

# Circular Flight Patterns for Dronevision

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## ABSTRACT

This paper presents the design and implementation of a circular flight pattern for use by a 3D multimedia display, a Dronevision (DV). A DV uses drones configured with light sources, Flying Light Specks (FLSs), that are battery powered. The flight pattern enables a swarm of FLSs to enter an opening, granting them access to the charging coils to charge their batteries. We present two algorithms for an FLS to travel from its current coordinate to rendezvous with its assigned slot on the flight pattern, Shortest Distance (SD) and Fastest Rendezvous Time (FRT). In addition to quantifying the trade-off associated with these algorithms, we present an implementation using a swarm of Crazyflie drones with Vicon localization.

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### Holodecks Artifact Availability:

See <https://github.com/flyinglightspeck/CircularFlightPattern> for our open source software implementation and its data set. A video demonstration of our implementation using a swarm of Crazyflie drones with Vicon is available at <https://youtu.be/H60r2oTPB4k>.

## 1 INTRODUCTION

A Dronevision (DV) is a non-immersive 3D multimedia display detailed in [4]. A swarm of cooperating miniature drones configured with RGB light sources, Flying Light Specks (FLSs), to illuminate 3D point clouds and provide haptic interactions [30]. Figure 1 shows a DV illuminating a rose with a falling petal captured using a depth camera. The ceiling of the DV consists of wireless charging coils used to charge the battery of FLSs with a fixed flight time.

STAG [31] is an algorithm that continuously charges FLSs by staggering their battery flight time. It minimizes the number of charging stations. In addition, it minimizes the number of FLSs that are in transit from an illumination to the charging coils. This number may range from 55 to 218 FLSs with today's batteries and the Rose point cloud requiring 65K FLSs [31].

A challenge is how a swarm of tens of FLSs may fly through an opening of the DV to access the charging coils. This is non-trivial for several reasons. First, the system must consider downwash [8, 14, 26, 66, 87, 94], a region of instability caused by the flight of one FLS that adversely impacts other FLSs entering this region,

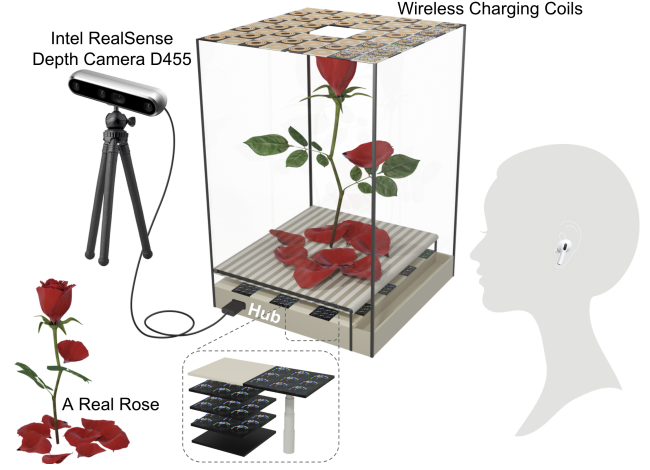


Figure 1: A Dronevision, DV [4].

e.g., loss of control or unpredictable behavior. Second, the flight pattern may be at an arbitrary angle  $\theta$  relative to the z-axis. Third, FLSs should occupy a moving slot in the flight pattern while minimizing either the traveled distance or the amount of time required to occupy the slot for arbitrary  $\theta$  angles. This paper presents the design, simulation, and implementation of a circular flight pattern. Figures 2a and 2b show a horizontal and a vertical orientation of a circular flight pattern accessing an opening. With 2a (2b), the opening at the top (back) provides FLSs with access to the charging coils on top (back) of the Dronevision.

*Definition 1.1.* A *flight pattern* is a formation consisting of a fixed number of slots where all slots maintain a general pattern or shape with a fixed distance between two consecutive slots. This is commonly termed a rigid formation [13, 81]. Slots travel at a fixed speed and in the same direction. Once an FLS occupied slot is below the opening, the occupying FLS flies through the opening and relinquishes its slot.

This paper focuses on circular flight patterns with a fixed radius  $R$ . The distance between the slots is dictated by downwash. For example, with quadrotor representing an FLS, its downwash is represented as a sphere with a fixed radius  $r$  [37, 50]. The sphere must be inclusive of the drone. We set the distance between two consecutive slots to be  $2r$  since two consecutive slots may be occupied by an FLS. Slots move either clockwise or counter clockwise.

A centralized scheduler hosted on the Hub [31], see Figure 1, of the DV may maintain the coordinates of the slots on the flight pattern and assign a vacant slot to an FLS. This raises the following research questions: First, what algorithms enable an FLS to compute a path from its current coordinate to rendezvous with its assigned

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slot? Second, what are their tradeoff? This paper provides an answer to these two questions.

We present two algorithms, Shortest Distance (SD) and Fastest Rendezvous Time (FRT), for an FLS to rendezvous with its assigned slot. As implied by their names, SD computes the shortest distance while FRT computes the fastest time. We provide analytical models, simulation studies, and an implementation of the circular flight pattern. We use the simulation model to quantify the tradeoff associated with SD and FRT. The implementation consists of a swarm of 5 Crazyflie drones using the Vicon localization technique. Figures 3a and 3b show the opening of this implementation from a corner and the bottom, respectively. It verifies the correctness of the analytical models and the simulation model that embodies them. Its output is almost identical to that of the simulation model, see Figure 4 and [video demonstration](#).

