_{\text{SK}}$ all three roots r , q and s are involved. In particular, we note that in the second velocity regime the width of the solutions is controlled by z_2 in (40), which depends in an essential way on $1/s$. As shown in Fig. 13(a-b), the roots s and s_D are significantly further apart at $\alpha = 0.5$ in panel (a) compared to the case $\alpha = 2$ in panel (b). Thus, we expect larger differences between the widths of discrete and QC solutions at $\alpha = 0.5$, as observed above. The roots for the compressive waves (42)-(49) presented in Fig. 10-12 are shown in Fig. 13(c-d). In this case it is $1/r$ that contributes in an essential way to z_2 in (48), and one can see that the roots r and r_D are further apart at $\alpha = 2$ in panel (d), which is consistent with the larger width discrepancy at this parameter value reported above. In all four cases shown in Fig. 13 q significantly deviates from q_D in the first velocity regime, contributing to the observed amplitude and width discrepancies between discrete and QC profiles.

Compressive solitary waves at $\alpha = 0$. Of particular interest are compressive solitary waves at $\alpha = 0$. The results for this singular limit are shown in Fig. 14 and Fig. 15.

In this case we can obtain exact solutions for small enough velocities. By periodicity modulo shift it suffices to consider the time interval $[0, T]$, where we recall that $T = 1/V$. Suppose at $t = 0$ the strain w_n has even symmetry about $n = 0$, and $|w_0 - w_c| < \delta/2$, while all other strains satisfy $w_n > w_c + \delta/2$. Let $t = T_1$ be the time when $w_0(t)$ switches to the (degenerate) upper linear regime, $w_0(T_1) = w_c + \delta/2$. Then by symmetry $w_1(t)$ switches to the intermediate linear regime at $t = T_2 = T - T_1$. In what follows, we assume that $T_1 < T_2$, i.e., $T_1 < T/2$. Under these assumptions we find that for $0 \leq t < T_1$ (2) with (3) at $\alpha = 0$ reduce to

$$\ddot{w}_0 + 2\beta w_0 = \beta(2w_c + \delta), \quad \ddot{w}_{\pm 1} = \beta(w_0(t) - w_c) - \beta\delta/2, \quad \ddot{w}_n = 0, \quad |n| \geq 2.$$

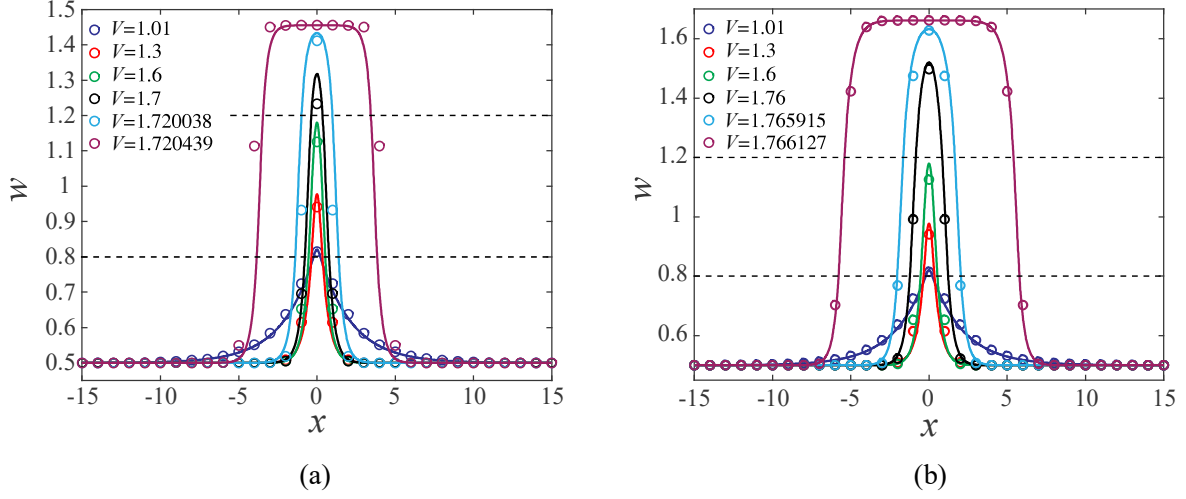


Figure 7: Tensile SW solutions $w_n(0) = w(n)$ of the discrete problem (8) (circles) with trilinear $f(w)$ and the corresponding solutions $w(x)$ for the QC model (14) (solid curves) evaluated at $t = 0$ for (a) $\alpha = 0.5$; (b) $\alpha = 2$. Here $\beta = 6$, $\delta = 0.4$, $w_c = 1$. The background strain is $w_+ = 0.5$, and the corresponding superkink velocity is $V_{SK} = 1.72044$ in (a) and $V_{SK} = 1.76613$ in (b).

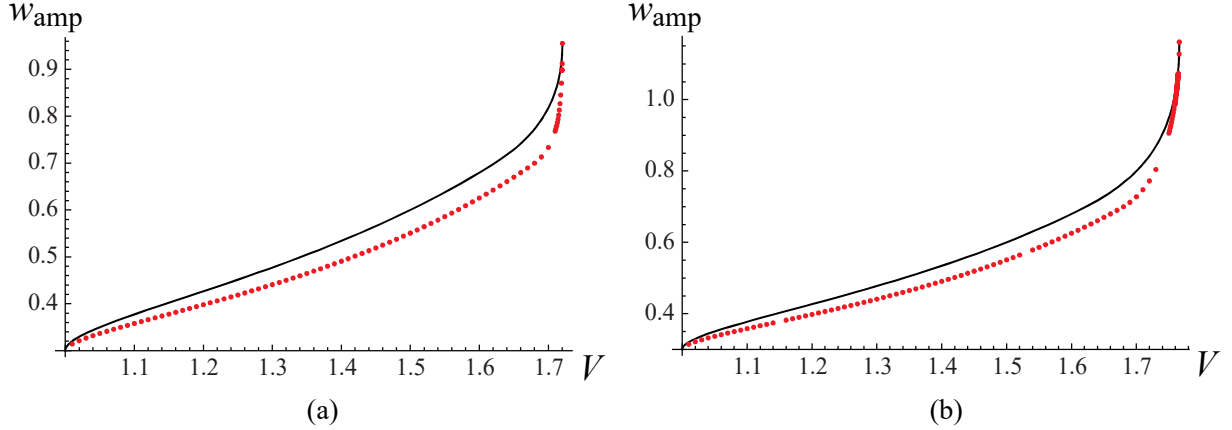


Figure 8: Amplitude $w_{amp} = |w(0) - w_+|$ as a function of velocity V for tensile SW solutions of the discrete problem (8) (circles) with trilinear $f(w)$ and the corresponding solutions for the QC model (14) (solid curves) evaluated for (a) $\alpha = 0.5$; (b) $\alpha = 2$. Here $\beta = 6$, $\delta = 0.4$, $w_c = 1$. The background strain is $w_+ = 0.5$, and the corresponding superkink velocity is $V_{SK} = 1.72044$ in (a) and $V_{SK} = 1.76613$ in (b).

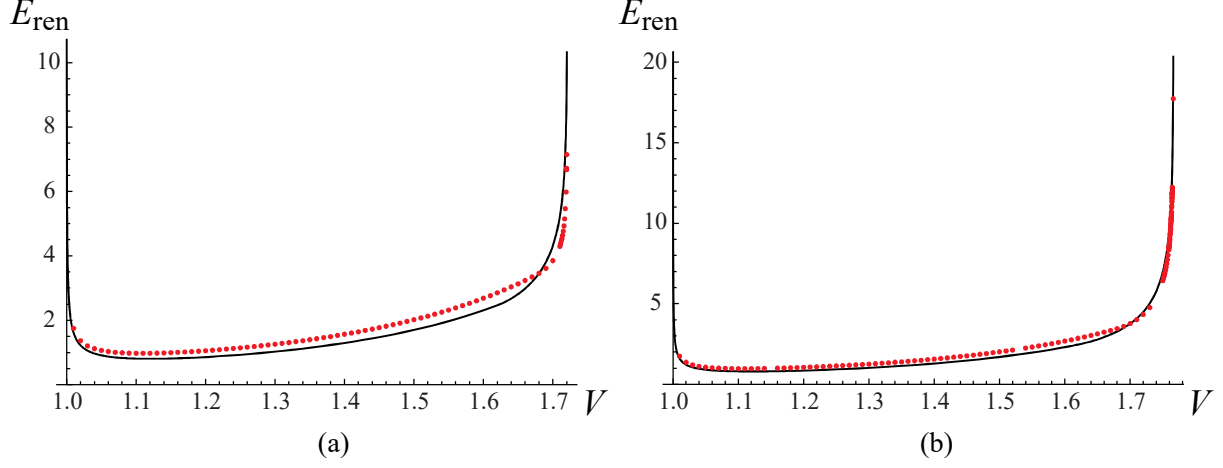


Figure 9: Renormalized energy E_{ren} given by (54) as a function of velocity V for tensile SW solutions of the discrete problem (8) (circles) with trilinear $f(w)$ and the corresponding energy (55) for the QC model (14) (solid curves) evaluated for (a) $\alpha = 0.5$; (b) $\alpha = 2$. Here $\beta = 6$, $\delta = 0.4$, $w_c = 1$. The background strain is $w_+ = 0.5$, and the corresponding superkink velocity is $V_{\text{SK}} = 1.72044$ in (a) and $V_{\text{SK}} = 1.76613$ in (b).

