

Fig. 2. S_{11} parameter of the proposed antenna.

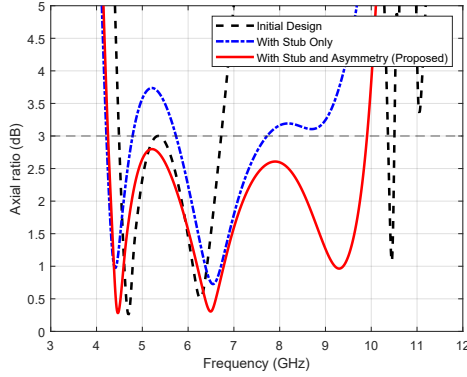


Fig. 3. Axial ratio of the proposed antenna.

4.26 GHz and 5.16 GHz, while the upper resonance frequency remains relatively unchanged, resulting in an increased 10-dB RLBW of 7.67 GHz. This modification also introduces a new upper resonant point at around 9 GHz in the AR curve, although the AR value at this point exceeds 3 dB. Finally, asymmetry between the ground planes is introduced, and the vertical extension of the C-shaped patch is modified. While the increased 10-dB RLBW is maintained, the AR at the new resonance point decreases below 3 dB, significantly enhancing the ARBW to 5.66 GHz. Figure 4 presents the simulated radiation patterns for left-hand circular polarization (LHCP) and right-hand circular polarization (RHCP) in both the XZ plane ($\phi = 0^\circ$) and YZ plane ($\phi = 90^\circ$). The significant separation between LHCP and RHCP patterns in the broadside direction clearly indicates that the antenna exhibits LHCP characteristics. Figure 5 illustrates the peak gain and radiation efficiency of the proposed antenna. Throughout the ARBW, the antenna maintains a peak gain exceeding 3.5 dB while simultaneously achieving a remarkably high radiation efficiency of over 95%. These results demonstrate the antenna's excellent performance across its operational bandwidth.

IV. CONCLUSION

This paper presents a flexible wideband CP antenna that covers multiple frequency bands, including the C-band (4-8

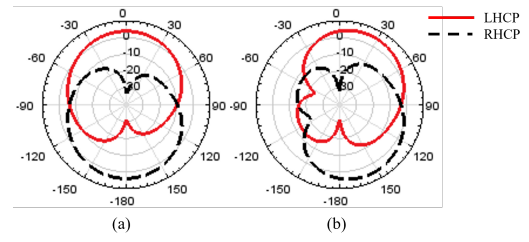


Fig. 4. Radiation pattern of the antenna at 6.51 GHz, where (a) $\phi = 0^\circ$, and (b) $\phi = 90^\circ$.

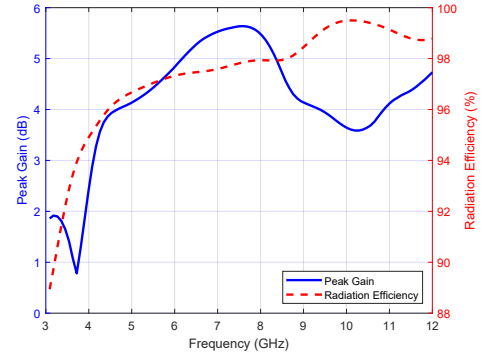


Fig. 5. Peak gain and radiation frequency of the proposed antenna.

GHz), portions of the X-band (8-12 GHz), the 5.8 GHz ISM band, and the 5 GHz Wi-Fi band. Utilizing a CPW-feeding mechanism simplifies fabrication and facilitates integration with other circuits, while the flexible PET substrate allows for seamless incorporation into IoT devices. Future work will explore multiple-input multiple-output (MIMO) technology and analyze the antenna's performance under bending. The antenna will be fabricated using inkjet printing technology, with measured results compared to simulations to validate performance.

ACKNOWLEDGEMENT

This work was supported by the National Science Foundation (NSF) under Grant No. ECCS-2104513.

REFERENCES

- [1] S. G. Kirtania, A. W. Elger, M. R. Hasan, A. Wisniewska, K. Sekhar, T. Karacolak, and P. K. Sekhar, "Flexible antennas: A review," *Micromachines*, vol. 11, no. 9, p. 847, Sep. 2020.
- [2] A. R. Hossain, M. S. I. Sagar, A. A. Mertvy, P. K. Sekhar and T. Karacolak, "Inkjet Printed Flexible Dual-Band Dual-Sense Circularly Polarized Patch Antenna," in *IEEE Access*, vol. 12, pp. 55424-55433, 2024.
- [3] S. Kumar, G. H. Lee, D. H. Kim, H. C. Choi, and K. W. Kim, "Dual circularly polarized planar four-port MIMO antenna with wide axial-ratio bandwidth," *Sensors*, vol. 20, no. 19, p. 5610, Oct. 2020.
- [4] K. Ding, C. Gao, T. Yu and D. Qu, "Broadband C-Shaped Circularly Polarized Monopole Antenna," in *IEEE Transactions on Antennas and Propagation*, vol. 63, no. 2, pp. 785-790, Feb. 2015.
- [5] F. M. Alnahwi, Y. I. A. Al-Yasir, N. T. Ali, I. Gharbia, C. H. See and R. A. Abd-Alhameed, "A Compact Wideband Circularly Polarized Planar Monopole Antenna With Axial Ratio Bandwidth Entirely Encompassing the Antenna Bandwidth," in *IEEE Access*, vol. 10, pp. 81828-81835, 2022.