**Contributions** of this study include:

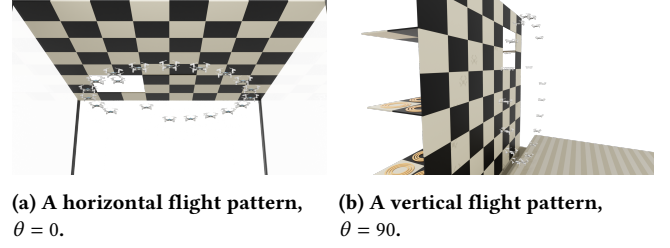
- Design and implementation of circular flight patterns at any angle  $\theta$  relative to the z-axis. It realizes horizontal ( $\theta=0^\circ$ ), vertical ( $\theta=90^\circ$ ), and in-between  $\theta$  values. (Section 2.)
- $\theta$  neutral algorithms to compute the Shortest Distance (SD) and the Fastest Rendezvous Time (FRT) for an FLS to rendezvous with its assigned slot. (Section 2.)
- Analytical models, a simulation study, and an implementation of the flight pattern and the SD and FRT algorithms. The implementation uses a swarm of Crazyflie drones with the Vicon localization system. Click [demonstration](#) for a video.
- An evaluation of SD and FRT, highlighting their tradeoffs. (Section 4.)
- We open source our software implementation and its data set at <https://github.com/flyinglightspeck/CircularFlightPattern>.

The rest of this paper is organized as follows. Section 2 details the design of a circular flight pattern, and SD and FRT algorithms. Section 3 presents an implementation using Crazyflie drones. Section 4 evaluates SD and FRT, quantifying their tradeoffs. Section 5 presents related work. Brief conclusions are presented in Section 6.

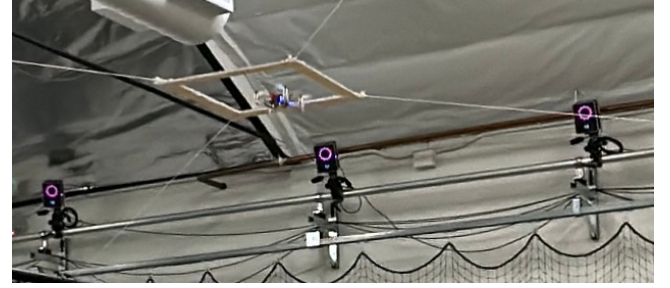
## 2 A CIRCULAR FLIGHT PATTERN SLANTED $\theta$ DEGREES

A single layer circular flight pattern locates on a plane. It has a fixed center  $P_C$ , a radius  $R$ , and  $N$  slots. The slots are rotating either clockwise or counter-clockwise at the linear speed  $S_{slot}$ . A normal vector  $\vec{V}_{Norm}$  defines the angle  $\theta$  between the flight pattern and the z-axis, see Figure 5. The normal vector may be perpendicular to the ground ( $\theta=0$ , horizontal, see Figure 2a), parallel to the ground ( $\theta=90$ , vertical, see Figure 2b), or slanted at  $\theta$  degrees relative to the z-axis. See Figure 5.

To accommodate downwash, the distance between two consecutive slots  $d_s$  is required to be greater than or equal to twice the radius  $r$  of the sphere that models a drone and its downwash,  $d_s \geq 2r$ . The maximum number of slots is  $N = \frac{2\pi R}{2r}$ ,  $d_s = 2r$ . The numerator is the circumference of the flight pattern. The denominator  $2r$  is the minimum allowed distance between two slots. Obviously, a flight pattern may consist of fewer slots  $n$ ,  $n < N$ . In this case the distance between slots may be larger than the required minimum,  $d_s = \frac{2\pi R}{n}$ ,  $d_s \geq 2r$ .



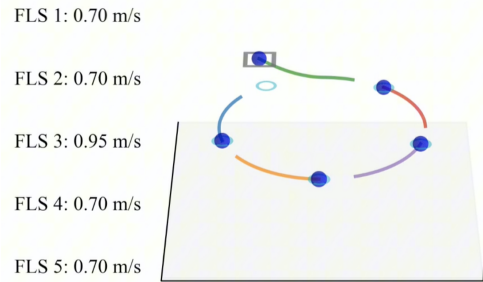
**Figure 2: Dronevision with a circular Flight Pattern: the horizontal ( $\theta=0^\circ$ ) and vertical ( $\theta=90^\circ$ ) alignment makes the charging coils accessible to FLSs.**



**(a) Corner view of the opening.**

**(b) Bottom view of the opening.**

**Figure 3: the opening of an implementation with a swarm of Crazyflie drones**



**Figure 4: Visualization of simulation.**



**2.2.1 Closest & Farthest Point.** Flight patterns may have different orientation in the global coordinate system. A general counter-clockwise rotating flight pattern,  $FP$ , lies on a plane  $\Pi$ . The included angle between  $\Pi$  and the positive direction of the z-axis (vector  $[0, 0, 1]$ ) of the global coordinate system is  $\theta$  degree. Let the normal vector of the flight pattern be  $\vec{V}_{Norm} = [x_N, y_N, z_N]$ , where  $|\vec{V}_{Norm}| = 1$ . Similar to previous, let  $P_f = [x_f, y_f, z_f]$ , and  $P_C = [x_C, y_C, z_C]$ . See Figure 5. Then,  $\vec{P_f P_C} = [x_C - x_f, y_C - y_f, z_C - z_f]$ . The distance from  $P_f$  to  $\Pi$  can be described as the length of the vector  $\vec{V}_H$ , where  $\vec{V}_H$  start from  $P_f$  and end at a point on  $\Pi$ , and  $\vec{V}_H$  is perpendicular to  $\Pi$ , meaning  $\vec{V}_H \parallel \vec{V}_{Norm}$ . Hence,  $V_H = |\vec{P_f P_C}| \times \cos(\beta) \times |\vec{V}_{Norm}|$ , where cosine value of the included angle between  $\vec{P_f P_C}$  and  $\vec{V}_{Norm}$ ,  $\cos(\beta) = \frac{\vec{P_f P_C} \cdot \vec{V}_{Norm}}{|\vec{P_f P_C}| \times |\vec{V}_{Norm}|}$ . The projection of vector  $\vec{P_f P_C}$  on the plane  $\Pi$ :  $\vec{V}_{proj} = \vec{P_f P_C} - \vec{V}_H$ , and the closest point position  $P_{close} = P_C - R \times \frac{\vec{V}_{proj}}{|\vec{V}_{proj}|}$ , the farthest point position  $P_{far} = P_C + R \times \frac{\vec{V}_{proj}}{|\vec{V}_{proj}|}$ .