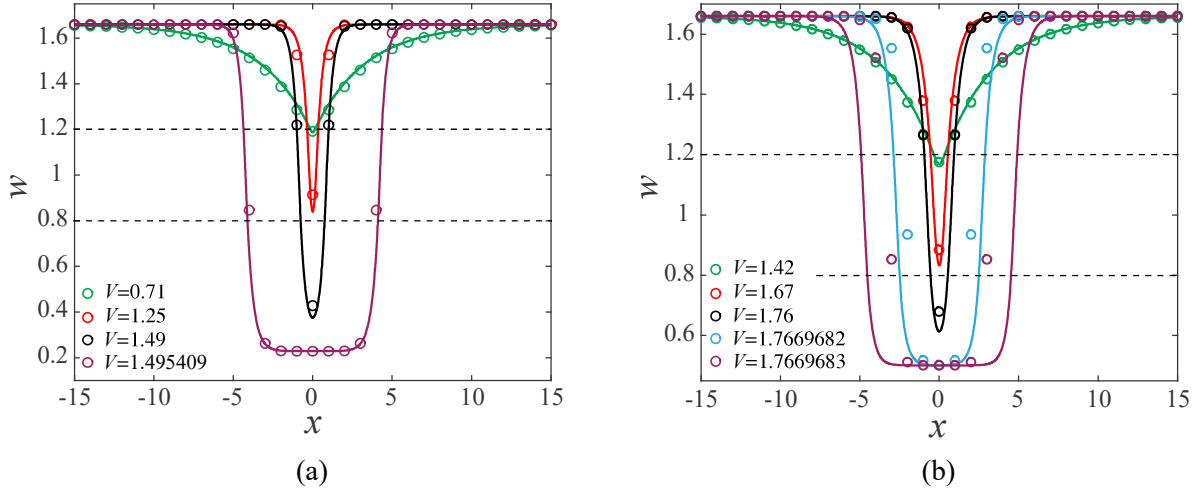


Figure 10: Compressive SW solutions $w_n(0) = w(n)$ of the discrete problem (8) (circles) with trilinear $f(w)$ and the corresponding solutions $w(x)$ for the QC model (14) (solid curves) evaluated at $t = 0$ for (a) $\alpha = 0.5$; (b) $\alpha = 2$. Here $\beta = 6$, $\delta = 0.4$, $w_c = 1$. The background strain is $w_+ = 1.66$, and the corresponding superkink velocity is $V_{\text{SK}} = 1.49541$ in (a) and $V_{\text{SK}} = 1.76697$ in (b).

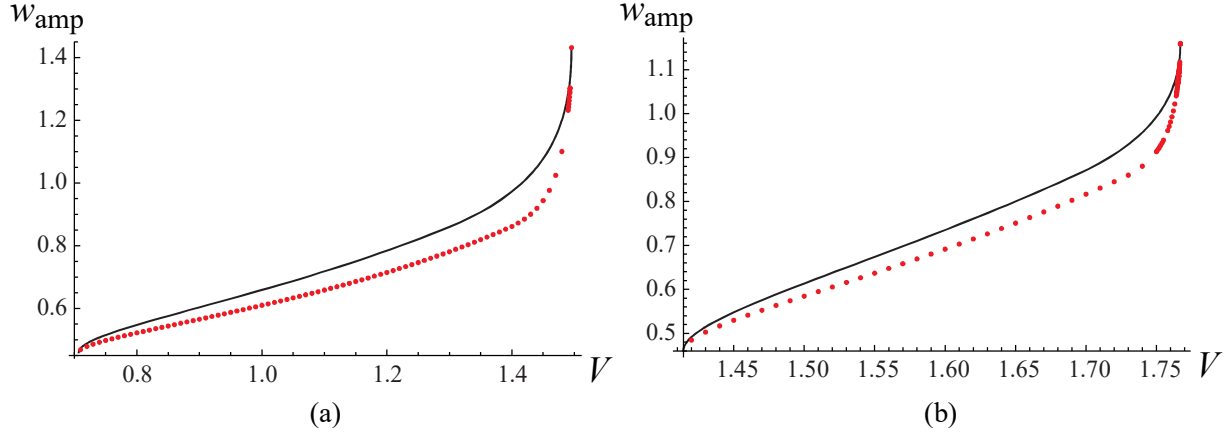


Figure 11: Amplitude as a function of velocity V for compressive SW solutions of the discrete problem (8) (circles) with trilinear $f(w)$ and the corresponding solutions for the QC model (14) (solid curves) for (a) $\alpha = 0.5$; (b) $\alpha = 2$. Here $\beta = 6$, $\delta = 0.4$, $w_c = 1$. The background strain is $w_+ = 1.66$, and the corresponding superkink velocity is $V_{\text{SK}} = 1.49541$ in (a) and $V_{\text{SK}} = 1.76697$ in (b).

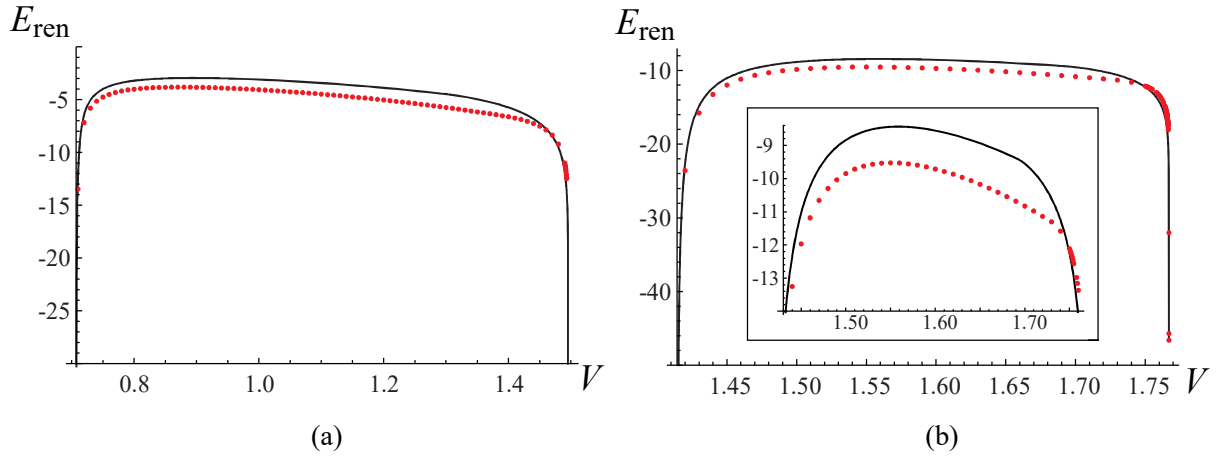


Figure 12: Renormalized energy as a function of velocity V for compressive SW solutions of the discrete problem (8) (circles) with trilinear $f(w)$ and the corresponding solutions of the QC model (14) (solid curves) for (a) $\alpha = 0.5$; (b) $\alpha = 2$. The inset in (b) zooms in on the upper energy range. Here $\beta = 6$, $\delta = 0.4$, $w_c = 1$. The background strain is $w_+ = 1.66$, and the corresponding superkink velocity is $V_{\text{SK}} = 1.49541$ in (a) and $V_{\text{SK}} = 1.76697$ in (b).