The simple horizontal and vertical flight patterns of Figures 2a and 2b are a special case with  $\theta$  set to  $0^\circ$  and  $90^\circ$ , respectively.

**2.2.2 Shortest Distance (SD) Path.** This technique minimizes the distance  $d$  traveled by an FLS to its assigned slot. It computes a straight line with a starting point set to the FLS's coordinates, an end point set to the closest point  $P_{close}$  on the flight pattern, some wait time  $\delta$  at the starting point, and the FLS flight duration. The duration is dictated by the FLS velocity model to travel  $d$  with the time required to decelerate to match the speed of a slot in the flight pattern.

When  $d$  is such that an FLS may reach its maximum speed, we consider 3 variants of SD. Their key difference is the duration of wait time  $\delta$  and the speed used to travel. All variants consider the time to either accelerate or decelerate to match the speed of a slot in a flight pattern.

Variant 1 requires an FLS to travel at its fastest speed  $S_{max}$  by adjusting the duration of  $\delta$ . When compared with the other alternatives, it maximizes the wait time  $\delta_{max}$ . Its highest speed must be as fast as the speed of the slots ( $S_{slot}$ ) in the flight pattern or faster,  $S_{max} \geq S_{slot}$ . When  $S_{max} > S_{slot}$ , Variant 1 considers the time to decelerate to match the speed of its assigned slot  $S_{slot}$ .

Variant 2 requires an FLS to leave its current coordinates as soon as possible. This means it may travel at its slowest speed  $S_{slow} > 0$  to rendezvous with its slot by adjusting the duration of  $\delta$ . It minimizes the wait time  $\delta_{min}$  when compared with the other variants. If  $S_{slow}$  is faster or slower than  $S_{slot}$ , Variant 2 considers the time to decelerate or accelerate to match the speed of its slot.

Variant 3 is a hybrid that uses a speed in between the minimum  $S_{slow}$  and the maximum  $S_{max}$  speed. It is motivated by the observation that the flight time of an FLS on its remaining battery lifetime may be maximized if it travels at a pre-specified speed  $S_{Battery}$ . Assuming this speed is somewhere between the minimum and maximum speed ( $S_{slow} \leq S_{Battery} \leq S_{max}$ ) then, this technique's wait time  $\delta_{hybrid}$  is somewhere between the minimum and maximum

wait times,  $\delta_{min} \leq \delta_{hybrid} \leq \delta_{max}$ . Note that Variant 3 is the same as Variants 1 and 2 when  $S_{Bat}$  equals  $S_{max}$  and  $S_{slow}$ , respectively.

Algorithm 2 implements SD by calculating the position and time for an FLS  $f$  to rendezvous with its assigned slot and its wait time at its starting coordinate denoted  $\delta$ . The three variants can be implemented by using different velocity models for an FLS. These velocity models are presented in Section 2.2.4. Based on the coordinate of the closest point to  $f$  on the flight pattern, this algorithm computes the time for  $f$  to arrive at this position and the time for its assigned slot to arrive at the same coordinate. Algorithm 2 is a sequence of analytical expressions with  $O(1)$  complexity. It outputs the rendezvous time, and the amount of time  $\delta$  that the FLS must wait.

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**Algorithm 2:** SD( $FP, f, P_{close}$ )

---

```

1  $P_{slot} \leftarrow FP.slots[f.sID]$ 
2  $\vec{V}_{(slot,C)} = \frac{\vec{P_{slot} FP.P_C}}{|\vec{P_{slot} FP.P_C}|}$ 
3  $\vec{V}_{(close,C)} = \frac{\vec{P_{close} FP.P_C}}{|\vec{P_{close} FP.P_C}|}$ 
4  $angle_{rotation} = \arccos(\vec{V}_{(slot,C)} \cdot \vec{V}_{(close,C)})$ 
5 if  $(\vec{V}_{(slot,C)} \times \vec{V}_{(close,C)}) \cdot FP.V_{Norm} < 0$  then
6    $angle_{rotation} = 2\pi - angle_{rotation}$ 
7 end
8  $t_{slot} = angle_{rotation} \div \frac{FP.S_{slot}}{FP.R}$ 
9  $t_f = \text{MIN-TIMEVELOCITYMODEL}(|f.P_f P_{close}|)$ 
10 if  $t_{slot} < t_f$  then
11    $t_{round} \leftarrow \frac{2\pi \times FP.R}{FP.S_{slot}}$ 
12    $t_{slot} \leftarrow t_{slot} + \left\lceil \frac{t_f - t_{slot}}{t_{round}} \right\rceil \times t_{round}$ 
13 end
14 if Variant 1 then
15    $\delta = t_{slot} - t_f$ 
16 end
17 else if Variant 2 then
18    $\delta = \text{FIX-TIMEVELOCITYMODEL}(|f.P_f P_{close}|, t_{slot})$ 
19 end
20 else if Variant 3 then
21    $\delta_{hybrid} \leftarrow$  The specified waiting time for Variant 3
22    $\delta = \delta_{hybrid}$ 
23 end
24 return  $[t_{slot}, \delta]$ 
```

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**2.2.3 Fastest Rendezvous Time (FRT) Path.** Algorithm 3 computes the path with the Fastest Travel Time (FRT) for an FLS to rendezvous with its assigned slot. The algorithm computes both the rendezvous time and its coordinate on the flight pattern by using the closest  $P_{close}$  and farthest  $P_{far}$  points on the flight pattern as a guide. Since the distance traveled by the FLS will not be longer than the distance from  $P_f$  to  $P_{far}$ , and will not be shorter than the distance from  $P_f$  to  $P_{close}$ , then the upper and lower bound can be calculated with the velocity model of the FLS using the fastest speed  $S_{max}$ . This defines an interval of time  $[T_{min}, T_{max}]$ . We break this interval into  $\mu$  slices, each with  $\epsilon$  duration,  $\mu = \frac{T_{max} - T_{min}}{\epsilon}$ . FRT uses binary search to determine when the assigned slot will rendezvous with the FLS in a time slice. It uses this slice as input to Algorithm 1 to



determine a point on the flight path. This is the coordinates of the rendezvous location. The complexity of the algorithm is  $O(\log \mu)$ .

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**Algorithm 3:** FRT( $FP, f, P_{close}, P_{far}, \epsilon$ )

---

```

1  $lo \leftarrow \text{VELOCITYMODEL}(|f.P_f P_{close}|)$ 
2  $hi \leftarrow \text{VELOCITYMODEL}(|f.P_f P_{far}|)$ 
3 while  $lo \leq hi + \epsilon$  do
4    $mid \leftarrow (lo + hi) \div 2$ 
5    $P_{slot} \leftarrow \text{GETSLOTPOSITION}(FP, f.SID, mid)$ 
6    $t_{travel} \leftarrow \text{VELOCITYMODEL}(|f.P_f P_{slot}|)$ 
7    $t_{diff} \leftarrow t_{travel} - mid$ 
8   if  $t_{diff} > 0$  then
9      $lo \leftarrow mid + \epsilon$ 
10  end
11  else
12     $hi \leftarrow mid$ 
13  end
14 end
15 return  $[\text{GETSLOTPOSITION}(FP, f.SID, lo), lo]$ 

```

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Algorithm 3 shows the pseudo-code for FRT. Its input includes a flight pattern object  $FP$ , an FLS  $f$ , the closest  $P_{close}$  and farthest  $P_{far}$  points on the flight pattern, and  $\epsilon$  which is the duration of a time slice. Steps 1 and 2 use the velocity model of Section 2.2.4 to compute the time to travel to  $P_{close}$  and  $P_{far}$ , respectively. Steps 3 to 14 implement the binary search technique to compute the FLS rendezvous time with its assigned time slot. The complexity of Algorithm 3 is  $O(\ln \mu)$ .

#### 2.2.4 Velocity Model.

*Assumption:* An FLS has a maximum acceleration  $a^\uparrow$ , a maximum deceleration  $a^\downarrow$ , and a maximum<sup>1</sup> speed  $S_{max}$ . At any time, the FLS may not travel faster than  $S_{max}$ , and the rate of which the FLS's speed changes cannot exceed  $a^\uparrow$  when accelerating or  $a^\downarrow$  when decelerating. Note that all  $S_{max}$ ,  $a^\uparrow$  and  $a^\downarrow$  are scalar values larger than 0, independent of the heading of an FLS.

*Min-Time Velocity Model:* SD (Variant 1) and FRT use the Min-Time Velocity Model. The velocity model describes the acceleration, deceleration, and a maximum speed  $S_{max}$  that an FLS may use to travel distance  $d$ . This is the distance from the FLS's current coordinate  $P_f$  to the coordinates of its assigned slot  $P_s$ ,  $d = |P_f P_s|$ . We assume the starting velocity of the FLS is zero and the maximum FLS speed is higher than the speed of a slot,  $S_{max} \geq S_{slot}$ . Factors such as gravity may cause  $a^\uparrow$  to not equal  $a^\downarrow$ .

**PROBLEM 1.** Minimize the time to travel distance  $d$  from  $P_f$  to  $P_s$  without exceeding the maximum speed  $S_{max}$ , or exceeding either the maximum acceleration  $a^\uparrow$  or maximum deceleration  $a^\downarrow$ .

Three scenarios constitute the solution to this problem:

- (1)  $d$  requires the FLS to accelerate at rate  $a^\uparrow$  to reach  $S_{max}$ , travel at speed  $S_{max}$  until a well defined point, and decelerate at rate  $a^\downarrow$  to match the speed of its assigned slot at  $P_s$ .
- (2)  $d$  requires the FLS to accelerate at rate  $a^\uparrow$  to reach  $S_{max}$ . However, the FLS must decelerate immediately at the rate  $a^\downarrow$  to match the speed of its assigned slot at  $P_s$ .
- (3)  $d$  requires the FLS to accelerate to arrive at a well defined point. Prior to reaching  $S_{max}$ , the FLS must decelerate to  $S_{slot}$ , the speed of its assigned slot at  $P_s$ .
- (4)  $d$  is too small, i.e., the FLS is too close to the slot, preventing the FLS from accelerating to match the speed of its slot at  $P_s$ .

An FLS detects the different scenarios using distance  $d$  to its destination, distance  $\Delta_a$  ( $\Delta_p$ ) required to accelerate to  $S_{max}$  ( $S_{slot}$ ), and distance  $\Delta_d$  required to decelerate to match  $S_{slot}$  from  $S_{max}$ . The FLS is in Scenario 1 when  $\Delta_a + \Delta_d$  is less than  $d$ , Scenario 2 when  $\Delta_a + \Delta_d$  equals  $d$ , Scenario 3 when  $\Delta_a + \Delta_d$  is greater than  $d$ , Scenario 4 when  $\Delta_p$  is greater than  $d$ . Note that the ideal scenario (not listed) is when  $\Delta_p$  equals to  $d$  as it enables an FLS to accelerate from rest to occupy its slot at speed  $S_{slot}$ .

Below, we describe how an FLS computes  $\Delta_a$  and  $\Delta_d$ . Subsequently, we detail each scenario in turn.