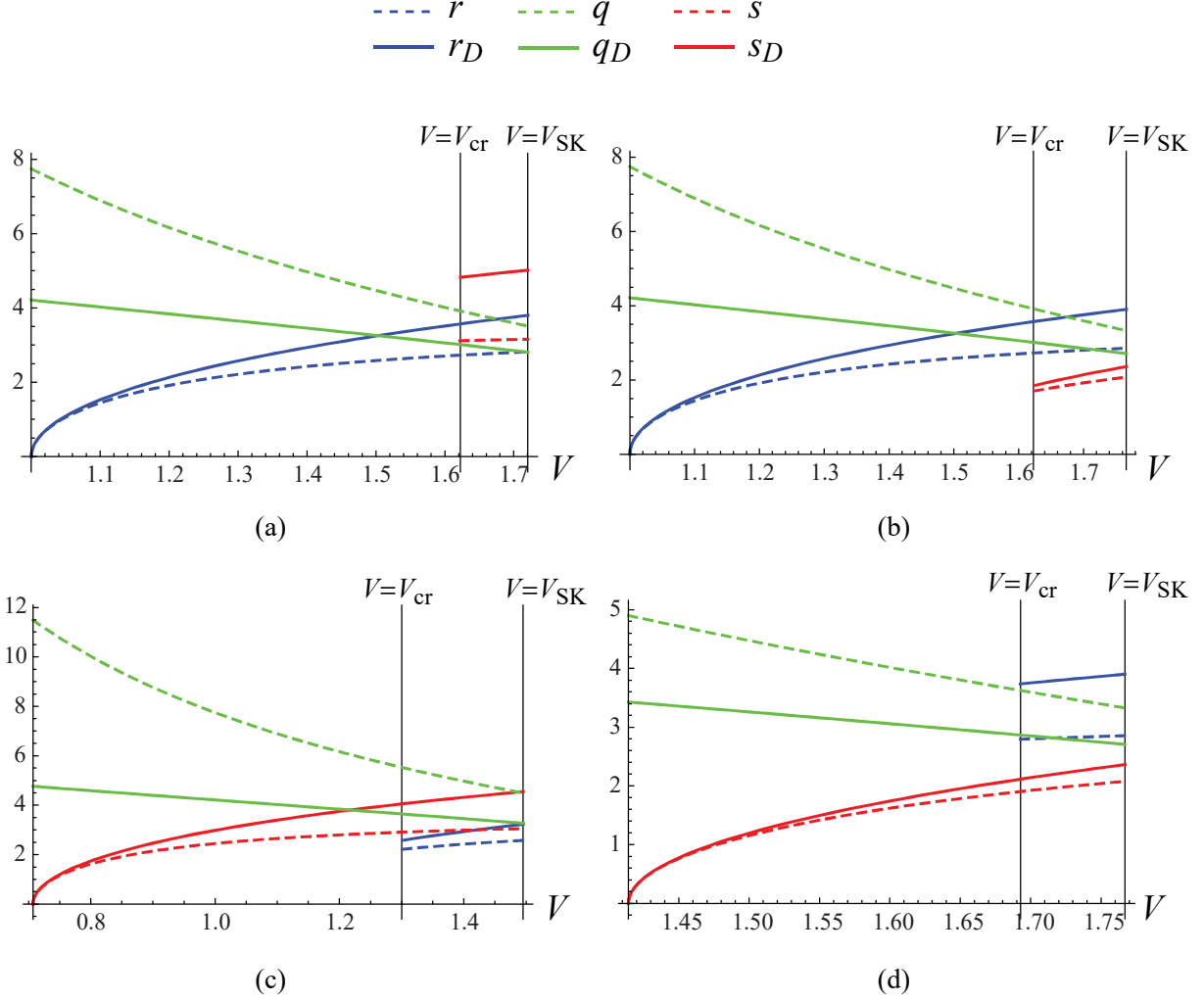


Figure 13: Roots r , q , s (dashed curves) contributing to the QC SW solutions and the corresponding characteristic roots r_D , q_D , s_D (solid curves) for the discrete problem (see the main text for details), in the respective velocity ranges at (a) $\alpha = 0.5$, $w_+ = 0.5$; (b) $\alpha = 2$, $w_+ = 0.5$; (c) $\alpha = 0.5$, $w_+ = 1.66$; (d) $\alpha = 2$, $w_+ = 1.66$. The vertical lines mark the corresponding V_{cr} and V_{SK} . Here $\beta = 6$, $\delta = 0.4$, $w_c = 1$. Tensile SW solutions corresponding to panels (a) and (b) are shown in Fig. 7-9, and compressive SW solutions corresponding to panels (c) and (d) are shown in Fig. 10-12.

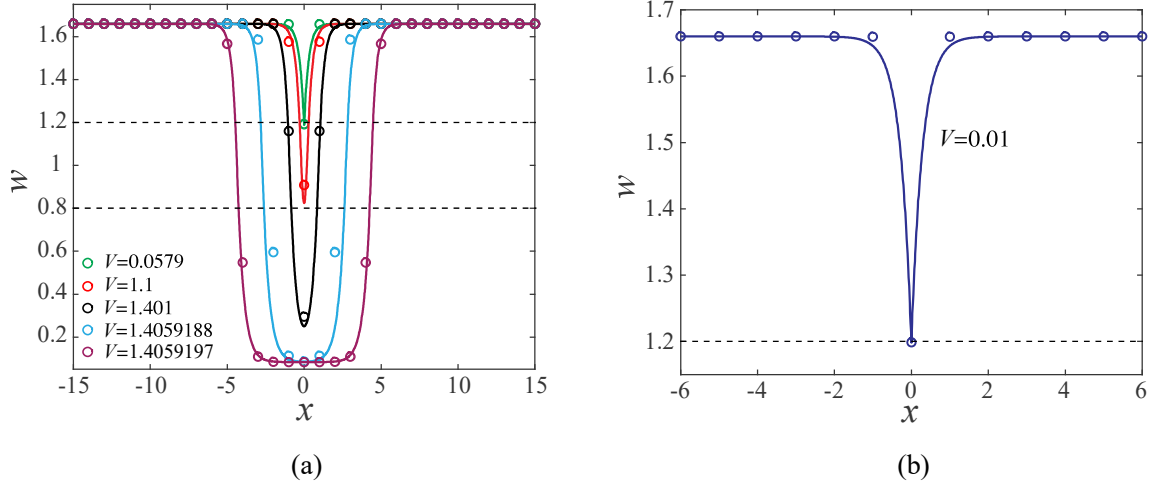


Figure 14: (a) Compressive SW solutions $w_n(0) = w(n)$ of the discrete problem (8) (circles) with trilinear $f(w)$ and the corresponding solutions $w(x)$ for the QC model (14) (solid curves) evaluated at $t = 0$ for $\alpha = 0$, $\beta = 6$, $\delta = 0.4$, $w_c = 1$. (b) The solutions at $V = 0.01$. The background strain is $w_+ = 1.66$, and the corresponding superkink velocity is $V_{SK} = 1.40592$.

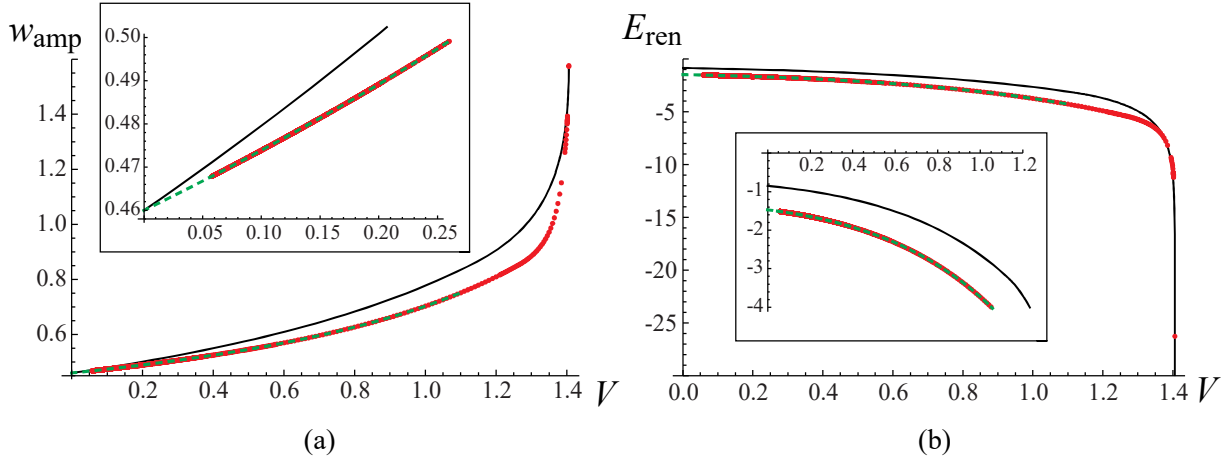


Figure 15: (a) Amplitude and (b) renormalized energy as functions of velocity V for compressive SW solutions of the discrete problem (8) (circles) with trilinear $f(w)$ and the corresponding solutions for the QC model (14) (solid curves) for $\alpha = 0$. The dashed green curves correspond to the exact small-velocity solution (56)-(58). Insets zoom in around smaller velocity values. Here $\beta = 6$, $\delta = 0.4$, $w_c = 1$. The background strain is $w_+ = 1.66$, and the corresponding superkink velocity is $V_{SK} = 1.40592$.

Solving these and imposing the symmetry conditions $\ddot{w}_0(0) = 0$, $w_1(0) = w_{-1}(0)$, $\dot{w}_1(0) = -\dot{w}_{-1}(0)$ and the boundary condition $w_n \rightarrow w_+$ as $|n| \rightarrow \infty$, we obtain

$$\begin{aligned} w_0 &= A \cos(\sqrt{2\beta}t) + w_c + \delta/2, & w_{\pm 1} &= -(A/2) \cos(\sqrt{2\beta}t) \pm Bt + C, \\ w_n &= w_+, & n &\leq -2, \quad n \geq 2 \end{aligned} \quad (56)$$

for $t \leq T_1$. The condition $w_0(T_1) = w_c + \delta/2$ then yields $A \cos(\sqrt{2\beta}T_1) = 0$, and since A must be nonzero, we deduce that $\sqrt{2\beta}T_1 = \pi/2$, which yields

$$T_1 = \frac{\pi}{2\sqrt{2\beta}}.$$

Since $T_1 < T/2$, we have

$$0 < V < \frac{\sqrt{2\beta}}{\pi}.$$

For $T_1 < t < T_2$, all strains are in the upper linear regime and satisfy $\ddot{w}_n = 0$. Together with continuity of w_n and \dot{w}_n at $t = T_1$ this yields

$$\begin{aligned} w_0 &= w_c + \delta/2 - \sqrt{2\beta}A(t - T_1), & w_{\pm 1} &= C \pm Bt + \sqrt{\beta/2}A(t - T_1), \\ w_n &= w_+, & n &\leq -2, \quad n \geq 2 \end{aligned} \quad (57)$$

for $T_1 \leq t \leq T - T_1$. For $T_2 < t \leq T$, we have

$$\ddot{w}_1 + 2\beta w_1 = \beta(2w_c + \delta), \quad \ddot{w}_{0,2} = \beta(w_1(t) - w_c) - \beta\delta/2, \quad \ddot{w}_n = 0, \quad n \leq -1, \quad n \geq 3.$$

Solving these and recalling that $w_n(0) = w_{n+1}(T)$ and $\dot{w}_n(0) = \dot{w}_{n+1}(T)$, we obtain

$$\begin{aligned} w_1 &= A \cos(\sqrt{2\beta}(t - T)) + w_c + \delta/2, & w_{0,2} &= -(A/2) \cos(\sqrt{2\beta}(t - T)) \mp B(t - T) + C, \\ w_n &= w_+, & n &\leq -1, \quad n \geq 3 \end{aligned} \quad (58)$$

for $T - T_1 \leq t \leq T$. Continuity of w_n and \dot{w}_n at $t = T_2$ then leads to three independent conditions

$$\begin{aligned} C + B(T - T_1) + \sqrt{\beta/2}A(T - 2T_1) &= w_c + \delta/2, \\ C - B(T - T_1) + \sqrt{\beta/2}A(T - 2T_1) &= w_+, \\ \sqrt{\beta/2}A - B &= 0, \end{aligned}$$

which yield

$$B = -\frac{w_+ - w_c - \delta/2}{2(T - T_1)} = \sqrt{\frac{\beta}{2}}A, \quad C = w_+ - \frac{w_+ - w_c - \delta/2}{2(T - T_1)}T_1.$$

In particular, at $t = 0$ we obtain

$$w_0 = w_c + \frac{\delta}{2} - \frac{w_+ - w_c - \delta/2}{\sqrt{2\beta}(T - T_1)}, \quad w_{\pm 1} = w_+ - \frac{w_+ - w_c - \delta/2}{2\sqrt{2\beta}(T - T_1)} \left(\frac{\pi}{2} - 1 \right), \quad w_n = w_+, \quad |n| \geq 2 \quad (59)$$

and

$$\dot{w}_{\pm 1} = \mp \frac{w_+ - w_c - \delta/2}{2(T - T_1)}, \quad \dot{w}_0 = 0, \quad \dot{w}_n = 0, \quad |n| \geq 2.$$

Together with $v_n = -Vw_+ + \sum_{k=-\infty}^n \dot{w}_k$ the latter yield

$$v_{-1} = v_0 = -Vw_+ + \frac{w_+ - w_c - \delta/2}{2(T - T_1)}, \quad v_n = -Vw_+, \quad n \leq -2, \quad n \geq 1. \quad (60)$$

Using (59) and (60), we obtain the renormalized energy (54) given by

$$E_{\text{ren}}^{\text{D}}(V) = \left(\frac{w_+ - w_c - \delta/2}{2(T - T_1)} - Vw_+ \right)^2 - V^2 w_+^2 + \Phi(w_0) + 2\Phi(w_1) - 3\Phi(w_+).$$

The amplitude and renormalized energy of the obtained solution are shown by the dashed green curves in Fig. 15. One can see that this solution differs from the one for the QC model even at very small velocities, as illustrated in Fig. 14(b). Indeed, in the limit $V \rightarrow 0$ ($T \rightarrow \infty$), we have $w_0 \rightarrow w_c + \delta/2$, $w_n \rightarrow w_+$, $n \neq 0$, $v_n \rightarrow 0$ for all n , and thus

$$E_{\text{ren}}^{\text{D}}(0) = \Phi(w_0) - \Phi(w_+) = -(w_c - \delta/2 + \beta\delta)(w_+ - w_c - \delta/2).$$

For comparison, we recall in the QC model the zero-velocity limit is given by (50). Thus the limiting renormalized energy (55) is given by

$$E_{\text{ren}}^{\text{QC}}(0) = \int_{-\infty}^{\infty} (\Phi(w(x)) - \Phi(w_+)) dx = -\frac{1}{\sqrt{3}}(w_c - \delta/2 + \beta\delta)(w_+ - w_c - \delta/2) = \frac{1}{\sqrt{3}}E_{\text{ren}}^{\text{D}}(0).$$

In addition to the quantitative difference between discrete and QC solutions that persists to the sonic limit, it is important to note that for the discrete solution $w(\xi) - w_+$ is *compact*, while its QC counterpart features exponential decay to the background strain.

5 Stability of superkink solutions

We tested stability of the superkinks by conducting numerical simulations of (2) on a finite chain. In the first set of simulations, we extracted initial conditions from the computed superkink solutions and used the corresponding fixed boundary conditions. These simulations resulted in steady propagation of the traveling wave with velocity that remained within $O(10^{-8})$ or less from the prescribed value for the entire range of velocities, suggesting that the traveling waves are at least long-lived and likely stable.

The second set of simulations was conducted on a chain with L particles using free-end boundary conditions and Riemann initial data

$$w_n(0) = \begin{cases} w^l, & 1 \leq n \leq L/2 \\ w^r, & L/2 + 1 \leq n \leq L \end{cases}, \quad \dot{w}_n(0) = 0, \quad n = 1, \dots, L. \quad (61)$$

The size L of the chain was chosen sufficiently large to avoid any boundary effects.

Some results of simulations with Riemann data (61) are shown in Fig. 16 and Fig. 17, where we fix $\beta = 6$, $\delta = 0.4$, $w_c = 1$ and vary α , w^l and w^r . Typical scenario, where a superkink propagating to the right is trailed by linear dispersive shock waves moving in opposite directions with velocities $\pm\sqrt{\alpha}$, is shown in Fig. 16(a) ($\alpha = 2$, $w^l = 4$, $w^r = 0.7$) and Fig. 16(b) ($\alpha = 0.5$, $w^l = 6$, $w^r = 0.3$). The velocity of the superkink is $V_{\text{SK}} = 2.0901$ in Fig. 16(a) and $V_{\text{SK}} = 1.5404$ in Fig. 16(b), in agreement with (35) when $w_+ = w^r$, $V = V_{\text{SK}}$ for each case. A more complex dynamics is observed in Fig. 16(c) ($\alpha = 0.5$, $w^l = 6$, $w^r = 0$). In this case two solitary waves form behind the left dispersive shock wave and eventually move to the left with velocities $V_1 = -0.8092$ and $V_2 = -0.792$, while a superkink moves to the right (ahead of another dispersive shock wave) with velocity $V = 1.39$, again consistent with (35). At $\alpha = 0.5$, $w^l = 8$, $w^r = -1$, the dynamics, shown in Fig. 16(d), is similar but there are four solitary waves moving to the left, with velocities $V_1 = -0.7913$, $V_2 = -0.7891$, $V_3 = -0.792$, $V_4 = -0.7514$ near the end of the simulation, while a superkink propagates to the right with $V_{\text{SK}} = 1.1926$.