*Detection of alternative scenarios:* The velocity of an FLS at time  $T + t$  is a function of its speed at time  $T$  and acceleration or deceleration afterwards:  $V_{i+1} = V_i + a\delta$ . Where  $\delta$  is the duration of the step.  $V_i$  is a value between 0 and  $S_{max}$ ,  $V_i \in [0, S_{max}]$ . The distance an FLS travels while accelerating or decelerating in time  $t$  is:

$$\Delta = V_i t + \frac{1}{2} a(t)^2 \quad (1)$$

Where  $V_i$  is the starting speed and  $a$  is set to either  $a^\uparrow$  or  $-a^\downarrow$  depending on whether the FLS is accelerating or decelerating, respectively.

Consider the scenario when an FLS accelerates from a starting velocity of zero to reach the maximum speed. The amount of time required to reach the maximum speed  $S_{max}$  is  $\frac{S_{max}}{a^\uparrow}$ . During this time, the FLS travels distance  $\Delta_a$  to reach  $S_{max}$ ,  $\Delta_a = \frac{1}{2} a^\uparrow t^2$ . When decelerating from the maximum speed with the objective to match  $S_{slot}$  then  $V_i$  is  $S_{max}$  and the required time is  $t = \frac{S_{max} - S_{slot}}{a^\downarrow}$ . The traveled distance  $\Delta_d = S_{max} t - \frac{1}{2} a^\downarrow (\frac{S_{max} - S_{slot}}{a^\downarrow})^2$ , see Equation 1.

*Alternative scenarios:* In Scenario 1, the FLS cruises at speed  $S_{max}$  for a distance equivalent to  $\Delta_c = d - (\Delta_a + \Delta_d)$ . Its duration is  $\frac{\Delta_c}{S_{max}}$ . In Scenario 2, once the FLS speed is  $S_{max}$ , it starts to decelerate at the rate  $a^\downarrow$  to arrive at its slot with speed  $S_{slot}$ . With Scenario 3, the FLS uses the following equation to compute the amount of

time to arrive at its slot:  $\frac{\sqrt{2a^\uparrow \frac{a^\downarrow}{a^\uparrow + a^\downarrow}} d}{a^\uparrow} + \frac{\sqrt{2a^\uparrow \frac{a^\downarrow}{a^\uparrow + a^\downarrow}} d}{a^\downarrow}$ . With the last scenario, the FLS must move  $\Delta_p - d$  away from its slot. Now, it is in the ideal scenario to accelerate to match  $S_{slot}$ .

#### Example 1.

Consider a horizontal flight pattern,  $FP.\theta=0$ , rotating at a speed of 0.7 m/second,  $FP.S_{slot}=0.7$  m/second. The radius of this circular flight pattern is 1 meter,  $FP.R=1$  m, and the coordinate of its center is  $[0,0,0.8]$ . An FLS with a starting coordinate  $[1, 1, 0]$  must rendezvous with its assigned slot. The maximum FLS speed is

<sup>1</sup>The speed of a stationary FLS is zero. The minimum speed that an FLS may travel is  $S_{slow}$ . It is dictated by Variant 2 of SD. The velocity model tries to realize  $S_{slow}$ .

$S_{max}=1.5$  m/second. Its maximum acceleration and deceleration are 1 m/second<sup>2</sup>. Hence,  $T_{min} = 0.901$  seconds and  $T_{max} = 2.543$  seconds. Assume the duration of a time slice is  $\frac{1}{30}$  seconds,  $\epsilon=0.033$  seconds. The number of time slots is 36,  $\mu=36$ . Hence, FRT of Algorithm 3 requires  $\lceil \log_2 36 \rceil = 6$  iterations. It computes a straight line path for the FLS to rendezvous with its assigned slot 0.83 seconds from the current time and travel 0.963 m with the fastest speed.

With the same settings, SD of Algorithm 2 (adjusted for Variant 2) requires a flight time of 2.574 seconds. This is more than 3x longer than FRT. However, its traveled distance (0.9 m) is 7% shorter than FRT. One reason for SD's long flight time is its wait time  $\delta = 7.526$  second to rendezvous with its slot.

**Fix-Time Velocity Model:** Variants 2 and 3 use the Fix-Time Velocity Model. This velocity model describes how an FLS may achieve rendezvous speed  $S_{slot}$  after traveling distance  $d$  during time  $T$ . The value of  $T$  is determined by the time to rendezvous with  $t_{slot}$  (see Algorithm 2) and the waiting time  $\delta$ ,  $T = t_{slot} - \delta$ . Similar to the Min-Time Velocity Model,  $d=|P_f P_s|$ , and we assume the FLS starts from the velocity zero and  $S_{max} > S_{slot}$ .

**PROBLEM 2.** Travel distance  $d$  from  $P_f$  to  $P_s$  in a fixed time  $T$  without exceeding the maximum speed  $S_{max}$ , or exceeding either the maximum acceleration  $a^\uparrow$  or maximum deceleration  $a^\downarrow$ .

Four scenarios constitute the solution to this problem:

- (1)  $d$  requires the FLS to continuously accelerate for a duration  $T$  to reach  $S_{slot}$ , so to match the speed of its assigned slot  $P_s$ .
- (2)  $d$  requires the FLS to accelerate to reach  $S_{slot}$ , then travel at speed  $S_{slot}$  until it rendezvous with its slot at  $P_s$ .
- (3)  $d$  requires the FLS to accelerate to reach  $S'_{max}$ , travel at speed  $S'_{max}$  until a well defined point, and decelerate to match the speed of its assigned slot at  $P_s$ . Note that  $S_{slot} < S'_{max} < S_{max}$ .
- (4)  $d$  is too small, i.e., the FLS is too close to the slot, preventing the FLS from accelerating to match the speed of its slot at  $P_s$ .

The acceleration and deceleration of an FLS may not be fixed constant. Multiple optimization approaches can be adapted to calculate a smooth change in acceleration (deceleration) [41, 60]. Here, we describe the simplest version using a constant acceleration and deceleration. An FLS detects different scenarios using distance  $d$  to its destination, speed of its assigned slot  $S_{slot}$  and travel time  $T$ .

**Detection of alternative scenarios:** If  $\frac{S_{slot}^2}{2a^\uparrow}$  is greater than  $d$ , the FLS is in Scenario 4. Otherwise, the FLS is in Scenario 1 when  $\frac{TS_{slot}}{2}$  is greater than or equal to  $d$ , Scenario 2 when  $\frac{TS_{slot}}{2}$  is smaller than  $d$  and  $\frac{S_{slot}^2}{2a^\uparrow} + (T - \frac{S_{slot}}{a^\uparrow})S_{slot}$  is greater than or equal to  $d$ , Scenario 3 when  $\frac{S_{slot}^2}{2a^\uparrow} + (T - \frac{S_{slot}}{a^\uparrow})S_{slot}$  is smaller than  $d$ . Note that there is one special case in Scenario 3, where  $S'_{max} = S_{max}$ , the acceleration is  $a^\uparrow$ , and the deceleration is  $a^\downarrow$ . In this case, Fix-Time Velocity Model generates the same moving pattern as the Min-Time Velocity Model. This may happen when  $\delta_{min}$  and  $\delta_{hybrid}$  in Variant 2 and 3 of SD and  $\delta_{max}$  of Variant 1 of SD are all limited to 0 by  $d$  and  $T$

Below, we fill in the detailed acceleration and deceleration of an FLS in different scenarios based on a constant acceleration and deceleration model.

With Scenario 1, an FLS may accelerate with the rate of  $a^\uparrow$ ,  $a^\uparrow = \frac{S_{slot}^2}{2d}$ . It will reach speed of  $S_{slot}$  by the time it rendezvous with its assigned slot.

With Scenario 2, the time that an FLS may accelerate is  $t^\uparrow$ ,  $t^\uparrow = 2(T - \frac{d}{S_{slot}})$ . Hence the acceleration  $a^\uparrow$  can be calculated accordingly,  $a^\uparrow = \frac{S_{slot}^2}{t^\uparrow}$ . Once it reach the speed of  $S_{slot}$ , it will move with this constant speed and

For Scenario 3, there are multiple ways an FLS can do to achieve the goal. An FLS maximize its accelerating time  $t^\uparrow$  and later have a longer decelerating time  $t^\downarrow$ , or the opposite, or choose a balance between these two. There are three constraints on  $t^\uparrow$  and  $t^\downarrow$ :

$$T \geq t^\uparrow + t^\downarrow \quad (2)$$

$$d = \frac{S'_{max} t^\uparrow}{2} + \frac{(S'_{max} + S_{slot}) t^\downarrow}{2} + (T - t^\uparrow - t^\downarrow) S'_{max} \quad (3)$$

$$\begin{cases} S'_{max} \leq a^\uparrow t^\uparrow \\ S'_{max} \leq a^\downarrow t^\downarrow + S_{slot} \end{cases} \quad (4)$$

Here, we provide the equation for calculation with a focus on minimizing the accelerating time  $t^\uparrow$  and the decelerating time  $t^\downarrow$  by using  $a^\uparrow$  and  $a^\downarrow$  for acceleration and deceleration. Equation 3 can be re-formalized as:

$$d = \frac{S'^2_{max}}{2a^\uparrow} + \frac{(S'^2_{max} + S_{slot})}{2a^\downarrow} + (T - \frac{S'_{max}}{a^\uparrow} - \frac{S'_{max}}{a^\downarrow}) S'_{max} \quad (5)$$

and  $S'_{max}$  can be calculated accordingly:

$$S'_{max} = \frac{T - \sqrt{T^2 - (\frac{1}{a^\uparrow} + \frac{1}{a^\downarrow})(\frac{S_{slot}}{2a^\uparrow} - d)}}{\frac{1}{a^\uparrow} + \frac{1}{a^\downarrow}} \quad (6)$$

### 3 IMPLEMENTATION

We developed a simulation model of the techniques and implemented them using a swarm of Crazyflie drones. We specified a horizontal circular flight pattern with a radius of 1 meter,  $R=1$ ,  $\theta=0$ . It rotates counter-clockwise. The speed of its slots is 0.7m/second. The slots are separated by a distance of 125.66 cm ( $\frac{2\pi \times 1m}{5}$ ) and are 1.79 seconds apart. The diameter of a Crazyflie is 15 cm (including span of propellers). We set its maximum speed  $S_{max}$  at 1.5 m/second, and maximum acceleration and deceleration at 1m/second<sup>2</sup>. The dimensions of the space is 3m  $\times$  3m  $\times$  1.5m, and the opening is 27cm  $\times$  27cm. Figures 3a and 3b show the side and bottom view of the opening of our implementation. A visualization of the simulation model is shown in Figure 4.

Our implementation starts with 5 Crazyflies at a stationary state on the ground. They fly to 5 random initial coordinate. Each drone is assigned with available slots using a Round Robin policy. We use the equations of Section 2.2.2 to compute the shortest path for each FLS to occupy its assigned slot, starting with the speed of zero.

The sudden turns when FLSs are rendezvousing with their assigned slots are handled by crazyswarm platform [66].

Once an FLS rendezvous with its assigned slot, it occupies the slot and flies at the speed of the slot until it is below the opening. Subsequently, it enters the opening and relinquishes its slot. The FLS flies to a corner of the display space, descends to the floor, and flies to its newly assigned random starting position to repeat the process. An experiment has a duration of one minute. It terminates by landing the 5 FLSs on the ground. See [implementation](#).

#### 4 EVALUATION

We used the experimental setup of Figure 6 to quantify the tradeoff associated with SD and FRT, Algorithms 2 and 3, respectively. The important configuration parameters of the flight pattern include its radius  $R=1$  meter, the speed of slots 0.7 m/second, and the number of slots 5. We simulated starting point for one FLS along a line that is a fixed distance below the center of the flight pattern. This distance is a function of the radius of the flight pattern,  $\omega \times R$ . We vary the value of  $\omega$  from 1 to 1000 including in between values. The distance between the points on the line is fixed at 1 meter, i.e., Point 10 is 9 meters away from Point 1 which is aligned below the center of the flight pattern. See Figure 6.