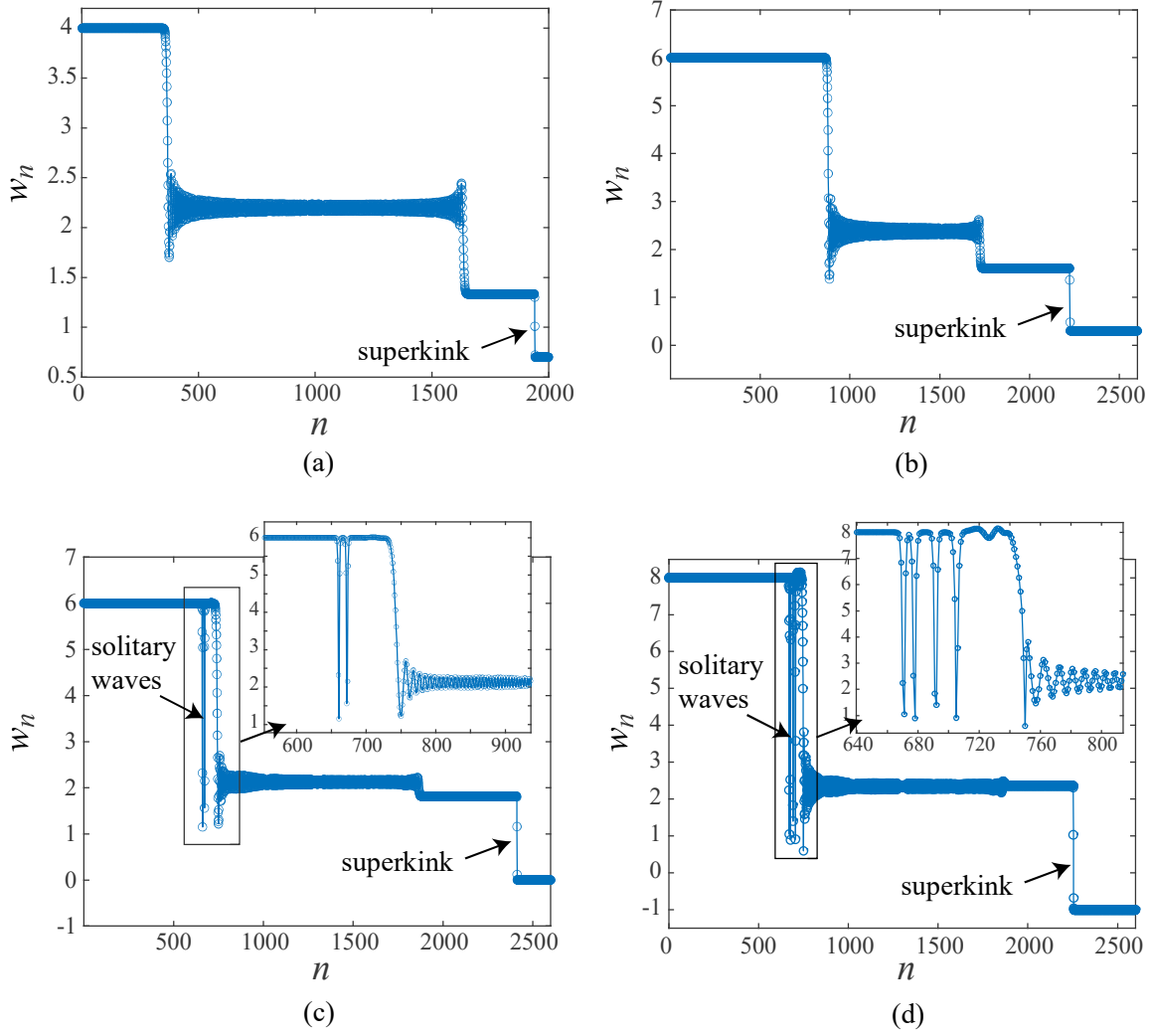


Figure 16: Snapshots of strain profiles in simulations with Riemann initial data (61): (a) $\alpha = 2$, $w^l = 4$, $w^r = 0.7$, $L = 2000$, $t = 450$; (b) $\alpha = 0.5$, $w^l = 6$, $w^r = 0.3$, $L = 2600$, $t = 600$; (c) $\alpha = 0.5$, $w^l = 6$, $w^r = 0$, $L = 2600$, $t = 800$; (d) $\alpha = 0.5$, $w^l = 8$, $w^r = -1$, $L = 2600$, $t = 800$. Here $\beta = 6$, $\delta = 0.4$, $w_c = 1$.

The most interesting dynamics takes place in the case $\alpha = 0$, as illustrated in Fig. 17(a,b), where $w^l = 6$ and $w^r = 0.3$. In this case of inelastic red linear regime, we see a superkink propagating with $V_{SK} = 1.5263$, in agreement with (35). Behind the superkink there is another transition front that moves to the left and connects the constant strain w^l to a periodic train of solitary waves. The solitary wave train in this dispersive structure, known as a Whitham shock [Sprenger and Hoefer, 2020], is spreading, with the left edge (the transition front) moving with velocity $V_L = -0.3415$, while its right edge propagates with $V_R = 1.5022$, trailing the superkink. Similar dynamics is observed when we set $w^l = -0.75$, while keeping all other parameters the same; see Fig. 17(c,d). In this case we have $V_L = -0.5003$, $V_R = 1.1797$, $V_{SK} = 1.2018$. The corresponding space-time evolution is shown in Fig. 18. While supporting stability of superkinks, these results also reveal the interesting phenomenon of Whitham shocks that, to our knowledge, have not been previously observed for the FPU system.

6 Stability of solitary wave solutions

To investigate the linear stability of the obtained SW solutions in the case $\alpha > 0$, we follow the approach of Cuevas-Maraver et al. [2017], Xu et al. [2018] and Vainchtein et al. [2020] and use Floquet analysis that exploits periodicity-modulo-shift (51) of the traveling wave solutions. Substituting $w_n(t) = \hat{w}_n(t) + \epsilon y_n(t)$ into (2), where $\hat{w}_n(t) = w(n - Vt)$ is the traveling wave solution, and considering $O(\epsilon)$ terms, we obtain the governing equations for the linearized problem:

$$\ddot{y}_n = f'(\hat{w}_{n+1})y_{n+1} - 2f'(\hat{w}_n)y_n + f'(\hat{w}_{n-1})y_{n-1}. \quad (62)$$

The Floquet multipliers μ for this problem are the eigenvalues of the monodromy matrix \mathcal{M} defined by

$$\begin{bmatrix} \{y_{n+1}(T)\} \\ \{\dot{y}_{n+1}(T)\} \end{bmatrix} = \mathcal{M} \begin{bmatrix} \{y_n(0)\} \\ \{\dot{y}_n(0)\} \end{bmatrix}. \quad (63)$$

To obtain \mathcal{M} , we compute the fundamental solution matrix $\Psi(T)$, which maps $[\{y_n(0)\}, \{\dot{y}_n(0)\}]^T$ onto $[\{y_n(T)\}, \{\dot{y}_n(T)\}]^T$, $n = -N/2, \dots, N/2 - 1$, for the first-order linear system equivalent to (62). We use periodic boundary conditions $y_{N/2}(t) = y_{-N/2}(t)$, $y_{-N/2-1}(t) = y_{N/2-1}(t)$, which is justified by the fact that for solitary waves the values $f'(\hat{w}_n)$ at the two ends of the chain have the same constant value (note, however, that this is not the case for superkinks unless $\alpha = 1$). Due to the piecewise linear nature of (3), the computation of the fundamental solution matrix $\Psi(T)$ involves determining the times instances T_i , $i = 1, \dots, k$, at which one of the nodes switches from one linear regime to another over the time interval $[0, T]$. This yields

$$\Psi(T) = e^{-\mathbf{C}_{k+1}(T-T_k)} e^{-\mathbf{C}_k(T_k-T_{k-1})} \dots e^{-\mathbf{C}_2(T_2-T_1)} e^{-\mathbf{C}_1 T_1},$$

where \mathbf{C}_i has the block form

$$\mathbf{C}_i = \begin{bmatrix} \mathbf{O} & \mathbf{I} \\ \mathbf{A}_i & \mathbf{O} \end{bmatrix}, \quad i = 1, \dots, k+1$$

involving the $N \times N$ identity matrix \mathbf{I} , the $N \times N$ zero matrix \mathbf{O} and $N \times N$ matrices \mathbf{A}_i that contain the coefficients for the corresponding linear system and have a tridiagonal structure extended to the upper right and lower left corner entries according to the periodic boundary conditions. We then shift the rows of $\Psi(T)$ up by one row in the two parts of the matrix corresponding to y_n and \dot{y}_n , respectively, with the last row in each part replaced by the first, obtaining \mathcal{M} in (63). We