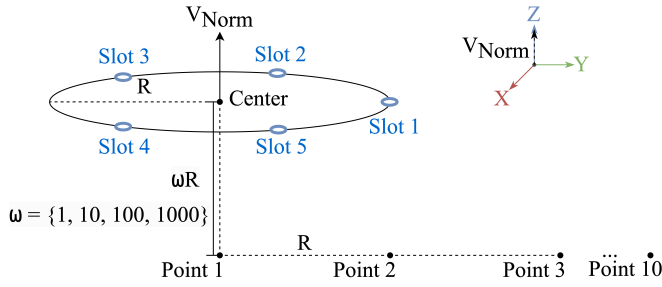


Figure 6: Experimental setup.

*Summary of lessons:* We conducted many experiments. A summary of lessons learned include: First, SD results in a shorter travel distance compared to FRT while FRT results in a faster rendezvous time when compared with SD. Second, the difference between SD and FRT becomes insignificant as we increase the distance between an FLS and its assigned slot, i.e.,  $\omega \geq 100$ . Third, minimizing the time for a slot to make a rotation on the flight pattern expedites the FLS rendezvous time with an FLS. Similarly, increasing the FLS speed, its acceleration and deceleration expedites its rendezvous time with an FLS. Fourth, with SD, the shortest distance may be such that an FLS arrives at the rendezvous point and misses its assigned slot. In this case, the FLS must wait for one rotation of the slot, delaying the rendezvous time. See Figure 7b.

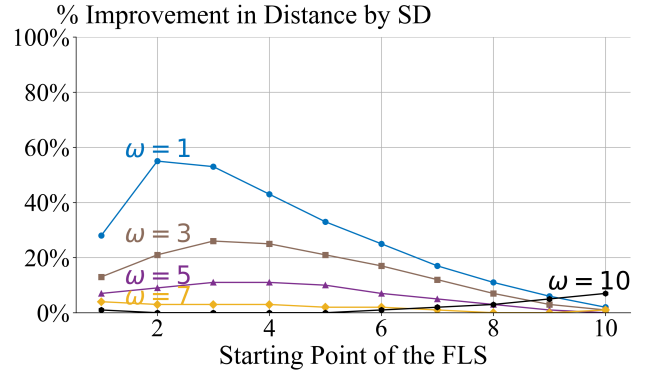
Table 1 shows the numerical results of distance traveled and time spent by FLS starting at point 1, assigned with Slot 2, different values of  $\omega$ .

*Detailed Results:* The experimental results presented in this section use a flight pattern with the specification of Example 1 and our Crazyflie implementation of Section 3.

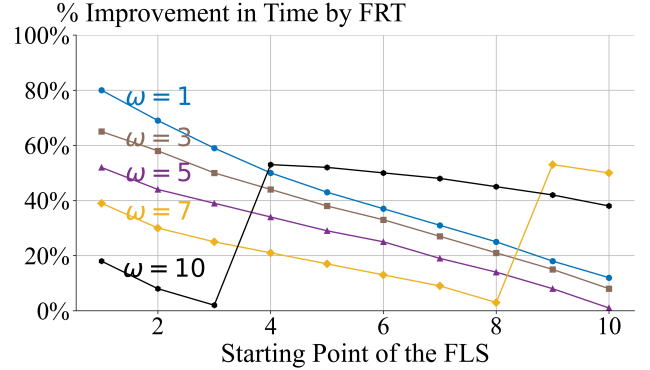
Figure 7a shows the percentage improvement in distance provided by SD when compared with FRT. The x-axis of this figure

Table 1: Traveled distance and rendezvous time, SD and FRT.

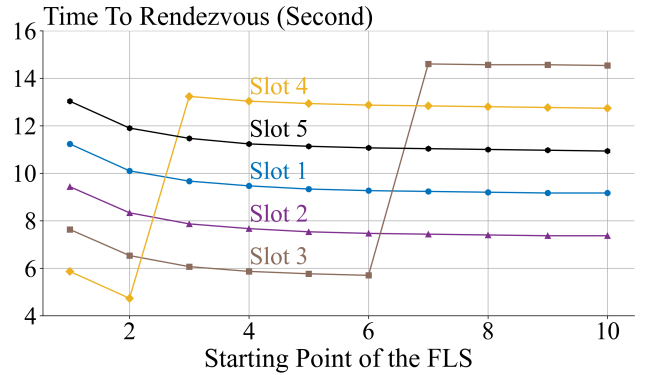
$\omega$	Dist Traveled (m)		Time (second)	
	SD	FRT	SD	FRT
1R	1.00	1.40	9.43	1.87
5R	5.00	5.38	9.43	4.57
10R	10.00	10.06	9.43	7.70
100R	100.00	100.02	72.27	67.67
1000R	1,000.00	1,000.00	673.67	673.67



(a) SD's % improvement in distance when compared with FRT.



(b) FRT's % improvement in time when compared with SD.



(c) Rendezvous time with different slot assignments, SD,  $\omega=5$ .

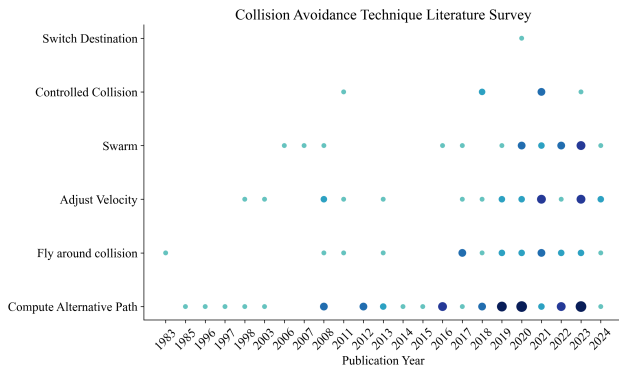
Figure 7: An evaluation of SD and FRT.

denotes the points on the line below the flight pattern. An FLS is assigned Slot 2. (We discuss other slots at the end of this section.) SD's highest percentage improvement is observed with low values of  $\omega$  (e.g.,  $\omega=1$ ), i.e., when the line is closest to the flight pattern. This improvement decreases as we increase  $\omega$ . Beyond  $\omega \geq 10$ , the percentage improvement provided by SD is insignificant because the traveled distance is large. This distance dominates to make the difference between the closest  $P_{close}$  and farthest  $P_{far}$  point (fixed at 2R) on the flight pattern insignificant.

Figure 7b shows the percentage improvement in time by FRT when compared with SD as a function of the points on the line. The different lines correspond to the different values of  $\omega$ . The percentage improvement provided by FRT decreases as a function of  $\omega$  with a few exceptions. The percentage decrease is due to an increase in the distance traveled by the FLS. SD requires the FLS to fly at the fastest speed similar to FRT. With sufficiently large distances, the rendezvous time to the closest point versus to a point between the closest and farthest points on the flight pattern becomes insignificant. This explains the decrease in percentage improvement as a function of  $\omega$ . This explanation also applies to the general decrease of a line, say  $\omega = 1$ , as a function of the points on the line. Point 10 is 10x farther away than Point 1, rendering the aforementioned different insignificant.

Figure 7b shows sudden jumps in the percentage improvement with  $\omega$  values 7 and 10. This is due to an FLS arriving at its rendezvous point  $P_{close}$  only to miss its assigned slot. The FLS waits for the slot to make a full rotation. This results in a significant increase in rendezvous time with SD. Note that SD requires the FLS to travel at its fastest speed. Reducing its speed will only increase the percentage improvement provided by FRT.

The slot assigned to an FLS dictates whether it must wait for a rotation of the slot. Figure 7c highlights this by focusing on  $\omega=5$ . It shows the time to rendezvous for different slots on the flight pattern as a function of the FLS location on the line, i.e., points shown in Figure 6. While with Slots 1, 2, and 5, the rendezvous time is a line that decreases smoothly and tends to flatten out, it increases with Slots 3 and 4 due to an FLS waiting for either a full or a partial rotation of its slot.



**Figure 8: 97 collision avoidance/handling studies.**

**Table 2: A summary of FRT and variants of SD.**

	Distance Traveled	Flight Time	Battery Flight Time
<b>SD:V1</b>	Optimizes	Optimizes	X
<b>SD:V2</b>	Optimizes	X	X
<b>SD:V3</b>	Optimizes	X	Optimizes
<b>FRT</b>	X	Optimizes	X

## 5 RELATED WORK

The concept of flight patterns for use by a Dronevision is first introduced in [107]. It presents alternative shapes for a flight pattern, e.g., square, circle, and ellipsoid. It also describes flight patterns that are either single layer or hierarchical. We focus on the circular pattern of [107] and extend it by presenting different angles  $\theta$  for a flight pattern relative to the Z-axis, and algorithms SD and FRT that enable an FLS to rendezvous with its assigned slot on the flight pattern. We present analytical models, simulation studies, and an implementation using a swarm of Crazyflie drones. These novel extensions are absent from [107].

Our novel extensions are absent from prior studies in collision handling techniques. This is based on our survey of 97 studies that were published from 1983-2024 . Figure 8 shows the six forms of collisions as a function of the publication year. The size of a circle and its darkness denotes the number of studies, ranging from 1 to 6. 48 studies compute an alternative path [10, 11, 14, 18, 19, 22, 23, 28–32, 34–36, 38, 40, 42, 45, 47–49, 52, 57, 58, 62, 68, 72, 74, 78, 80, 82, 84, 85, 87, 90, 92, 95–97, 99, 100, 102–105, 108], 21 studies fly around the collision point [3, 12, 15, 17, 21, 23, 24, 27, 43, 44, 53, 66, 67, 71, 76, 77, 83, 86, 91, 93], 26 studies adjust velocity [17, 20, 21, 23, 27, 28, 30, 38, 43–45, 51, 52, 54, 64, 67, 72, 76, 79, 80, 83, 86, 91, 93, 97, 99], 27 studies employ a swarming technique [1, 2, 5–8, 12, 16, 20, 25, 30, 31, 33, 39, 55, 59, 63, 65, 66, 73, 88, 89, 98, 101, 105–107], 6 studies use controlled collision [46, 51, 54, 56, 61, 64], and 1 study switches destination of the colliding agents [76] <sup>2</sup>.

We also analyzed more recent papers related to drone swarm managements [9, 69, 70, 75]. None have the concept of a flight pattern, SD and FRT algorithms.

## 6 CONCLUSION

This paper presents the design and implementation of a circular flight pattern that enables a swarm of FLSs to enter an opening of a 3D multimedia display, Dronevision. This opening provides FLSs with access to charging coils. We presented two novel algorithms, SD and FRT, that enable an FLS to occupy its assigned slot with the flight pattern at an arbitrary angle  $\theta$  relative to the z-axis. The 3 variants of SD optimize for different metrics as shown in Table 2. One may view Variant 1 of SD as a hybrid of FRT that prioritizes optimizing traveled distance followed with travel time. Experimental results show SD minimizes the distance traveled by an FLS while FRT minimize the time traveled. Our [implementation](#) using a swarm of Crazyflie drones validates the correctness of our designs. Both our design and implementation scale to a large number of drones and slots. While we focused on a 3D multimedia display, the

<sup>2</sup>Total is 129 since a study overlaps multiple categories.



concept of a flight pattern and our algorithms are flexible for use by other applications that require a swarm of drones to fly through an opening.

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