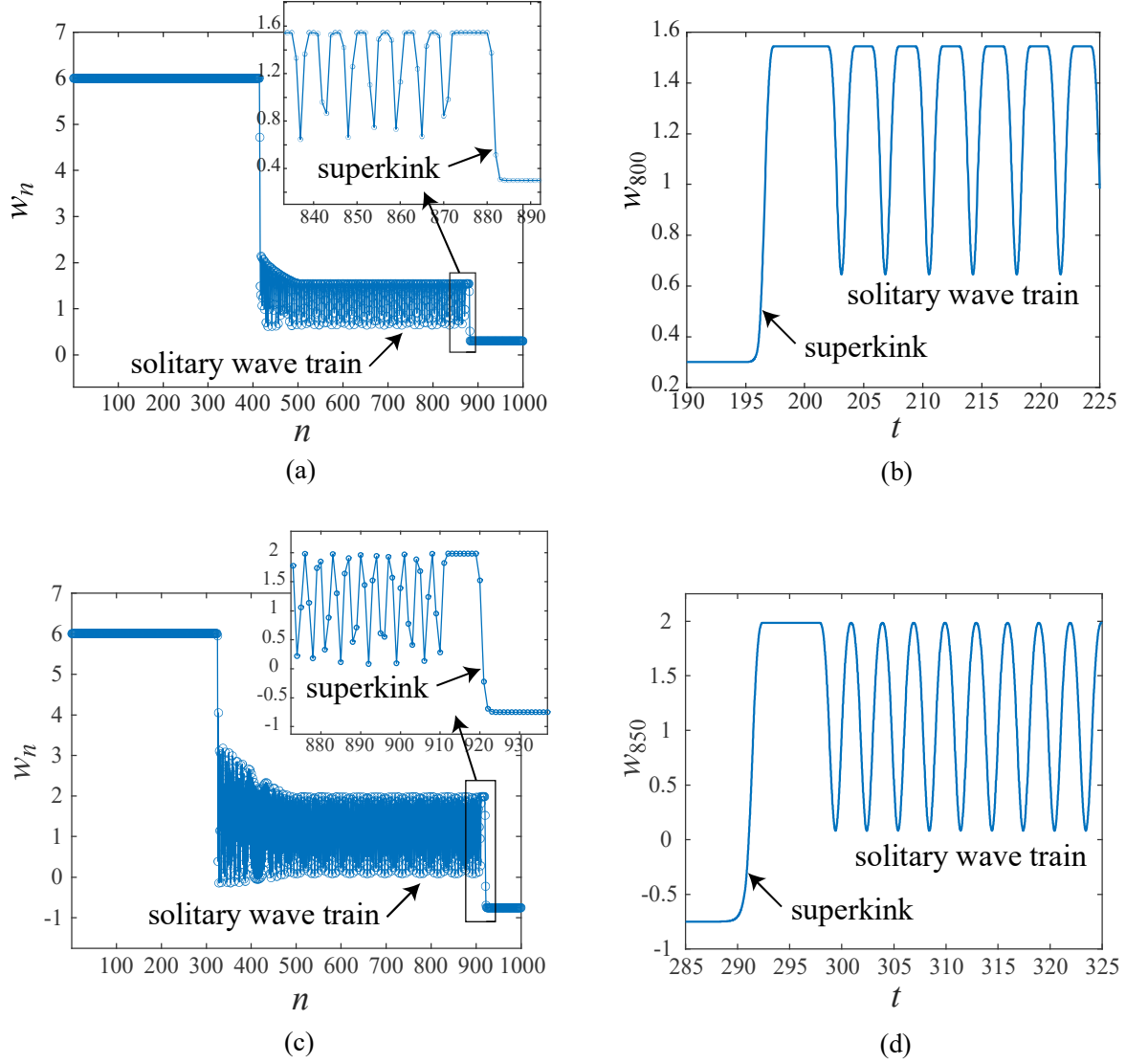


Figure 17: (a) Snapshot of strain profiles in simulations with Riemann initial data (61) and $\alpha = 0$, $w^l = 6$, $w^r = 0.3$, $L = 1000$, $t = 250$; (b) time evolution of $w_{800}(t)$ for the simulation in (a); (c) snapshot of strain profiles in simulations with Riemann initial data (61) and $\alpha = 0$, $w^l = 6$, $w^r = -0.75$, $L = 1000$, $t = 350$; (d) time evolution of $w_{850}(t)$ for the simulation in (c). Here $\beta = 6$, $\delta = 0.4$, $w_c = 1$.

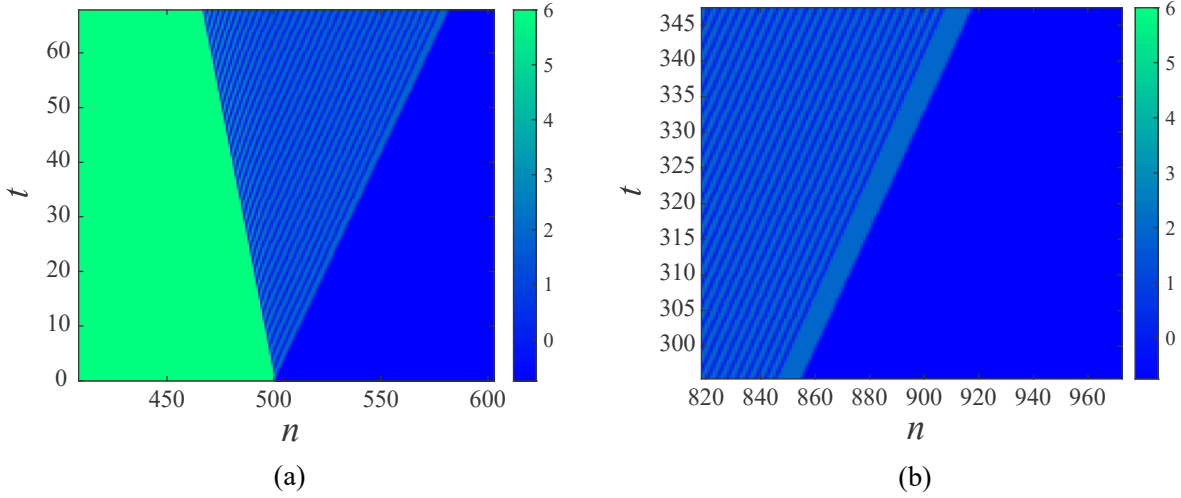


Figure 18: Space-time evolution of strain in simulations with Riemann initial data (61): (a) formation of the superkink front and SW train early in the simulation; (b) evolution near the end of the simulation, zoomed in around the superkink front. Here $\alpha = 0$, $\beta = 6$, $\delta = 0.4$, $w_c = 1$, $w^l = 6$, $w^r = -0.75$, $L = 1000$.

note that this procedure relies on the periodic boundary conditions, which, as mentioned above, are justified for solitary waves but in general not for superkinks.

The Floquet multipliers are related to the eigenvalues λ of the linearization operator via $\mu = e^{\lambda/V}$, and thus $|\mu| > 1$ ($\text{Re}(\lambda) > 0$) corresponds to instability. The Hamiltonian nature of the problem means that there are quadruples of non-real Floquet multipliers, i.e., if μ is a multiplier, then so are $\bar{\mu}$, $1/\mu$ and $1/\bar{\mu}$, while the real multipliers come in pairs μ and $1/\mu$. Linear stability thus requires that all Floquet multipliers lie on the unit circle: $|\mu| = 1$.

The resulting maximum modulus of Floquet multipliers as a function of V is shown in Fig. 19.

In each case, for sufficiently small velocities the maximum-modulus multiplier is real $\mu > 1$ (red segments in Fig. 19) and corresponds to exponential instability mode. As velocity increases, the real multiplier μ outside the unit circle and the companion real multiplier $1/\mu$ inside the unit circle move toward the unit circle and join it at the threshold velocity $V = V_*$. This is illustrated in Fig. 20 for the case $\alpha = 2$, $w_+ = 0.5$, where we see the two real multipliers approach the unit circle as velocity is increased from 1.01 (panel (a)) to 1.05 (panel (b)), slightly below $V_* \approx 1.064$. Starting with velocities slightly below V_* , the maximum-modulus multipliers are complex and correspond to mild instability modes similar to those observed by Marín and Aubry [1998], Xu et al. [2018] and Vainchtein and Truskinovsky [2024]. Since their magnitude decreases as the chain size is increased, these mild instabilities appear to be a spurious artifact due to the finite chain size. An example is shown in Fig. 20(c,d). Direct numerical simulations initiated by solitary waves with velocities $V > V_*$ show steady propagation of the waves and suggest their effective stability, as illustrated in Fig. 21.

For solitary waves that tend to zero at infinity, the onset of exponential instability associated with $\mu > 1$ typically corresponds to threshold velocities at which their energy changes monotonicity [Friesecke and Pego, 2004, Cuevas-Maraver et al., 2017, Xu et al., 2018]. In this case, the onset of instability occurs prior to the change in monotonicity of the renormalized energy (54), which takes place at $V > V_*$, as can be seen in Fig. 9 and Fig. 12. It is possible that another relevant quantity changes monotonicity at $V = V_*$.

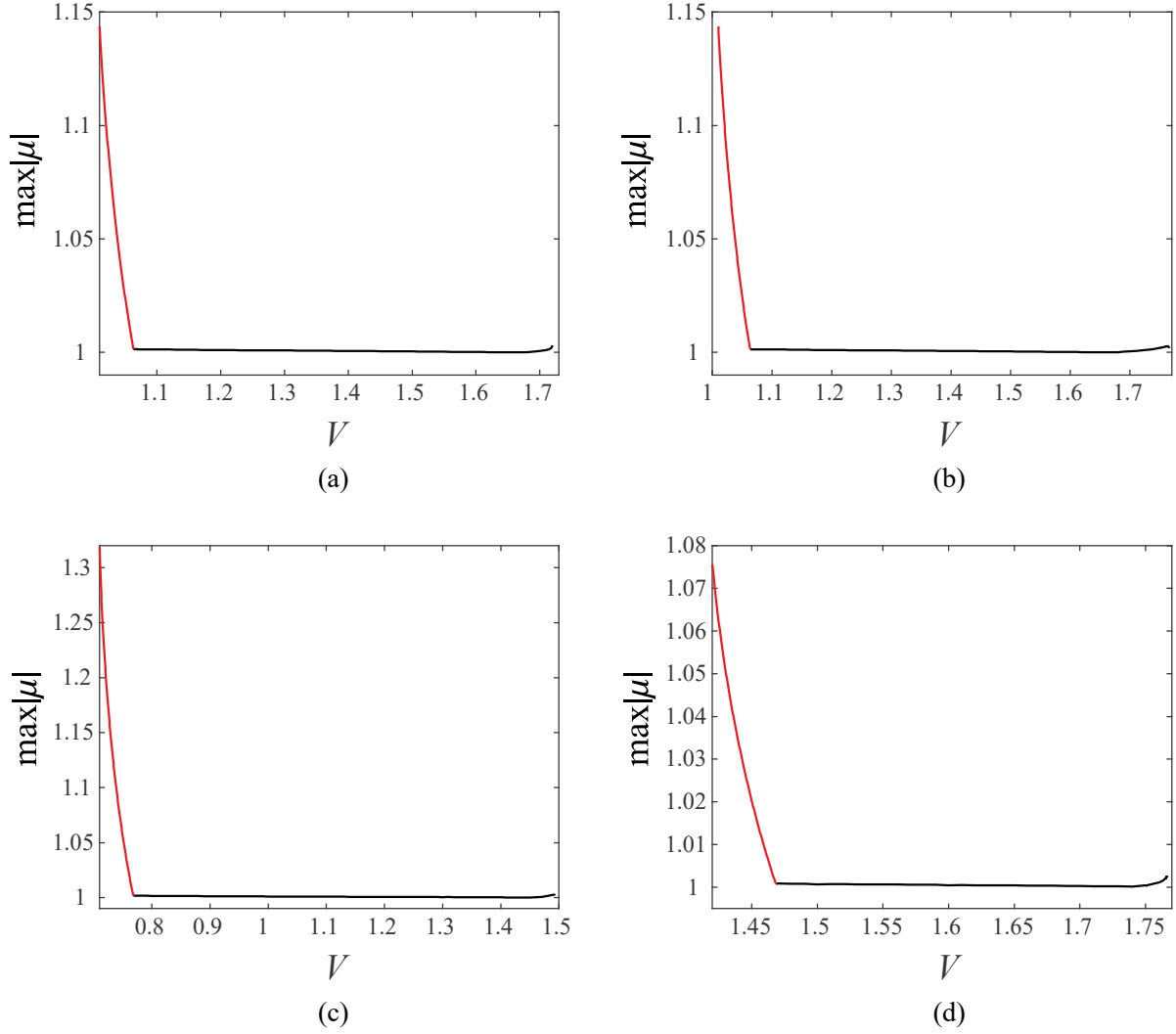


Figure 19: Maximum modulus of Floquet multipliers for (a) tensile waves with $w_+ = 0.5$, $\alpha = 0.5$; (b) tensile waves with $w_+ = 0.5$, $\alpha = 2$; (c) compressive waves with $w_+ = 1.66$, $\alpha = 0.5$; (d) compressive waves with $w_+ = 1.66$, $\alpha = 2$. The red segments correspond to real multiplier $\mu > 1$. Here $\beta = 6$, $\delta = 0.4$, $w_c = 1$, and the corresponding values of the superkink velocity are $V_{\text{SK}} = 1.72044$ in (a), $V_{\text{SK}} = 1.76613$ in (b), $V_{\text{SK}} = 1.49541$ in (c) and $V_{\text{SK}} = 1.76697$ in (d). Mild oscillatory instabilities ($\max|\mu| > 1$) along the black portion of the curves appear to be an artifact due to the finite chain size.

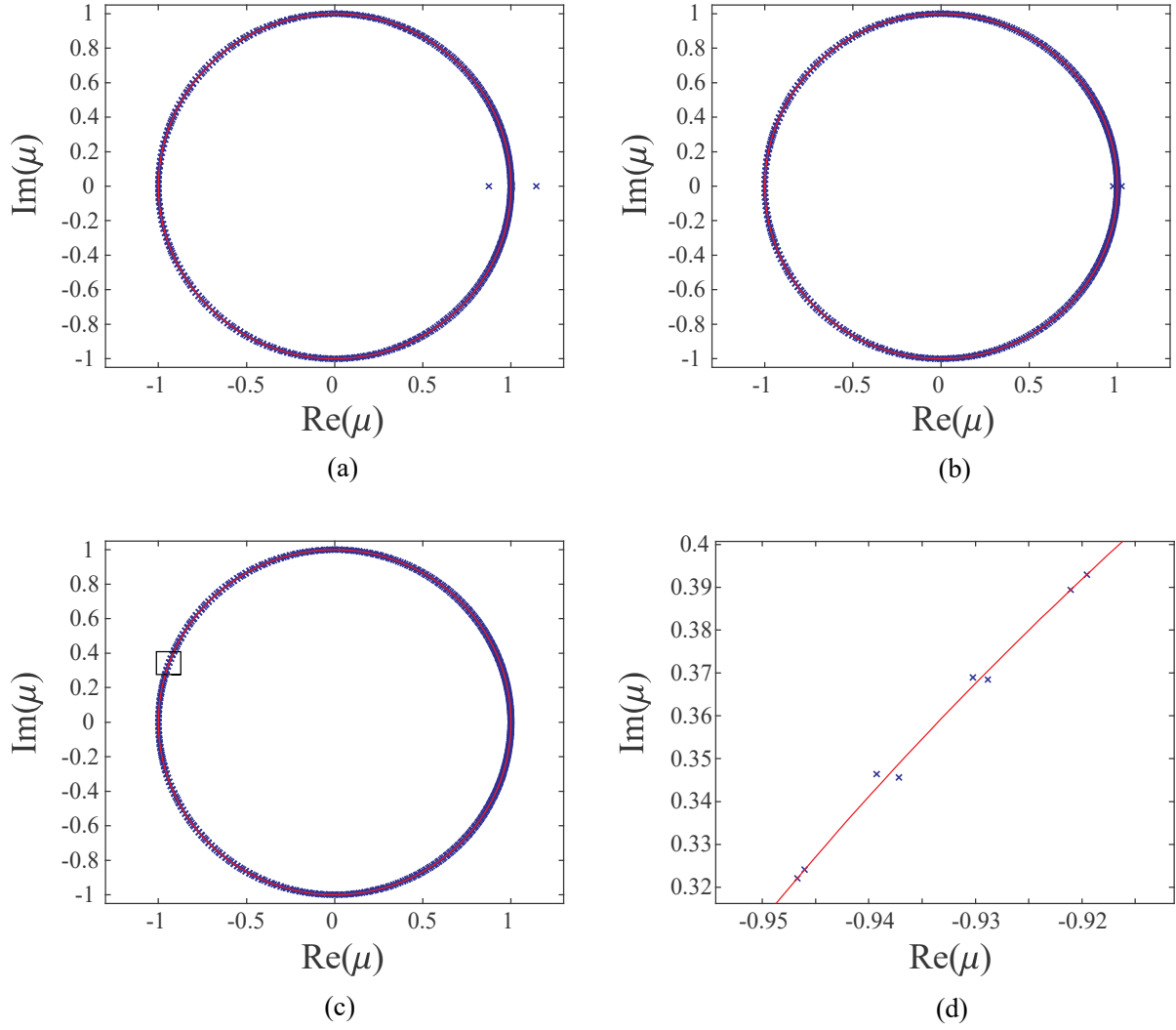


Figure 20: Floquet multipliers (blue crosses) for tensile solitary waves at (a) $V = 1.01$; (b) $V = 1.05$; (c) $V = 1.14$; (d) $V = 1.14$, zooming inside the rectangle in panel (c). The unit circle is marked in red. Here $\alpha = 2$, $w_+ = 0.5$, $\beta = 6$, $\delta = 0.4$, $w_c = 1$.

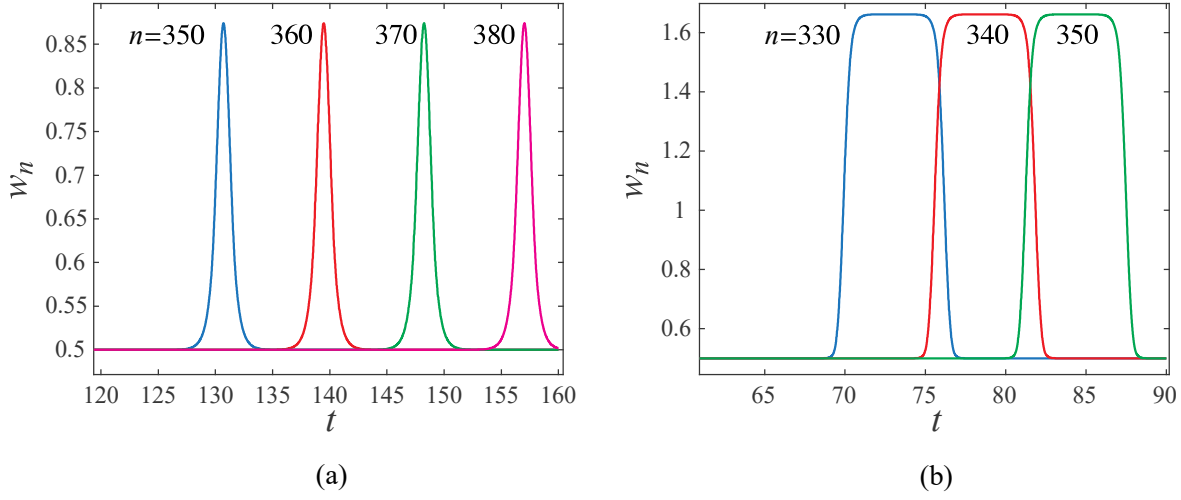


Figure 21: Strain evolution in numerical simulations initiated by computed solitary waves with (a) $V = 1.14$; (b) $V = 1.7661272$. Here $\alpha = 2$, $w_+ = 0.5$, $\beta = 6$, $\delta = 0.4$, $w_c = 1$.

To explore the consequences of the instability at $V < V_*$, we ran numerical simulations initiated by an unstable solitary waves perturbed along the corresponding eigenmode. A typical scenario for ensuing dynamic evolution is shown in Fig. 22, where the simulation was initiated by the perturbed unstable compressive wave with velocity $V = 0.72$ below the threshold value $V_* \approx 0.7685$ at $\alpha = 0.5$, $w_+ = 1.66$ (see Fig. 19(c) for the corresponding maximum-modulus Floquet multipliers). One can see formation of an apparently stable solitary wave with $V = 0.8288$ above the threshold followed by dispersive wave that propagates with lower (sonic) speed.

Stability of compressive waves in the degenerate case $\alpha = 0$, shown in Fig. 14, was investigated numerically. Simulation results suggest stable propagation of solitary waves in the entire velocity range $0 < V < V_{SK}$.

7 Concluding remarks

In this paper, we considered the FPU system with trilinear force-elongation relation. It was chosen to be of generally asymmetric soft-hard-soft type, and the resulting mechanical behavior can be classified as hardening-softening. We showed that in addition to the classical finite-amplitude, spatially localized solitary waves, this model exhibits supersonic kinks (superkinks) and finite-amplitude, spatially delocalized flat-top solitary waves which acquire the structure of a kink-antikink bundle when their velocity tends to the kink limit. Exploiting the periodic-modulo-shift property of traveling waves, we computed these solutions as fixed points of the corresponding nonlinear map. In a particularly interesting degenerate case when the elastic modulus of one of the soft regimes is zero, we obtained exact solutions for sufficiently slow solitary waves.

Floquet analysis of solitary waves in the non-degenerate case shows that near-sonic waves are unstable when their velocity is below a certain threshold. Perturbation along the corresponding eigenmode led to the formation of a stable wave with velocity above the threshold. Stability of these and other solutions was also confirmed by direct numerical simulations initiated by the computed traveling waves and piecewise constant Riemann data. In the degenerate case, Riemann simulations revealed emergence of Whitham shocks involving periodic train of solitary waves.

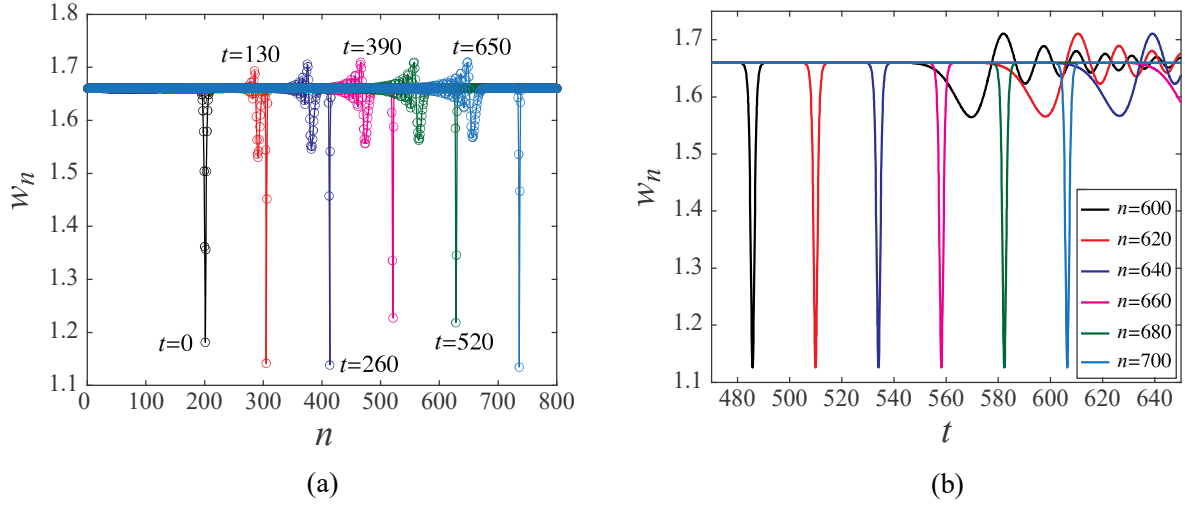


Figure 22: (a) Snapshots of strain profiles and (b) $w_n(t)$ at different fixed n for the dynamic evolution initiated by an unstable compressive wave propagating with velocity $V = 0.72 < V_*$ at $\alpha = 0.5$ and $w = 1.66$, perturbed along the eigenmode corresponding to the real Floquet multiplier $\mu = 1.20795$. The dynamic evolution leads to the formation of compressive solitary wave with $V = 0.8288 > V_*$ followed by a sonic dispersive wave. Here $V_* \approx 0.7685$, $\delta = 0.4$, $\beta = 6$, $w_c = 1$.

To complement this picture, we analyzed in detail a QC approximation of the FPU problem, which introduces into the continuum model mixed space-time higher-order derivative term describing microinertia. Using this model, we derived explicit solutions for both solitary waves and superkinks. The analytical transparency of the QC model allowed us to examine in full detail the properties of the waves and the effect of asymmetry of the interaction force. Comparison of the obtained solutions with their discrete counterparts showed that the QC model captures the main effects qualitatively, and quantitative agreement exists near the superkink and, for the non-degenerate case, sonic limit. In the degenerate case the discrepancy between the discrete and QC model persists to the sonic limit of zero velocity.

Finally, we mention a potential application of the obtained results. It is known that persistent “particle-like” wave packets can be generated in mechanical metamaterials to transfer mechanical energy and communicate mechanical information [Bertoldi et al., 2017]. An important class of applications of such metamaterials involves autonomous locomotion. In particular, wave-driven robots, utilizing geometric phase transitions as internal mechanisms, are becoming a subject of intense research due to their adaptability to complex environments [Deng et al., 2020]. Moreover, a new paradigm in robotics is emerging in the form of a transition from movable machines to movable materials with self-propulsion interpreted as dynamics of uniform regions (or domains) bounded by coherently moving interfaces (domain walls) [Yasuda et al., 2020]. The idea is that constructive interplay between material nonlinearity and dispersion can lead to the emergence of such robust disturbances which would propagate with constant velocity and fixed profile. The corresponding nonlinear wave would be then associated with some functionality, as, for instance, in the case of peristaltic motion [Gorbushin and Truskinovsky, 2021]. The advantage of soft mechanical alternatives to rigid controlling actuators in otherwise soft crawling robots is obvious, and the main challenge is to learn to generate such programmable dynamic regimes. The delocalized flat-top solitary waves discussed in this work offer an example of stable nonlinear pulses which can be used to make the corresponding metamaterial crawl. In this respect our conclusion that the resulting

delocalized active pulses are necessarily supersonic is still realistic because in biologically relevant soft solids the acoustic speeds may be arbitrarily small. Note also that in this perspective our trilinear model can be interpreted as describing a material capable of generating active stresses [Gorbushin and Truskinovsky, 2019]. In the same sense, the flat-top solitary waves would imply dynamic passive-to-active transformations taking place in the front of a steadily moving pulse with the corresponding reverse transformation taking place in its rear.

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A Some technical results

The coefficients in (39) are found by imposing continuity of $w(\xi)$ and $w'(\xi)$. This yields

$$\begin{aligned} A &= (q(q(w_S - w_+) \cosh(sz_2) \sin(q(z_1 - z_2)) + s(w_S - w_- \\ &\quad + (w_+ - w_S) \cos(q(z_1 - z_2))) \sinh(sz_2))) / \mathcal{D}, \\ B &= (qr(w_S - w_+) \cos(qz_2) \cosh(sz_2) + s((w_S - w_-)(q \cos(qz_1) + r \sin(qz_1)) \\ &\quad - r(w_S - w_+) \sin(qz_2)) \sinh(sz_2))) / \mathcal{D}, \\ C &= (qr(w_S - w_+) \cosh(sz_2) \sin(qz_2) + s(r(w_S - w_+) \cos(qz_2) \\ &\quad - (w_S - w_-)(r \cos(qz_1) - q \sin(qz_1))) \sinh(sz_2))) / \mathcal{D}, \\ D &= (q(r(w_S - w_+) + (w_- - w_S)(r \cos(q(z_1 - z_2)) - q \sin(q(z_1 - z_2)))) / \mathcal{D}, \end{aligned} \tag{A.1}$$

where

$$\mathcal{D} = \sin(q(z_1 - z_2))(q^2 \cosh(sz_2) - rs \sinh(sz_2)) - q \cos(q(z_1 - z_2))(r \cosh(sz_2) + s \sinh(sz_2)).$$

Similarly, we find the coefficients in (47):

$$\begin{aligned} A &= q(q(w_S - w_+) \cosh(rz_2) \sin(q(z_1 - z_2)) + r(w_S - w_- \\ &\quad + (w_+ - w_S) \cos(q(z_1 - z_2))) \sinh(rz_2))) / \mathcal{D} \\ B &= (qs(w_S - w_+) \cos(qz_2) \cosh(rz_2) + r(w_S - w_-)(q \cos(qz_1) + s \sin(qz_1)) \\ &\quad + s(w_+ - w_S) \sin(qz_2)) \sinh(rz_2))) / \mathcal{D} \\ C &= (qs(w_S - w_+) \cosh(rz_2) \sin(qz_2) + r(s(w_S - w_+) \cos(qz_2) \\ &\quad + (w_- - w_S)(s \cos(qz_1) - q \sin(qz_1))) \sinh(rz_2))) / \mathcal{D} \\ D &= (q(s(w_S - w_+) + (w_- - w_S)(s \cos(q(z_1 - z_2)) - q \sin(q(z_1 - z_2)))) / \mathcal{D}, \end{aligned} \tag{A.2}$$

where

$$\mathcal{D} = \sin(q(z_1 - z_2))(q^2 \cosh(rz_2) - rs \sinh(rz_2)) - q \cos(q(z_1 - z_2))(s \cosh(rz_2) + r \sinh(rz_2)).$$

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